RedRiver
RESOURCES LIMITED

ACN 100 796 754

ASX Announcement

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Waterloo Deposit – Updated Mineral Resource Estimate

Highlights

- **JORC 2012 Resource estimate for Waterloo Deposit of 707kt @ 19.1% zinc equivalent**
- **Waterloo mine design and production schedule currently being completed by Mining One**
- **Exploration program underway to identify extensions to known mineralisation and target additional mineralisation**

Zinc developer Red River Resources Ltd ("Red River" or the "Company") is pleased to announce an updated mineral resource estimate for the Waterloo deposit, part of its Thalanga Zinc Project, 60km south-west of Charters Towers in Central Queensland.

Table 1 Waterloo Mineral Resource Estimate

Resource Class	Tonnage (kt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Zn Eq. (%)
Transition							
Indicated	97	3.2	2.4	14.5	1.6	78	21.7
Inferred	69	0.8	1.1	6.4	0.4	24	7.8
Subtotal	166	2.2	1.9	11.1	1.1	55	15.9
Fresh							
Indicated	309	2.5	2.0	13.0	1.3	65	25.5
Inferred	232	0.9	0.8	8.3	0.4	28	13.0
Subtotal	541	1.8	1.5	11.0	0.9	49	20.1
Total	707	1.9	1.6	11.0	0.9	50	19.1
Oxide							
Inferred	55	0.2	2.3	0.1	3.7	15	-

Source: Mining One Consultants, 7 Feb 2015

Tonnages and grades are rounded. Discrepancies in totals may exist due to rounding.

Zinc equivalent (Zn Eq) has been calculated using the metal selling prices, recoveries and other assumptions contained in Table 2 of this announcement. It is Red River's opinion that all elements included in the metal equivalent calculation have a reasonable potential to be recovered and sold. Zinc equivalent grade was not calculated for the oxide resource

Red River engaged independent mining consultants Mining One to conduct a review of the previous mineral resource estimate for the Waterloo deposit and to restate the resource estimate in compliance with the JORC Code (JORC 2012). The estimate has been classified as Indicated and Inferred Mineral Resources in accordance with the JORC Code (JORC 2012) and supersedes the previously published JORC 2004 resource estimate for the Waterloo deposit (30 June 2011). The updated Mineral Resource for the Waterloo deposit is reported in Table 1. Please refer to the Waterloo Appendix for the full disclosure as per the JORC Code (2012 Edition).

Zinc equivalent (Zn Eq.) calculation parameters are listed in Table 2. The metallurgical recoveries are derived from historical metallurgical recoveries from the Thalanga deposit and metallurgical test work carried out at the Waterloo deposit. The Waterloo deposit is of a similar style of mineralisation to Thalanga and it is appropriate to apply similar recoveries. It is Red River's opinion that all elements included in the metal equivalent calculation have a reasonable potential to be recovered and sold.

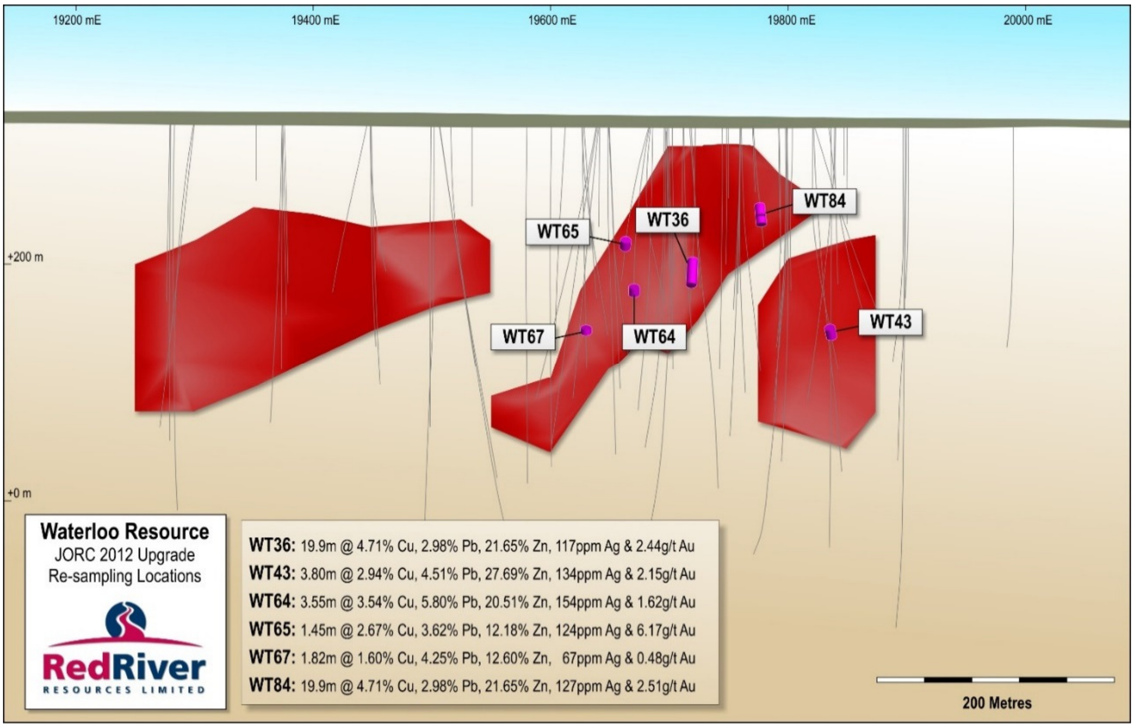
Table 2 Zinc Equivalent Calculation Factors

Metal	Price	Unit	Fresh Resource		Transition Resource	
			Recoveries	Zn Eq. Factors	Recoveries	Zn Eq. Factors
Copper	US$3.00	US$/lb	80%	3.4	58%	2.5
Lead	US$0.90	US$/lb	70%	0.75	0%	0.0
Zinc	US$1.00	US$/lb	88%	1.0	76%	0.84
Gold	US$1,200	US$/oz	50%	0.5	30%	0.4
Silver	US$17.00	US$/oz	65%	0.025	58%	0.01
FX Rate: A$0.85:US$1						

Quality Assurance/Quality Control (QAQC) protocols were implemented during the drilling of the Waterloo deposit, however a recommendation was made by Mining One to conduct a re-sampling program using the remnant half core samples stored at the site core yard facility to ensure that sufficient QAQC data was available to meet the JORC 2012 guidelines for reporting and use of assay data within resource estimates.

A total of 81 samples from 6 drill holes were collected and re-assayed. These samples were selected from ore intervals within the existing resource shapes and represent a spread of sample locations and grades across the Waterloo deposit. The new samples were either quarter or one eighth core cut to match the original intervals. Where possible the entire ore interval including the sample of waste either side was sampled and re-assayed. The location of the re-samples and resultant interval grades are illustrated in Figure 1.

Figure 1 Waterloo Re-sampling Locations



Forward Program

As part of the Thalanga Zinc Project restart study, Red River in conjunction with Mining One consultants are currently working on mine design and production schedules for Waterloo.

Red River has recently completed an induced polarisation survey over the Waterloo Project with the objective of confirming the response of known mineralisation, and seeking to identify extensions to known mineralisation and to target additional mineralisation. This survey successfully fulfilled its objectives, and planning has started on a number of drill holes to follow up on the results of the induced polarisation survey.

As previously announced, the Company is working towards re-starting production at Thalanga by end calendar year 2015.

On behalf of the Board

Donald Garner
Managing Director
Red River Resources Limited

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Competent Person Statement

The information in this report that relates to the estimation and reporting of the West 45 and Orient Resources is based on and fairly represents, information and supporting documentation compiled by Mr Stuart Hutchin who is a Member of The Australasian Institute of Mining and Metallurgy, Member of the Australian Institute of Geoscientists and a full time employee of Mining One Consultants Pty Ltd.

Mr Hutchin has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

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JORC Code, 2012 Edition – Table 1 (Waterloo Deposit)

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• The deposit was primarily sampled via NQ2 half core samples based on geological considerations within diamond drill holes drilled on a 40m x 40m pattern through the deposit area. • The holes were orientated to ensure drill intersections were approximately perpendicular to the dip and strike of the ore lenses and overall geological package. • Diamond core samples were analyzed for Cu, Pb, Zn, Ag and Fe by atomic absorption spectrum (A103) that used a mixed acid digest. Gold was analyzed for via 50g fire assay with an atomic absorption spectrum finish (method PM209).
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• A total of 92 diamond and RC holes holes have been drilled in the Waterloo project area, of these a total of 45 diamond holes have been used to estimate resources for the project. The diamond core size drilled was predominately with standard tube HQ3/NQ2 sized core and sometimes down to BQ sized core where difficult ground conditions were encountered. • Downhole surveys have been taken at 30m intervals on average for each of the holes with single shot Eastman cameras used for the earlier programs and a digital shot Reflex camera for the Kagara programs.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• The diamond core drill recovery was monitored using a combination of the drillers run sheets, core block markings and manual piecing together of core and measurement by Geologists and Field Assistants in the core processing facility. Any core loss was noted within the logging sheets. • The resource is based on diamond drilling, the deposit predominately consists of zinc, lead and copper mineralization, there are no concerns regarding loss of fine material during the core sampling process for this deposit.

Criteria	JORC Code explanation	Commentary
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• All diamond core was logged for geological and geotechnical characteristics. Rock type, alteration style and sulphide mineral content were logged by a site geologist. The logging was sufficient to enable creation of detailed geological model that supports the resource estimate. Core photographs are taken of each core tray and stored as part of the resource database dataset.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• HQ3 sized diamond core was marked up and cut in half with a diamond core saw. The right side of the core as sampled according to the geological intervals selected by the site Geologist. • The methodology of selecting half core via geological intervals guarantees that the core samples are representative. • The sample sizes vary from material sourced from the core samples given the varying sample lengths. • The sample sizes are appropriate given the relatively even distribution of base metal grades within the deposit
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• The ALS laboratory – Charters Towers completed internal standard and duplicate samples. In addition to this Red River Resources have completed a series of 81 duplicate samples on remnant Waterloo drill core to add further support to the QAQC process relating to the deposit. The results from the January 2015 duplicate sampling indicate a 0.97 correlation coefficient with the original drill core samples, this provides confirmation that the original source assay database is suitable for use in resource estimation.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Holes are drilled to within 25m of each other in some areas of the deposit as either twins or scissor holes, the assay data in these holes is consistent through the mineralized zone between the holes. • Data was entered into a central database and then validated by a series of validation checks to ensure erroneous data was not saved into the resource database.

Criteria	JORC Code explanation	Commentary
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• The Waterloo local grid was used to cover the Waterloo deposit. All holes were surveyed using the site survey team who used an EDM theodolite. • The topography surface is represented by a wireframe file that has been edited over time by the site survey team. The surface covers the complete Waterloo deposit area. The surface is an accurate representation of the actual topographic surface at the site.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• The Waterloo deposit has been drilled on an average spacing of 40m x 40m in the main resource area and down to 25m x 25m in some places. This drill spacing provides evidence of mineralized zone continuity for the purposes of resource estimation. • No sampling compositing was necessary in the initial diamond drilling however compositing of raw assay data was completed in preparation for the resource estimation process.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• The majority of diamond holes were orientated to provide an approximate perpendicular intersection angle with the main mineralized zones. • No sampling bias is assessed as been caused by the orientation of the drilling orientation. Scissor holes provide confirmation of domain orientations and thickness.
Sample security	• *The measures taken to ensure sample security.*	• Samples were supervised by either the drill crew, field assistant or geologist and at all times. Given the base metal nature of the deposit sample security was no assessed as a significant risk.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• A due diligence review of the resource estimation was completed by Mining One Consultants was completed in November 2013.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The Waterloo Deposit is situated within Exploration Permit; EPM 10582 • This tenement form part of the Thalanga project acquired by Red River Resources from the previous operator Kagara Copper Pty Ltd in October 2014. This tenure is currently pending title transfer from Kagara Copper Pty Ltd to Cromarty Resources Pty, a wholly owned subsidiary of Red River Resources. Application for transfer lodged 26/03/2015. • The tenements are in good standing and not subject to any material issues with third parties or joint venture arrangements
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Penarroya (Australia) Pty Ltd, Pancontinental Pty Ltd and RGC (Thalanga) Pty Ltd drilled a total of 39 diamond holes between 1984 and 1997. KCPL drilled a total of 53 further diamond holes in 2007 and 2008. The majority of older core intersections through the ore horizon are NQ2/NQ3 with some BQ drilling completed by Penarroya in the earlier programs. Most of Kagara's diamond drilling was HQ3. .
Geology	• *Deposit type, geological setting and style of mineralisation.*	• The Waterloo deposit is a VHMS style deposit that consists of a zone of massive and semi-massive sulphides developed within a rhyolitic quartz eye volcaniclastic within a larger andesite dominated volcano-sedimentary sequence.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* – *easting and northing of the drill hole collar* – *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* – *dip and azimuth of the hole* – *down hole length and interception depth* – *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• A list of each resource drillhole location and interval is located as an appendix to this table, see below.

Criteria	JORC Code explanation	Commentary
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• The exploration results reported for the Waterloo deposit were included as weighted average assay intervals for Zn, Cu, Ag and Pb. No cutting of high grades was completed when reporting as exploration results
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• The typical drill sample interval is 1m in length, the average thickness of the mineralized zone is 5m, there are no issues with reporting the results based on this. • The drillholes intercepted the mineralized lenses at an approximately perpendicular angle. All exploration results were reported as downhole thicknesses.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• See Appendix 4 for a location plan of all drill collars used in the resource estimate.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All ore domain intercepts are listed in Appendix 3
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• No other exploration data reported
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• A detailed economic assessment is to be completed to establish likelihood of establishing project reserves. • No additional drilling planned at this stage.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• The survey, sampling and logging data was electronically imported into the resource database. Checks were also made of the original lab sample sheets and the database to ensure that transcription errors were not present. A visual check was also made of the drill traces, assay and logging data in the 3D environment of Surpac to ensure that results correlated between drillholes and were in line with the geological interpretation and mineralization continuity.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• A site visit was completed by Stuart Hutchin during 2013 where the Waterloo prospect and core samples were inspected.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• The confidence in the overall geological interpretation is high given the continuity of the mineralized zone defined at the 40m x 40m drill spacing. • The andesite, sediments and quartz eye volcanclastic geological units have been modelled and are used to define general areas of rock types within the deposit. The mineralized zones typically occur within the quartz eye volcanoclastics. • The mineralized lenses occur within the quartz eye volcanoclastic package, they are discrete pods of massive sulphide and stringer mineralization.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The strike length of the overall mineralized zone is 600m, thickness of the zones ranges from 5m to 10m. The resource domains are located from 50m below the surface topography and extend to a depth of 200m below surface.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes*	• The resource model was constructed using Surpac software. Mineralised domain wireframes were constructed by modelling the geological cut-off seen in the logging for both the massive sulphide zone and the stringer zone. A minimum domain thickness of 2m was used, this corresponds to the minimum practical mining width within an underground operation. • High grade Zn, Cu, Pb, Ag and Au were top cuts were applied using the 95th percentile method. For the Central massive sulphide zone a total of 8 copper assay values were cut and 7 for lead

Criteria	JORC Code explanation	Commentary
	appropriate account of such data. • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	and zinc. • A composite file was created using an average composite length of 1m. The average sample length within the assay dataset is also 1m. • Variograms were not created due insufficient quantity of sample pairs within the relatively small dataset, meaningful variograms were not created. • An inverse distance estimate was run given the lack of variograms. This method is however deemed to be suitable given the style and orientation of the mineralization. • A 12.5m x 12.5m x 2.5m (RL) parent block size was used with sub blocking to 0.78125m x 0.78125m x 0.15625m (RL) used.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• The resource tonnages have been estimated on a dry basis
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• A cutoff using 5% Zn Eq has been used to report resources. This was chosen as the lower limit of potentially economically extractable material within an underground mining operation in this style of deposit. The zinc equivalent formula used is: ZnEq% = Zn% + (0.77 x Pb%) + (4.46 x Cu%) + (1.46 x Au g/t) + (0.06 x Ag g/t)
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions.*	• The resources have been estimated using a minimum thickness of 2m for each of the domain shapes, this minimum thickness therefore accounts for any dilution in zones that are less than this thickness. The proposed mining method is via underground long hole stoping techniques, the model parameters are therefore deemed to be suitable for this type of potential mining operation.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral*	• The ore is planned to be crushed and a concentrate containing Zn, Pb, Ag and Cu produced, metallurgical test work has shown that a saleable concentrate can be produced from the Waterloo ore. The ore will be processed at the existing Thalanga processing facility.

Criteria	JORC Code explanation	Commentary
	Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The tailings produced during the creation of the concentrate will be disposed of at the currently permitted Thalanga tailings facility. Waste rock from the mine will be placed on the existing waste dump locations.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• The bulk densities for the ore and waste rock types were estimated using the Archimedes method, that is (Dry Weight / (Dry Weight – Wet Weight). Bulk density measurements were obtained for all sample intervals within the diamond drill holes with a total 1,174 samples collected.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The resources have been classified according to the drill density and the modelled continuity of both the thickness and grade of the mineralized zones in the view of the resource geologist. Only indicated and inferred blocks have reported for the resource, no measured blocks are reported. • The resource classification is deemed appropriate in relation to the drill spacing and geological continuity of the mineralized domains.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• Mining One consultants completed a review of the Waterloo resource as part of a due diligence program. No critical flaws were highlighted with the source data set or the modelling methodology.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical*	• The resource estimate is deemed to be an accurate reflection of both the geological interpretation and tenure of mineralization within the deposit.

Criteria	JORC Code explanation	Commentary
	procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	

APPENDIX 1

WATERLOO – DRILLHOLE COLLAR LOCATIONS

HOLE_ID	HOLE_DEPTH	LOCAL_EAST	LOCAL_NORTH	RL
WT1	92	19792.2	19691.5	320.99
WT10	214.05	19696.45	19829.67	323.32
WT11	85.4	19792.61	19940.26	321.3
WT12	299.75	19696.3	19819.19	323.1
WT13	288.3	19373.46	19759.33	323.87
WT14	166.2	19899.67	19990.26	321.64
WT15	102.5	19700.089	19963.961	323.986
WT16	358.25	19900.27	20100.05	322.61
WT17	147.5	19700.088	19970.923	324.063
WT18	337.4	19601.56	20025.92	325.15
WT19	189	19279.97	19938.11	324.72
WT1A	123.5	19792.2	19691.5	320.99
WT2	475.55	19792.2	19693.5	320.96
WT20	207.5	19500.121	19962.156	324.897
WT21	340.6	19279.82	20007.98	325.03
WT22	333.5	19499.96	20031.82	325.25
WT23	509.25	19701.539	19705.287	322.631
WT24	542	19502.16	19655.07	323.23
WT25	488.1	19902.16	19708.7	318.17
WT26	243.5	19745.5	20007.7	323.67
WT27	149.4	19748.776	19980.227	323.179
WT29	159	19840.141	19984.725	322.106
WT3	241.9	19613.2	20020.1	325.03
WT30	165.3	19800	19985	323
WT31	279	19841.097	20044.585	323.1
WT32	261.4	19800.13	19799.758	320.369
WT33	90	19801.034	19759.991	320.135
WT33A	339.3	19801.052	19757.949	320.147
WT34	96	19760	19835	323
WT34A	188.7	19760	19830.5	323
WT35	321	19760.567	20065.388	324.021
WT36	195.2	19722.655	19989.284	324.002
WT37	258.7	19648.622	19794.103	323.222
WT38	233.6	19648.69	19797.811	323.211
WT39	312.7	19648.375	19790.711	323.095
WT40	60	19642.702	19790.994	323.403
WT41	306.6	19641.841	19792.297	323.379
WT42	267.5	19640.082	19796.063	323.459
WT43	249.7	19822.249	19816.496	319.524
WT44	225.4	19821.213	19819.062	319.492

HOLE_ID	HOLE_DEPTH	LOCAL_EAST	LOCAL_NORTH	RL
WT45	318.5	19821.748	19814.162	319.509
WT46	48	19834.239	19839.219	319.546
WT47	207.5	19834.645	19841.193	319.574
WT48	365.5	19716.961	19755.581	321.823
WT49	414.3	19505.669	19704.926	323.567
WT5	235.6	19799.43	19823.57	321.01
WT50	366.5	19506.188	19707.975	323.788
WT51	195.5	19448.816	19761.42	324.039
WT52	219.8	19448.921	19758.983	324.151
WT53	246.7	19448.997	19757.557	324.015
WT54	171.4	19450.477	19766.637	324.086
WT55	174.1	19447.367	19742.247	324.01
WT56	183.5	19684.652	19834.33	323.522
WT57	370.7	19836.882	19839.606	319.535
WT58	246.7	19375.216	19766.53	324.015
WT59	201.6	19374.955	19768.409	324.054
WT6	185.3	19373.66	19809.99	324.11
WT60	183.5	19375.025	19770.626	324.035
WT61	288.5	19300.537	19748.992	323.671
WT62	252.6	19300.435	19749.304	323.7
WT63	267.5	19687.19	19822.226	323.335
WT64	186.2	19685.86	19822.734	323.214
WT65	173.9	19685.435	19824.005	323.345
WT66	189.5	19628.125	19811.054	323.782
WT67	234.3	19628.071	19809.702	323.772
WT68	213.5	19626.37	19811.077	323.811
WT69	216.4	19712.381	19813.82	323.074
WT7	214.6	19990.4	19989.5	320.7
WT70	150	19712.004	19812.28	323.044
WT71	357.5	19283.388	19716.881	323.399
WT72	351.1	19581.108	19744.539	323.569
WT73	285.4	19642.779	19755.877	323.163
WT74	76.2	19533.917	19711.605	323.566
WT75	253	19760.362	19825.96	322.666
WT76	53.4	19352.699	19639.557	323.19
WT77	92	19641.298	19755.824	323.129
WT78	240.5	19760.76	19830.304	322.783
WT79	132.4	19703.003	19869.932	323.41
WT8	224	19897.7	19840.4	319.06
WT80	157.6	19718.558	19869.653	323.072
WT81	180.1	19760.742	19831.396	322.81
WT82	125.3	19718.545	19870.058	323.139

HOLE_ID	HOLE_DEPTH	LOCAL_EAST	LOCAL_NORTH	RL
WT83	102	19697.164	19790.261	322.271
WT84	119.5	19770.406	19949.817	322.093
WT85	249.5	19697.229	19788.617	322.235
WT86	79.1	19770.308	19950.471	322.085
WT87	127.8	19804.407	19969.753	321.832
WT88	146.5	19516.108	19822.432	324.238
WT89	114	19837.017	19842.527	319.571
WT8A	250.15	19897.7	19840.4	319.06
WT9	124.5	19799.96	20025.17	323.09
WT9A	270.5	19799.96	20025.17	323.09
WTRC1	72	19698.58	19939.74	323.47
WTRC10	112	19601.14	19919.4	324.62
WTRC11	76	19600.87	19900.17	324.55
WTRC12	70	19650	19900	323.93
WTRC13	112	19498.76	19892.48	324.54
WTRC2	78	19750	19930	322.3
WTRC3	96	19748.463	19950.124	322.692
WTRC4	54	19800	19930	321.14
WTRC5	102	19798.38	19959.83	321.58
WTRC6	54	19848.498	19929.057	321.212
WTRC7	102	19850	19960	321.34
WTRC8	84	19898.77	19939.77	321.06
WTRC9	100	19650	19920	324.01

RedRiver
RESOURCES LIMITED

ACN 100 796 754

APPENDIX 2

WATERLOO– DOWNHOLE SURVEY TABLES

HOLE_ID	DEPTH	GRID_AZ	DIP
WT1	92	3.5	-65
WT10	0	359.5	-72
WT10	34	358	-72.3
WT10	70	357	-73.5
WT10	86	357	-73.7
WT10	107	356	-70.7
WT10	128	352.3	-67
WT10	161	349	-57.8
WT10	191	349	-55.5
WT10	214.05	349	-56
WT11	0	179.5	-60
WT11	41	177.3	-60.7
WT11	85.4	175	-61
WT12	0	359.5	-74
WT12	30	0.3	-74
WT12	60	1.3	-74.6
WT12	90	2	-75.8
WT12	120	357	-74
WT12	150	353.5	-72
WT12	180	350	-68.5
WT12	210	346	-65.3
WT12	240	345	-59.8
WT12	270	346	-58.3
WT12	299.7	342	-59
WT13	0	359.5	-64
WT13	30	359.4	-64
WT13	60	356.3	-64.2
WT13	90	356.1	-64
WT13	119	356	-63.3
WT13	149	356	-63
WT13	180	356	-63
WT13	210	356	-63.9
WT13	240	354	-63
WT13	288.3	352	-61.7
WT14	0	180.5	-55
WT14	30	180.7	-54.1
WT14	50	180.8	-54.9
WT14	70	180.9	-55.6
WT14	90	181	-56.2

HOLE_ID	DEPTH	GRID_AZ	DIP
WT14	110	181	-55.93
WT14	130	180.7	-55.86
WT14	150	180	-55.99
WT14	166.2	179.5	-56.1
WT15	0	180.5	-53
WT15	20	180.2	-53.33
WT15	40	180.6	-53.95
WT15	50	181.2	-54.41
WT15	60	181.8	-54.86
WT15	70	182	-55.26
WT15	80	182	-55.63
WT15	90	182	-56
WT15	100	182	-56.37
WT15	102.5	182	-56.46
WT16	0	180.5	-55
WT16	40	176	-54.87
WT16	80	179.9	-55.59
WT16	110	181.6	-55.32
WT16	150	183.5	-53.36
WT16	200	183.7	-52.75
WT16	240	184	-52.51
WT16	280	183.7	-52.14
WT16	330	182	-52.68
WT16	358.25	183.5	-51.99
WT17	0	180.5	-60
WT17	20	180.4	-60.67
WT17	50	180.2	-61.13
WT17	80	180.1	-61.4
WT17	110	180	-61.3
WT17	130	178.9	-61.3
WT17	147.5	177	-60
WT18	0	180.5	-63
WT18	40	181.2	-62.73
WT18	70	181.7	-62.4
WT18	100	182	-62.8
WT18	140	180.7	-62.8
WT18	180	180	-62
WT18	220	179	-61.67
WT18	260	179	-60.2
WT18	300	179	-59.9
WT18	337.4	179	-58.65
WT19	0	180.5	-55

HOLE_ID	DEPTH	GRID_AZ	DIP
WT19	30	181.2	-55
WT19	50	181.5	-55.48
WT19	80	181.9	-56.37
WT19	110	182	-57.02
WT19	140	181.4	-57.2
WT19	170	181	-56.57
WT19	189	181	-55.93
WT1A	0	3.5	-65
WT1A	10	3	-65.42
WT1A	20	2.9	-65.83
WT1A	30	2.9	-66.25
WT1A	40	2.9	-66.67
WT1A	50	2.8	-67.08
WT1A	60	2.8	-67.5
WT1A	70	2.8	-67.92
WT1A	80	3.3	-64
WT1A	90	3.8	-66.11
WT1A	100	4.4	-66.19
WT1A	103	3.5	-66
WT1A	110	358.5	-65.49
WT1A	120	357.9	-64.75
WT1A	123.5	357.6	-64.5
WT2	0	3.5	-62
WT2	20	2.5	-62
WT2	40	1.5	-62.25
WT2	60	0.5	-62.5
WT2	77.5	0.5	-62.75
WT2	102	360	-62.75
WT2	120	360	-59
WT2	140	359.5	-58
WT2	169.5	1.5	-54.75
WT2	199.5	357.5	-51.75
WT2	229.5	356.5	-51.5
WT2	259.5	356.5	-50.25
WT2	290	355.5	-47
WT2	320	356	-45
WT2	350	353.5	-43.8
WT2	380	353.5	-42.4
WT2	410	356.5	-41
WT2	440	349.5	-38.75
WT2	475.55	340.5	-36.5
WT20	0	180.5	-55

HOLE_ID	DEPTH	GRID_AZ	DIP
WT20	20	180.5	-55.6
WT20	40	180.5	-55.8
WT20	60	180.5	-55.6
WT20	80	180.5	-56
WT20	110	180.2	-55.2
WT20	140	179	-53.8
WT20	170	177.5	-52.45
WT20	190	176.5	-51.55
WT20	207.5	175.6	-50.76
WT21	0	180.5	-55
WT21	32	180.7	-55
WT21	62	180.8	-55
WT21	91	181	-55.8
WT21	121	180	-56.8
WT21	151	180	-55.5
WT21	181	181	-55.1
WT21	211	179	-54.5
WT21	241	180	-53.2
WT21	271	179	-51
WT21	301	179	-50
WT21	340.6	181	-48.3
WT22	0	180.5	-55
WT22	33	180.6	-54.9
WT22	63	180.8	-54.9
WT22	90	180.9	-55.2
WT22	121	181	-55
WT22	151	181	-54
WT22	181	180	-53.5
WT22	211	180	-52
WT22	241	180.5	-50
WT22	271	179	-48.1
WT22	301	179	-48.1
WT22	333.5	179	-45
WT23	0	360	-69
WT23	33	360	-68.25
WT23	63	360	-68.75
WT23	93	360	-68.7
WT23	122	359	-69
WT23	152	359	-69.3
WT23	158	358.5	-66.3
WT23	170	357	-65
WT23	200	353	-64.7

HOLE_ID	DEPTH	GRID_AZ	DIP
WT23	230	352.5	-61
WT23	245	353	-60.5
WT23	260	352.5	-59.3
WT23	290	352.5	-58.9
WT23	320	353.5	-56.7
WT23	350	347	-53.9
WT23	380	348	-48.3
WT23	410	349	-44.8
WT23	440	348.5	-41.4
WT23	470	348.5	-39.9
WT23	509.25	347	-38
WT24	0	360	-67
WT24	33	360	-66.3
WT24	63	360	-67
WT24	92	360	-66
WT24	122	358.5	-65.8
WT24	152	357.6	-63.1
WT24	182	356	-62
WT24	212	356	-61
WT24	242	355.8	-60.8
WT24	272	357	-59.7
WT24	302	356	-59
WT24	332	357	-58.9
WT24	362	356.5	-57
WT24	392	357	-56.3
WT24	422	357	-56
WT24	452	357	-54.1
WT24	482	357.5	-53
WT24	512	358.5	-51.4
WT24	542	359	-50.9
WT25	0	355	-67
WT25	29	355	-67.1
WT25	59	355	-67.9
WT25	89	355	-69.7
WT25	119	359	-70
WT25	149	359.5	-70
WT25	179	359	-69
WT25	194	359	-67.9
WT25	224	358.5	-66.3
WT25	254	360	-66
WT25	284	359	-65.6
WT25	314	359	-64.1

HOLE_ID	DEPTH	GRID_AZ	DIP
WT25	344	359	-56.5
WT25	374	358.5	-50.4
WT25	404	357	-48.9
WT25	434	355	-46.9
WT25	488.1	355	-44.9
WT26	0	180.5	-63
WT26	30	180.5	-63
WT26	60	180.5	-62
WT26	75	180.5	-62
WT26	105	181	-61
WT26	126	181	-60.8
WT26	147	182	-60
WT26	159	182	-59.7
WT26	180	182	-59.3
WT26	210	182	-59.5
WT26	243.5	181	-59
WT27	0	180	-60
WT27	48	180	-56.7
WT27	96	180	-55
WT27	149.4	182	-55
WT29	0	180	-62
WT29	30	179	-61
WT29	60	177.5	-61.1
WT29	90	178	-61.1
WT29	120	178	-62.1
WT29	159	178	-62.4
WT3	0	183.5	-50
WT3	73	185.5	-52
WT3	103	183.5	-52
WT3	133	183.5	-50.3
WT3	163	182.5	-48
WT3	193	183.5	-45.7
WT3	223	181.5	-43
WT3	241.9	181.5	-43
WT30	0	180	-61
WT30	6	177	-61.8
WT30	30	179.5	-61.8
WT30	60	177.5	-62
WT30	87.3	177	-62
WT30	116.5	177.5	-61
WT30	147.3	179	-62
WT30	165.3	179.5	-60.2

HOLE_ID	DEPTH	GRID_AZ	DIP
WT31	0	184	-60
WT31	30	183.5	-59.8
WT31	60	186	-60.4
WT31	90	189.5	-60.7
WT31	117	190	-60.2
WT31	150	192	-59.4
WT31	180	192	-58.4
WT31	210	191.5	-57
WT31	249	193	-56.5
WT31	279	192	-56.3
WT32	0	360	-58
WT32	12	358	-59
WT32	22.8	358	-59
WT32	82.9	357.5	-59.8
WT32	120.1	357	-59.5
WT32	155.8	356.5	-58.9
WT32	180	354	-58.9
WT32	216.4	354	-57.1
WT32	261.4	353	-57.5
WT33	0	360	-58
WT33	6	359	-59.1
WT33	30	359.5	-57.1
WT33	60	358	-57
WT33	90	359.5	-55.3
WT33A	0	360	-61
WT33A	6	358.5	-62.2
WT33A	30	359.5	-62.1
WT33A	60	360	-62.3
WT33A	90	359	-61
WT33A	104.9	0.5	-60.3
WT33A	125.9	360	-59.5
WT33A	162.3	359	-58
WT33A	192.3	358	-56.3
WT33A	222.3	357	-56
WT33A	252.3	357	-54.9
WT33A	281.9	356	-53.9
WT33A	314.7	356	-54
WT33A	339.3	355	-54.5
WT34	0	360	-60
WT34	6	360	-59.5
WT34	30	359	-60
WT34	60	358	-60.7

HOLE_ID	DEPTH	GRID_AZ	DIP
WT34	90	358	-58.2
WT34A	0	360	-59
WT34A	6	360	-59.7
WT34A	24	359.5	-59.5
WT34A	75	358	-59.6
WT34A	150.4	354.5	-57.9
WT34A	188.7	354	-57.2
HOLE_ID	DEPTH	GRID_AZ	DIP
WT35	0	180	-60
WT35	31	182	-60.2
WT35	61	182.5	-60
WT35	79	183	-60
WT35	90	182.5	-59.8
WT35	119.8	182	-57
WT35	141	183	-57
WT35	176.6	183	-56.2
WT35	209.4	183	-55.9
WT35	240	183.5	-54.9
WT35	270	184	-54.7
WT35	312	184	-53.9
WT36	0	180	-62
WT36	25	180	-62.2
WT36	43	181.8	-61
WT36	61	183	-60
WT36	84	180.5	-60.7
WT36	90.7	183.5	-60.8
WT36	114.7	183.5	-60.2
WT36	123.7	184	-59.5
WT36	153.2	185	-59.5
WT36	183.2	185	-60
WT37	18	4.1	-65.6
WT37	30	5.3	-65.6
WT37	60	6.5	-64.5
WT37	90	5.6	-63.1
WT37	102	4.9	-62.4
WT37	120	3.95	-61.5
WT37	150.2	8.43	-60.4
WT37	180	2.34	-60
WT37	213	6.7	-59.5
WT37	243	1.44	-60.4
WT38	18	4.2	-62.5
WT38	30	4.8	-62.4

HOLE_ID	DEPTH	GRID_AZ	DIP
WT38	60	5	-61.9
WT38	90	7.5	-61.4
WT38	108	5.3	-60.5
WT38	120	5.2	-59.6
WT38	129	5.7	-57.8
WT38	150	11.9	-55.7
WT38	180	12.3	-54.7
WT38	210	12.3	-54.4
WT38	233.6	5.4	-54.6
WT39	18	0.9	-70
WT39	30	0.5	-69.3
WT39	60	357.7	-68.1
WT39	90	5.7	-65.2
WT39	102	5.5	-64
WT39	120	7.17	-64.2
WT39	129.4	7.17	-64.2
WT39	150	2.2	-64.25
WT39	180	2.35	-64.14
WT39	210	2.18	-63.9
WT39	240	2.88	-63.63
WT39	270	1.92	-63.87
WT39	300	6.23	-63.26
WT40	15	333.7	-72
WT40	28	333.8	-72.6
WT40	57	333	-75.2
WT41	15	333.6	-70.7
WT41	27	332.8	-70.9
WT41	57	329.37	-70.2
WT41	75	332.62	-70.1
WT41	93	334.62	-69.5
WT41	105	337.21	-69
WT41	117	339.53	-69
WT41	129	339.85	-69.1
WT41	144.4	339.8	-68.5
WT41	153.6	343.17	-68.2
WT41	171.6	341.3	-66.1
WT41	189	343.74	-64.9
WT41	201.6	342.71	-63.7
WT41	219.6	345.9	-61.4
WT41	237	343.92	-59.6
WT41	270	348.95	-59.6
WT41	294	344.64	-60.2

HOLE_ID	DEPTH	GRID_AZ	DIP
WT42	18	338.01	-67.9
WT42	30	333.4	-66.5
WT42	60	335.7	-64.1
WT42	78	331.8	-63.8
WT42	96	335.5	-63.1
WT42	114	338.4	-61.1
WT42	129	335.9	-61
WT42	159	336.1	-61.1
WT42	189	332.8	-61.2
WT42	219	334.8	-61.2
WT42	264.5	332.79	-61.4
WT43	18	357.5	-63.2
WT43	30	355.7	-62.7
WT43	60	359.1	-62.4
WT43	90	6.8	-62.7
WT43	120	10.1	-57.5
WT43	132	10.9	-54.3
WT43	150	15.8	-53
WT43	186	13.5	-52.4
WT43	216	14.4	-52.05
WT43	243.7	13.4	-52.7
WT44	18	25.5	-51.5
WT44	30	23.4	-51
WT44	48	23.7	-53
WT44	66	25.1	-56.1
WT44	90	27.1	-55.5
WT44	120	29.3	-54.5
WT44	150	28	-50.5
WT44	225.4	24.6	-46.6
WT45	60	6.7	-67.5
WT45	90	11.5	-69.7
WT45	120	10.7	-69.4
WT45	150	15	-68.1
WT45	165	14.5	-67.6
WT45	195	13.2	-67.4
WT45	225	14.4	-67
WT45	255	12.9	-67.3
WT45	285	14	-67.3
WT45	315	12	-67.9
WT46	15	14.6	-62.8
WT46	27	13.3	-64.4
WT46	45	13.4	-67.2

HOLE_ID	DEPTH	GRID_AZ	DIP
WT47	15	9	-56.3
WT47	27	12.3	-57.6
WT47	60	11.9	-63
WT47	72	15.2	-63.5
WT47	90	18.9	-63
WT47	102	19.1	-61
WT47	120	19.7	-57.1
WT47	138	20.7	-52.5
WT47	156.5	20.6	-51.8
WT47	183.5	20.74	-52.7
WT47	207.5	18	-52.8
WT48	18	8	-65.8
WT48	30	9.1	-66.5
WT48	60	8.5	-66.7
WT48	96	9	-64
WT48	114	11.2	-60.7
WT48	135	9.5	-59.4
WT48	147	12.5	-59.1
WT48	180	9.5	-58.1
WT48	210	8.5	-55.1
WT48	240	7.3	-55.3
WT48	270	6.2	-55.1
WT48	300	4.4	-52.5
WT48	330	5.1	-53.29
WT48	360	1	-53.7
WT49	18	18.2	-64.4
WT49	30	17.7	-65
WT49	60	17.7	-63.6
WT49	90	20.3	-63.5
WT49	120	17.4	-64
WT49	150	15.3	-62.2
WT49	168	18	-63
WT49	180.4	16.1	-63
WT49	210.4	16.1	-61.7
WT49	239.4	17.73	-61
WT49	270	15.78	-60.2
WT49	300.3	17	-58
WT49	330	15.94	-56.5
WT49	360.3	16.3	-54.6
WT49	390.3	17.9	-53.3
WT49	414.3	19.95	-52.1
WT5	0	359.5	-60

HOLE_ID	DEPTH	GRID_AZ	DIP
WT5	30	359	-59.5
WT5	60	358.5	-60
WT5	90	358	-61
WT5	130	357	-60
WT5	160	356	-51.5
WT5	190	354.4	-45.8
WT5	235.6	352	-41.8
WT50	18	13.56	-62.57
WT50	30	13.82	-63
WT50	60	16.48	-62.5
WT50	90	14.98	-62.3
WT50	102	15.4	-61.5
WT50	117	15.9	-57.6
WT50	138	13.29	-59
WT50	150	12.83	-57.2
WT50	168	12.4	-55.9
WT50	180.5	13.18	-55.8
WT50	210.5	12.98	-54.9
WT50	240.5	14.8	-54.3
WT50	270	14.88	-52.3
WT50	312.5	12	-51.1
WT50	330	14.75	-51
WT50	360	15.71	-51.2
WT51	15	358.94	-58.9
WT51	27	358.55	-58.1
WT51	42	357.5	-57.2
WT51	60	359	-57.1
WT51	72	3.1	-57.2
WT51	84	1.2	-57.5
WT51	96	2.8	-56.9
WT51	120	4.4	-57
WT51	150	2.7	-57.1
WT51	180	2.8	-57.6
WT51	195.5	3.1	-57.6
WT52	18	0.8	-68
WT52	30	359.7	-68
WT52	60	0.3	-66
WT52	90	0.1	-64.8
WT52	102	1.2	-62.7
WT52	114	5.1	-60.3
WT52	120	5.2	-59.8
WT52	150	4.8	-58.8

HOLE_ID	DEPTH	GRID_AZ	DIP
WT52	180	3.2	-58.2
WT52	219	2.4	-57.4
WT53	18	2.7	-70.8
WT53	30	0.4	-71.3
WT53	45	359.3	-71.6
WT53	60	2.4	-71.2
WT53	78	1.9	-71.3
WT53	96	7.1	-68.8
WT53	114	7	-68
WT53	132	6.6	-67.3
WT53	150	4.5	-66.9
WT53	180	6.1	-62.5
WT53	210	5.9	-61.1
WT53	243.7	5.8	-59.7
WT54	15	358.11	-53
WT54	27	357.93	-52.6
WT54	48	0.9	-53.2
WT54	66	2.3	-53.9
WT54	84	7	-50.8
WT54	102	9.7	-46.7
WT54	120	9.9	-46.4
WT54	150	10.4	-46.5
WT54	168	11.6	-46.7
WT54	171.4	9.99	-46.7
WT55	18	337.1	-63.2
WT55	36	335.8	-62.5
WT55	60	335.5	-61
WT55	90	337	-58.2
WT55	105	342.35	-55.8
WT55	132	344.61	-54.5
WT55	162.2	344.5	-54.4
WT56	18	353	-62
WT56	30	352.8	-62.3
WT56	60	354.49	-66.1
WT56	78	1	-64.1
WT56	90	7	-62.2
WT56	106	14.3	-59.7
WT56	117	17.2	-56.9
WT56	129	19.2	-54.3
WT56	153	19.35	-52.9
WT56	183.5	18.3	-53.6
WT57	15	3.6	-80.8

HOLE_ID	DEPTH	GRID_AZ	DIP
WT57	27	0.9	-80.2
WT57	57	355.2	-79.9
WT57	87	357.9	-78.9
WT57	117	0.2	-76.6
WT57	135	359.1	-76
WT57	153	357.7	-75.3
WT57	159	359.5	-75.2
WT57	165	0.7	-74.8
WT57	183.7	1.7	-74
WT57	210.7	0.2	-74.1
WT57	240	0.3	-74
WT57	270.7	359.2	-73.9
WT57	300	356.9	-73.5
WT57	330	357.9	-72.3
WT57	360	354.4	-72.3
WT57	369.7	356.1	-72.5
WT58	15	0.6	-64
WT58	27	359.3	-63.1
WT58	60	357.5	-60.1
WT58	72	357.6	-60.7
WT58	90	359.3	-60.1
WT58	108	0.9	-59.7
WT58	120	0.2	-58.9
WT58	132	359.1	-58.6
WT58	180	359.1	-58
WT58	210	359.2	-58.1
WT58	240	359.5	-58
WT59	18	357.5	-61.2
WT59	30	0.9	-61
WT59	60	358.9	-59
WT59	90	1.9	-57
WT59	102	3.6	-55.1
WT59	114	3.2	-53.4
WT59	144.6	2.9	-52.5
WT59	180	2.7	-53
WT59	201	3.4	-53.1
WT6	0	359.5	-60
WT6	34	359.5	-59
WT6	94	359.8	-59.7
WT6	124	360	-60
WT6	154	1	-58.2
WT6	185.3	1	-55.6

HOLE_ID	DEPTH	GRID_AZ	DIP
WT60	18	3.6	-51.2
WT60	30	4.2	-51.2
WT60	48	2.1	-50.3
WT60	54	2.8	-50
WT60	60	2.8	-50.1
WT60	90	1	-50
WT60	120	1	-50.1
WT60	150	1.3	-50.3
WT60	180	1.5	-50.4
WT61	18	341.6	-74.2
WT61	30	340.1	-73.9
WT61	60	340.1	-72.9
WT61	90	335.9	-71
WT61	120	342.5	-70.2
WT61	132	346.8	-67.3
WT61	150	347.7	-64.5
WT61	180.5	348	-63.4
WT61	210	349	-60.7
WT61	240	348.6	-57.5
WT61	270	349	-55.7
WT61	288.5	349.2	-54.4
WT62	18	338.2	-69.3
WT62	27	340.6	-69
WT62	39	340.4	-67.9
WT62	90	342.6	-68.4
WT62	102	342.6	-68.4
WT62	120	350	-65.9
WT62	132	354.2	-63.8
WT62	162	357	-60.5
WT62	192.6	356.8	-58.4
WT62	222.6	357.4	-57
WT62	252.6	358.2	-55.7
WT63	15	355.2	-73.6
WT63	27	353.8	-74
WT63	57	353.3	-75.5
WT63	87	353.7	-75.6
WT63	99	352.7	-74.6
WT63	117	353.2	-71.5
WT63	129	353.4	-70.4
WT63	144	356.8	-68.9
WT63	174	350.3	-64
WT63	192	350.7	-62

HOLE_ID	DEPTH	GRID_AZ	DIP
WT63	220	351.3	-60.1
WT63	249.5	352.1	-59.1
WT63	267.5	352.2	-58.3
WT64	15	340.7	-60.3
WT64	27	340.6	-60.8
WT64	57	343.4	-63.3
WT64	87	346.3	-64.7
WT64	102	352.2	-62.9
WT64	114	355.8	-61.2
WT64	126	357.5	-58.9
WT64	150	358.8	-57.7
WT64	180	358.5	-57.7
WT65	15	338.8	-51.6
WT65	27	340.4	-52.8
WT65	57	340.7	-56
WT65	87	344	-55.9
WT65	99	348.2	-53.4
WT65	129.4	353.1	-49.5
WT65	160	353	-49.9
WT65	174.4	353.8	-49.1
WT66	15	3.9	-53.4
WT66	27	4.5	-53.5
WT66	60	7	-54.1
WT66	87	5.7	-54.9
WT66	100	6.5	-53.6
WT66	135.5	5.4	-54.1
WT66	165.5	5.5	-54.1
WT66	186.5	5	-54.1
WT67	18	1.4	-69.8
WT67	30	1.1	-69.4
WT67	60	359.3	-66.2
WT67	78	0.4	-65.1
WT67	90	0.8	-65
WT67	100	1.5	-64.4
WT67	132.5	2.9	-63.9
WT67	179.3	2.6	-62.8
WT67	201.3	1.8	-62.3
WT67	234.3	1.1	-62.8
WT68	15	5.4	-63
WT68	27	7.1	-62.7
WT68	57	5.8	-60.4
WT68	87	9.7	-59.8

HOLE_ID	DEPTH	GRID_AZ	DIP
WT68	117	15.3	-59
WT68	150.5	16.9	-59.1
WT68	180.5	18.1	-59.6
WT68	210.5	16.7	-59.8
WT69	18	2.9	-60.2
WT69	30	0.9	-59.5
WT69	60	2.3	-61.9
WT69	90	2.7	-59.6
WT69	108	1.3	-58
WT69	123	2.6	-56.9
WT69	135	5.3	-55.6
WT69	171.5	5.4	-53.7
WT69	201.5	5.4	-54.2
WT69	216	5.8	-54.2
WT7	0	179.5	-63
WT7	40	180.2	-62
WT7	80	180.8	-63
WT7	115	181.4	-63.2
WT7	145	182	-64
WT7	184	192	-64.8
WT7	214.6	192	-63
WT70	18	359.7	-67.1
WT70	30	358.9	-66.7
WT70	60	358.5	-67.8
WT70	90	2.2	-66.4
WT70	120	4.5	-62.8
WT70	132	6.2	-62.2
WT70	138	6.2	-61.4
WT70	150	11.5	-58
WT71	18	355.9	-76.1
WT71	30	354.2	-75.5
WT71	88	358	-74
WT71	99.3	1.7	-74.5
WT71	129.3	1.6	-74
WT71	159.1	2.8	-71.2
WT71	189.5	2.3	-68.5
WT71	219.4	1.8	-66.1
WT71	249.4	2.1	-64.6
WT71	281.4	2.6	-62.9
WT71	312.5	2.2	-61.4
WT71	342.5	2.8	-57.9
WT71	357.5	2.8	-56.2

HOLE_ID	DEPTH	GRID_AZ	DIP
WT72	18	357.8	-64.9
WT72	30	355.8	-64.2
WT72	60	358.2	-63.3
WT72	82.5	359	-63
WT72	144.6	1.6	-63.5
WT72	150.6	1.1	-63.3
WT72	180.6	0.3	-62.4
WT72	210.6	0.7	-61.4
WT72	240.6	0.7	-60.4
WT72	270.6	1.3	-58.7
WT72	300.6	0.2	-58.5
WT72	330.6	1.2	-58.1
WT72	351.1	1.9	-58.2
WT73	16.5	349.3	-61.4
WT73	28.5	348.7	-61.3
WT73	60	347.9	-60.5
WT73	90	349.2	-57
WT73	102	350.3	-55.7
WT73	123.4	352.7	-55.2
WT73	150.4	353.6	-55.1
WT73	183.4	352	-54.9
WT73	212.9	352.9	-54.3
WT73	243.4	352.4	-53.5
WT73	270.4	353.7	-53.3
WT73	285.4	354.2	-53.6
WT74	15	159.1	-89.8
WT74	30	239.6	-89.6
WT74	60	197.2	-89.9
WT75	18	358.2	-70.5
WT75	30	359.9	-69.9
WT75	60	358.7	-69.2
WT75	90	360	-70.6
WT75	101	0.5	-70.5
WT75	120	359.9	-68.9
WT75	132	1.4	-65.6
WT75	150.7	4.2	-63.8
WT75	180.7	5.9	-63
WT75	210.7	5.4	-62.9
WT75	240.7	5.7	-63.1
WT76	15	109.3	-89.8
WT76	30	343.2	-89.7
WT76	50	330.8	-89.6

HOLE_ID	DEPTH	GRID_AZ	DIP
WT77	15	321.3	-89.5
WT77	30	198.8	-89.7
WT77	45	90.2	-89.9
WT77	60	346.2	-89.6
WT77	75	295.4	-89.7
WT77	90	98	-89.5
WT78	18	3.3	-65.3
WT78	30	3.9	-65.2
WT78	60	2.9	-64.3
WT78	90	6.7	-64.5
WT78	102	7.7	-63.6
WT78	114	11	-61.4
WT78	141.5	12.3	-61.2
WT78	174.5	11.9	-60.7
WT78	201.5	12.7	-60.9
WT78	234.5	9.9	-61.4
WT79	15	183.3	-89.3
WT79	30	114.3	-89.2
WT79	60	50.2	-89.1
WT79	90	30.9	-88.8
WT79	120	46.2	-89
WT8	0	359.5	-72
WT8	68	359.2	-73
WT8	80	359	-71.7
WT8	110	359	-64.2
WT8	140	354	-63
WT8	170	351	-56.5
WT8	200	350	-56.5
WT8	224	349	-55
WT80	9	6	-64.9
WT80	30	6	-64.4
WT80	81	6.9	-65.8
WT80	90	6.6	-65.9
WT80	104	7.3	-66
WT80	120	7.6	-65.8
WT80	154	6.8	-65.2
WT81	18	0.4	-57.2
WT81	30	358.9	-57.1
WT81	60	356.4	-55
WT81	72	358.9	-54.9
WT81	90.5	358.5	-54.5
WT81	120.5	359	-54.7

HOLE_ID	DEPTH	GRID_AZ	DIP
WT81	150.5	358.4	-55.1
WT81	180.1	357.5	-55
WT82	15	7	-55.2
WT82	30	5	-54.9
WT82	65	3.2	-55.7
WT82	90	3.8	-55.7
WT82	120	4.6	-56.2
WT83	18	5.7	-60.9
WT83	30	5.5	-59.3
WT83	60	357.4	-60
WT83	90	0.4	-56.5
WT83	102	0.7	-55.5
WT84	30	170	-64.4
WT84	60	169	-64.4
WT84	90	168.3	-65.6
WT84	115	167.7	-65.7
WT85	18	6.4	-64.6
WT85	30	4.5	-64
WT85	60	4.2	-62.2
WT85	90	5.6	-60.7
WT85	105.5	3.8	-60.6
WT85	120	5.4	-60.2
WT85	150.5	0.2	-54.1
WT85	180.5	359.8	-53.7
WT85	210.5	1.6	-52.9
WT85	231.5	1.4	-52.8
WT85	249.5	0.7	-52.5
WT86	50	177.2	-50.8
WT86	75	175.3	-51.9
WT87	30	181	-62
WT87	79	185	-62.9
WT87	90	185.4	-63
WT87	120	185.3	-63.5
WT88	30	2	-68.4
WT88	60	7	-67.4
WT88	90	13.6	-59.8
WT88	120	12.4	-60.1
WT88	145	11.3	-59.9
WT89	18	355.8	-62.3
WT89	30	356.1	-61.8
WT89	60	358.5	-63.4
WT89	90	3.7	-63.9

HOLE_ID	DEPTH	GRID_AZ	DIP
WT89	108	4.6	-62.6
WT89	114	5.5	-61.1
WT8A	0	359.5	-72
WT8A	68	359.2	-73
WT8A	90	3	-73.2
WT8A	121	2	-72
WT8A	151	359	-70.7
WT8A	166	360	-70
WT8A	174	1	-71
WT8A	199	0.5	-69.3
WT8A	250.15	360	-68.4
WT9	124.5	179.5	-68
WT9A	0	179.5	-68
WT9A	85	181	-67
WT9A	96	182	-66
WT9A	114	183	-65
WT9A	138	186	-62.2
WT9A	162	188	-60.2
WT9A	192	189	-57.7
WT9A	222	188	-56.1
WT9A	270.5	188	-56
WTRC1	0	180	-60
WTRC10	0	180	-65
WTRC11	0	180	-60
WTRC12	0	180	-65
WTRC13	0	180	-65
WTRC2	0	180	-60
WTRC3	0	180	-60
WTRC4	0	180	-60
WTRC5	0	180	-60
WTRC6	0	180	-60
WTRC7	0	180	-60
WTRC8	0	180	-60
WTRC9	0	180	-65

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APPENDIX 3

WATERLOO – ORE INTERVALS TABLE

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WTRC7	72	75	0.04	2.62	0.02	11	0.59		3.74
WTRC7	75	78	0.03	0.99	0.02	16	0.3		2.31
WTRC5	84	87	5.51	9.6	18.6	446	2.95		81.63
WTRC5	87	90	0.19	0.51	0.25	64	0.66		6.29
WTRC5	81	84	0.17	0.91	0.23	34	0.99		5.17
WTRC5	78	81	0.06	0.33	0.05	16	0.81		2.71
WTRC5	90	93	0.11	0.28	0.19	14	0.59		2.60
WTRC4	27	30	0.08	0.53	0.02	1	0.79		2.00
WTRC3	72	75	1.44	0.89	3.71	38	0.41		13.70
WTRC3	75	78	0.5	0.39	0.39	39	0.43		5.89
WTRC3	78	81	0.44	0.31	0.44	15	0.21		3.85
WTRC2	24	27	0.92	4.6	0.03	15	11.2		24.93
WTRC2	27	30	0.24	2.08	0.01	9	0.98		4.65
WTRC2	21	24	0.1	1.03	0.01	10	0.33		2.33
WTRC1	51	54	0.12	3.69	0.06	5	4.41		10.18
WTRC1	54	57	0.07	1.83	0.04	4	1.53		4.24
WTRC1	57	60	0.05	1.91	0.04	5	1.5		4.22
WTRC1	48	51	0.06	0.61	0.05	5	0.9		2.40
WT9A	242.85	243	7.94	4.79	17.3	241	38.9	4.01	127.65
WT9A	245	246	3.54	3.72	22.6	59	1.18	3.97	46.52
WT9A	246	247	2.01	3.69	23.3	80	1.63	4.1	42.29
WT9A	244	245	3.08	1.68	21.5	37	0.58	3.94	39.60
WT9A	247	247.3	3.3	1.93	18.1	51	0.3	3.6	37.80
WT9A	239	239.4	1.92	0.24	10.8	30	1.72	3.23	23.86
WT9A	243	244	1.77	4.44	2.82	14	1.39	3.98	17.00
WT9A	242	242.85	0.76	1.45	3.04	17	1.11	2.98	10.19
WT9A	239.4	240	0.33	0.01	2.77	13	2.22	3.02	8.27
WT9A	240	241	0.28	0.02	3.76	11	0.3	3.27	6.12
WT9A	241	242	0.11	0.18	0.98	16	1.25	3.18	4.39
WT9A	238	239	0.16	0.28	0.67	9	0.17		2.39
WT88	112.8	114.2	1.29	5.06	21.7	165	0.005	3.45	41.26
WT88	118	119	0.15	0.3	2.91	3	4.1	3.39	9.98
WT88	112	112.8	0.3	0.54	2.05	30	0.17	3.31	5.85
WT88	123.85	124.6	0.47	0.04	1.37	10	0.29	3.66	4.52
WT88	110	111	0.33	0.31	0.58	14	0.19	3.25	3.41
WT88	117	118	0.09	0.28	1.93	3	0.14	3.41	2.93
WT88	114.2	115	0.2	0.32	0.94	7	0.13	3.28	2.69
WT87	93	95	0.02	0.005	0.2	71			4.55
WT87	95	97	0.02	0.005	0.14	60			3.83

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT87	115	116.2	0.21	0.66	1.73	7			3.59
WT87	97	99	0.01	0.005	0.08	48			3.01
WT86	50	51	0.07	1.77	0.02	9	8.48	3.49	14.62
WT86	46.25	47	0.25	3.25	0.02	39	5.83	4.19	14.49
WT86	47	48	0.29	2.93	0.04	20	5.95	3.81	13.48
WT86	51	52.15	0.16	3.08	0.02	9	5.33	4.07	11.43
WT86	48	49	0.11	2.5	0.02	6	2.07	3.75	5.82
WT86	49	50	0.09	1.83	0.01	13	1.79	3.4	5.21
WT86	52.15	53.2	0.09	1.77	0.01	4	1.78	3.81	4.61
WT86	43	44.2	0.01	0.08	0.02	74	0.02	2.86	4.60
WT86	44.2	45.4	0.02	0.2	0.005	41	0.03	2.91	2.75
WT85	214.4	215	7.34	0.58	7.08	225	38.2	4.25	109.54
WT85	217	218	6.6	5.09	29.7	121	0.68	4.35	71.31
WT85	218	219	7.36	3.49	23.5	131	1.27	4.33	68.73
WT85	215	216	4.96	2.36	30.6	108	3.46	4.63	66.07
WT85	219	220.05	6.63	3.16	25.1	102	1.92	4.48	66.03
WT85	216	217	7.29	1.67	19.2	87	0.56	4.69	59.04
WT85	220.05	221	0.46	0.23	0.94	21	2.08	3.25	7.47
WT84	88	89.2	9.27	1.73	40.1	337	11.5	4.35	119.79
WT84	87	88	8.85	2.04	35.2	266	7.25	4.4	102.79
WT84	85	86	14	0.71	18.8	119	2.96	4.56	93.25
WT84	86	87	6.44	1.13	42.2	151	2.99	4.39	85.22
WT84	89.2	90.4	7.71	9.92	27.8	220	1.45	4.55	85.14
WT84	84	85	6.86	2.13	38.5	161	2.26	4.47	83.70
WT84	83	84	4.74	4.35	38.4	132	0.42	4.56	71.42
WT84	81.7	83	4.91	5.32	36.2	103	0.66	4.5	69.34
WT84	90.4	90.9	1.4	1.67	7.95	92	1.84	3.28	23.69
WT84	95.5	97.05	0.54	1.07	5.73	46	0.36	3.45	12.25
WT84	92.3	93.5	0.61	0.17	2.18	22	0.66	3.06	7.32
WT84	81	81.7	0.25	0.09	0.2	59	0.42	3.05	5.54
WT84	79	80	0.02	0.09	0.09	79	0.07	2.87	5.09
WT84	93.5	94.5	0.36	0.49	1.27	20	0.3	3.15	4.89
WT84	80	81	0.005	0.05	0.05	53	0.09	2.86	3.42
WT82	90.65	91.35	3.92	7.68	25.6	106	0.87	4.57	56.63
WT82	91.35	91.85	7.35	0.16	2.97	32	5.47	4.45	45.78
WT82	93	94	2.45	2.01	9.51	67	1.14	3.82	27.67
WT82	91.85	93	2	1.1	9.16	62	0.81	3.58	23.83
WT82	90	90.65	0.45	3.65	0.42	34	0.57	3.39	8.11
WT82	88.95	90	0.1	2.32	0.22	8	2	3.89	5.85
WT82	94	95	0.24	0.1	0.21	3	0.46	3.58	2.21
WT81	140.55	141.25	7.94	0.55	6.5	133	6.94	4.14	60.45
WT81	141.25	142.25	4.57	1.12	18.2	113	3.14	4.35	50.81

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT81	142.25	143.25	4.16	1.09	22	84	0.65	4.64	47.38
WT81	139.5	140.55	0.57	0.05	1.15	21	0.71	3.04	6.03
WT81	143.25	144	0.49	0.15	0.63	16	1.24	3.58	5.70
WT81	145	146.4	0.28	0.08	1.42	5	0.14	3.24	3.23
WT81	144	145	0.18	0.05	0.6	5	0.39	3.45	2.31
WT80	120	121.16	6.55	6.3	34.9	179	3.57	4.56	84.92
WT80	115.35	116	6	7.99	33.4	78	0.43	4.58	71.62
WT80	119	120	3.52	3.07	35.5	79	0.38	4.57	58.86
WT80	118	119	6.46	1.03	9.17	100	1.97	4.69	47.65
WT80	116	117	2.79	4.23	15.9	119	1.24	4.84	40.55
WT80	117	118	3.94	1.75	11.7	101	1.98	4.82	39.57
WT80	114.7	115.35	1.09	2.43	7.73	51	0.3	3.46	17.96
WT80	121.16	122	1.82	0.17	1.77	21	1.55	3.31	13.54
WT80	122	123	0.39	0.35	3.35	6	0.06	3.12	5.81
WT80	123	124	0.35	0.35	1.8	9	0.2	3.07	4.46
WT73	246.45	247.58	6.13	2.29	18.2	73	2.62		55.51
WT73	247.58	247.95	1.04	0.08	2.02	12	0.67		8.42
WT72	338	339	11.6	0.02	0.37	13	0.12		53.08
WT72	339	340	8.79	0.005	0.38	14	0.08		40.54
WT72	337.1	338	6.42	0.02	0.05	9	0.16		29.47
WT72	329.25	330.3	4.53	0.13	1.6	11	0.06		22.65
WT72	276.6	277.1	2.61	0.66	5.1	29	1.53		21.22
WT72	274.65	275.05	1.13	0.26	1.58	27	0.79		9.59
WT72	340	341	1.08	0.01	0.12	3	0.12		5.30
WT72	278	279	0.03	0.02	0.28	8	1.91		3.70
WT72	273.3	274.65	0.67	0.005	0.03	11	0.005		3.69
WT72	312	313.5	0.28	0.005	2.26	1	0.02		3.60
WT72	341	341.6	0.76	0.005	0.04	1	0.06		3.58
WT72	330.3	331.3	0.67	0.09	0.16	3	0.1		3.54
WT72	281.15	282	0.24	0.02	0.2	6	1.18		3.37
WT72	282	282.65	0.34	0.005	0.17	7	0.84		3.34
WT72	282.65	283.8	0.41	0.005	0.02	7	0.68		3.27
WT72	313.5	315	0.33	0.005	1.16	1	0.01		2.71
WT72	292.4	293.65	0.12	0.005	1.8	1	0.14		2.60
WT72	341.6	343	0.49	0.005	0.03	1	0.02		2.31
WT72	277.1	278	0.04	0.06	0.11	8	0.95		2.20
WT72	283.8	285	0.22	0.005	0.03	5	0.56		2.13
WT71	341.4	342.2	0.31	0.17	2.82	6	0.04		4.75
WT71	345	347	0.36	0.005	1.06	1	0.02		2.76
WT69	180.6	181.4	6.13	5.8	18.5	85	0.71	4.58	56.44
WT69	181.4	182.2	4.28	2.07	27.9	50	0.57	4.42	52.41
WT69	182.2	183.05	2.33	2.05	21.7	74	4.54	4.55	44.74

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT69	180	180.6	0.26	0.53	1.42	10	0.31	3.32	4.04
WT69	172.95	173.87	0.45	0.27	0.9	5	0.14	3.23	3.62
WT69	171.1	172	0.19	0.64	1.56	6	0.04	3.21	3.32
WT69	206	207	0.67	0.005	0.03	1	0.01	3.1	3.10
WT68	179	180	0.63	1.68	3.04	20	0.11	2.99	8.50
WT68	178.1	179	0.52	1.25	3.33	15	0.13	3.03	7.70
WT68	180	181	0.21	0.42	1.77	7	0.11	3	3.61
WT68	181	181.6	0.14	0.37	0.62	8	0.14	3.01	2.21
WT67	198.18	198.8	3.58	9.03	26.2	107	0.45	4.05	56.20
WT67	210	211	1.59	0.005	0.05	3	0.03	3.1	7.37
WT67	198.8	200	0.61	0.33	1.55	24	0.33	3.23	6.45
WT66	114	114.5	0.43	0.01	0.005	4	0.14	3.22	2.37
WT65	133.15	134	3.09	3.83	11.9	150	6.79	3.93	47.54
WT65	134	134.6	1.43	2.8	16.5	75	0.36	4.44	30.06
WT65	138.3	139.3	0.61	0.03	0.06	9	0.28	3.8	3.75
WT65	134.6	135.1	0.29	0.08	0.21	11	0.91	3.45	3.55
WT65	135.1	136.05	0.26	0.05	0.19	7	0.9	3.75	3.12
WT65	148.65	149.2	0.23	0.01	0.94	3	0.25	3.52	2.52
WT64	164	165	2.58	11.8	26.7	235	2.58	4.08	65.16
WT64	166	167	3.48	6.27	24.3	87	1.12	4.28	51.50
WT64	167	167.55	3.67	4.87	24.3	88	1.19	4.46	51.44
WT64	165	166	4.56	1.17	16	74	1.14	4.68	43.34
WT64	167.55	168.3	1.24	0.62	3.67	44	3.35	3.8	17.21
WT64	163.15	164	0.71	0.68	2.39	10	0.4	3.05	7.26
WT64	168.3	169	0.22	0.37	1.31	5	0.69	3.19	3.88
WT64	169	170	0.14	0.17	0.76	4	0.55	3.28	2.56
WT62	226	227	0.17	0.74	2.28	26	0.32	3.41	5.64
WT62	217.65	218.55	0.03	0.11	0.2	67	0.6	3.01	5.31
WT62	227	228	0.19	0.24	2.14	14	0.17	3.37	4.26
WT61	257	258	1.28	0.05	2.33	3	0.05	3.23	8.33
WT61	259	260.1	0.87	0.005	0.15	2	0.04	3.24	4.21
WT61	260.1	261.2	0.86	0.01	0.08	1	0.03	3.3	4.03
WT61	256	257	0.06	0.12	2.27	1	0.07	3.16	2.79
WT61	255	256	0.22	0.05	1.48	1	0.07	3.14	2.66
WT61	251.2	252.1	0.15	0.03	1.45	2	0.15	3.18	2.48
WT61	250	251.2	0.1	0.21	1.22	3	0.16	3.08	2.24
WT60	121.65	122.25	1.25	6.79	25.9	213	0.39	4.08	50.05
WT60	148	149.1	1.11	0.53	14.1	14	0.24	3.22	20.65
WT60	147.15	148	0.52	0.07	13.5	4	0.17	3.19	16.36
WT60	122.25	123	0.11	0.3	2.32	96	0.95	3	10.19
WT60	145	146	0.53	0.07	6.38	1	0.1	3.04	9.00
WT60	146	147.15	0.4	0.14	5.68	2	0.1	2.96	7.84

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT60	152	153	0.41	0.05	2.33	1	0.05	3	4.33
WT60	119	120	0.2	0.07	1.84	16	0.12	2.95	3.92
WT60	138	139	0.23	0.03	1.19	4	0.12	3.04	2.65
WT60	150	151	0.19	0.02	1.62	1	0.04	3.01	2.60
WT60	137	138	0.19	0.04	1.35	1	0.12	3.11	2.46
WT60	134	135	0.16	0.02	1.42	1	0.17	3.15	2.46
WT60	123	124	0.005	0.02	1.55	5	0.14	3.07	2.09
WT6	99.65	100.7	2.64	1.29	13.4	32	0.42	3.23	28.70
WT6	98.9	99.25	2.78	11.9	0.36	64	0.45	3.45	26.42
WT6	100.7	101	1.12	0.49	12.6	11	0.16	3.36	18.87
WT6	107	107.45	0.54	0.07	9.25	3	0.07	2.9	11.99
WT6	117	118.7	0.97	0.2	1.6	3	0.05		6.33
WT6	106	107	0.33	0.08	2.81	4	0.06	2.84	4.67
WT59	138.9	139.2	0.9	8.71	27	262	1.05	4.2	54.97
WT59	177.6	178.45	1.12	0.08	17.1	4	0.05	3.28	22.47
WT59	141.5	142	0.37	1.85	7.33	15	0.13	3.17	11.49
WT59	155	156.2	0.59	0.02	0.44	7	0.22	3.6	3.83
WT59	160	160.75	0.21	0.04	2.21	3	0.09	3.25	3.49
WT59	146	148	0.13	0.48	1.9	4	0.06	3.06	3.18
WT59	171	172	0.03	0.04	2.88	1	0.04	3.19	3.16
WT59	156.2	158	0.09	0.04	1.96	1	0.12	3.11	2.63
WT59	154.5	155	0.23	0.03	0.79	4	0.12	3.54	2.25
WT58	149.9	150.1	0.25	2.28	5.21	53	0.38	3.15	11.82
WT58	211.8	212.1	2.26	0.02	1.11	4	0.05	3.59	11.52
WT58	176	178	0.46	0.21	1.88	6	0.15	3.21	4.67
WT58	170.25	171.5	0.24	0.21	0.33	10	0.15	3.63	2.38
WT56	153.4	154.6	5.28	2.71	35.9	74	1.11	4.41	67.60
WT56	154.6	155.8	6.53	1.82	28.1	70	1.77	4.46	65.41
WT56	152.2	153.4	0.737	1.02	2.88	27	0.31	3.18	9.03
WT56	150	151	0.193	0.89	2.4	8	0.06	2.99	4.51
WT56	151	152.2	0.17	0.124	2.88	3	0.04	2.96	3.97
WT56	158	159	0.308	0.128	1.31	4	0.15	3.02	3.24
WT56	160	161	0.0626	0.0249	0.04	6	1.31	3.39	2.61
WT56	161	162	0.0746	0.03	0.214	6	1.03	3.56	2.43
WT56	157	158	0.283	0.107	0.599	3	0.12	2.99	2.30
WT56	155.8	157	0.209	0.0434	0.661	5	0.09	2.93	2.06
WT54	135.5	136	2.6	6.2	30.6	80	0.69	3.95	52.78
WT54	131.5	132	0.683	1.71	25.9	51	0.3	3.75	33.76
WT54	169	169.7	1	0.0222	1.36	6	0.12	3.33	6.37
WT53	218.8	219.8	0.0959	0.0392	0.882	34	0.13	3.36	3.57
WT52	187.8	188.7	2.56	0.177	32.1	50	0.6	3.93	47.53
WT52	186.9	187.8	3.49	0.209	25.9	80	0.66	3.9	47.39

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT52	188.7	189.4	2.34	0.068	22.8	50	0.6	3.86	37.16
WT52	189.4	190.4	0.72	0.046	3.61	10	0.3	3.55	7.89
WT52	185.5	186.2	0.129	0.654	2.65	5	0.13	3.38	4.22
WT52	186.2	186.9	0.301	0.178	1.88	10	0.08	3.3	4.08
WT51	164	164.8	2.53	1.89	27.1	90	1.45	3.85	47.36
WT51	162.1	163	0.739	2.41	27.2	70	0.32	3.92	37.02
WT51	163	164	2.14	3.16	16.9	80	0.36	3.65	34.20
WT51	161.75	162.1	0.799	1.06	3.63	30	0.2	3.16	10.10
WT51	164.8	166	0.178	0.06	0.849	5	0.14	2.94	2.19
WT5	183	183.8	6.19	0.99	24.1	220	19.83	4.11	94.62
WT5	176.35	177	7.97	3.07	17.2	330	1.34	3.83	76.87
WT5	179	180	4.46	8.32	38.8	150	0.49	4.16	74.81
WT5	177	178	5.8	2.55	23.6	290	1.29	3.81	70.71
WT5	178	179	4.5	5.92	33.3	120	1.51	3.95	67.33
WT5	182	183	4.06	4.42	35.4	120	1.88	4.26	66.86
WT5	181	182	3.73	2.22	34.6	70	0.27	4.03	57.54
WT5	180	181	4.59	3.68	25.7	110	0.47	4.07	56.29
WT5	173	174	0.26	0.11	1.83	10	0.01		3.69
WT5	185	186	0.1	0.01	0.06	50	0.01		3.53
WT5	183.8	184	0.27	0.11	1.15	1	0.01		2.51
WT48	345.4	345.95	2.55	0.0016	0.0096	4	0.03	4.31	11.67
WT47	163.7	164.4	3.77	4.14	15.2	201	3.1	4.33	51.79
WT47	162.85	163.7	1.43	1.31	10	60	0.4	3.98	21.57
WT47	164.4	165	0.721	0.0333	1.4	18	0.39	3.31	6.29
WT45	292	292.8	6.78	1.11	11.5	52	0.54	3.72	46.50
WT45	291.5	292	4.14	0.58	9.62	40	1	4.11	32.39
WT45	302.3	302.8	4.44	1.01	6.29	78	0.25	4.36	31.92
WT45	291	291.5	1.63	0.169	8.9	33	1.35	4.1	20.25
WT45	290.4	291	0.764	0.391	7.11	31	1.1	4.02	14.28
WT45	287.4	288.4	0.304	0.194	7.55	11	0.85	3.78	10.96
WT45	292.8	293.8	0.454	0.0478	1.71	7	0.46	3.45	4.86
WT45	302.8	304	0.274	0.0582	0.741	13	0.85	3.77	4.03
WT45	288.4	289.4	0.164	0.0785	1.16	6	1	3.45	3.77
WT45	295	296	0.423	0.198	0.245	13	0.45	3.65	3.72
WT45	298	299	0.166	0.298	0.553	12	0.2	3.34	2.53
WT45	289.4	290.4	0.145	0.0904	0.392	6	0.41	3.32	2.07
WT43	204.05	205	1.88	8.18	36.2	240	4.64	4.13	72.06
WT43	205	206	3.26	4.51	34.1	160	2.04	4.16	64.69
WT43	207	207.85	2.81	3.95	26.1	80	1.59	4.4	48.80
WT43	206	207	2.92	2.09	17.2	100	0.9	3.96	39.15
WT43	207.85	209	1.39	0.39	5.02	140	2.7	3.92	23.86
WT43	209	210	0.592	0.109	2.62	20	0.63	3.82	7.46

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HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT43	212	213.2	0.373	0.049	0.433	10	0.46	3.55	3.41
WT43	210	211	0.311	0.133	0.643	5	0.36	3.87	2.96
WT43	211	212	0.296	0.125	0.434	5	0.27	3.98	2.54
WT42	233	234	1.8	0.004	0.22	5	0.08	3.27	8.67
WT42	227	228.25	1.25	0.007	0.069	5	0.08	3.85	6.07
WT42	232	233	1.05	0.003	0.138	5	0.06	3.09	5.21
WT42	235	236.15	0.856	0.003	0.034	5	0.06	3.02	4.24
WT41	254.7	255.8	3.75	5.15	26.9	110	8.58	4.08	66.72
WT41	258.3	259.35	3.99	5.68	27.8	90	1.66	4.33	57.79
WT41	257.3	258.3	3.08	6.17	24.3	100	1.73	4.04	51.31
WT41	255.8	256.8	3.98	2.72	20.9	30	0.1	4.12	42.69
WT41	284.2	285	3.42	0.007	0.3	5	0.38	4.14	16.41
WT41	260	261	0.399	2.01	4.34	20	0.87	3.19	10.14
WT41	259.35	260	0.41	0.348	3.71	5	0.3	3.21	6.54
WT41	261	262	0.266	0.814	3.33	5	0.22	3.07	5.76
WT41	256.8	257.3	0.573	0.254	0.541	5	0.08	3.31	3.71
WT41	285	285.6	0.607	0.005	0.021	5	0.12	3.41	3.21
WT41	252.4	253.6	0.192	0.031	0.595	5	0.43	3.17	2.40
WT39	44	48	0.367	0.002	1	0.5	0.005		2.68
WT38	197.75	198.9	3.7	7.12	14.3	390	1.78	3.69	62.28
WT38	198.9	199.3	1.37	6.34	11.1	140	1.15	3.56	32.17
WT38	200	200.8	0.783	0.128	0.637	40	0.74	3.63	7.71
WT38	199.3	200	0.346	0.401	1.66	20	0.9	3.63	6.03
WT38	50	54	0.341	0.0117	0.489	1	0.005		2.09
WT37	222.7	224	6.79	5.28	31.7	160	1.71	4.13	78.15
WT37	224	225	7.54	3.26	32.6	100	1.01	4.38	76.21
WT37	226	227	8.34	5.08	26.5	120	0.78	4.36	75.95
WT37	225	226	7.83	3.25	19.3	150	2.23	4.32	68.98
WT37	227	227.9	4.49	5.77	29.9	70	0.3	4.28	59.01
WT37	227.9	229	0.342	0.79	3.33	20	0.32	3.07	7.13
WT37	244	245	0.845	0.004	0.045	2.5	0.1	3.52	4.11
WT37	222.2	222.7	0.194	0.017	0.14	10	1.48	3.47	3.78
WT37	60	64	0.25	0.0055	1.2	0.5	0.02		2.38
WT37	44	48	0.345	0.0324	0.666	0.5	0.02		2.29
WT37	221.2	222.2	0.068	0.024	0.297	5	0.8	3.23	2.09
WT36	145.4	146.9	10.9	4.37	32.8	195	1.02	3.67	97.97
WT36	151.8	152.8	9.9	2.42	22	155	5.2	3.81	84.91
WT36	144.4	145.4	6.87	3.71	32.6	230	2.3	3.69	83.25
WT36	149.6	150.6	5.4	4.38	33.8	157	3.68	3.73	76.05
WT36	150.6	151.8	5.62	6.15	33.4	161	0.66	3.73	73.82
WT36	148.6	149.6	5.99	1.7	33.7	114	3.1	3.95	73.09
WT36	143.4	144.4	7.92	1.31	12.4	162	8.06	4.1	70.22

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT36	155.9	156.9	5.3	1.39	34.9	96	2.7	4.07	69.31
WT36	156.9	157.9	7.6	1.09	28.8	72	0.26	4.06	68.23
WT36	152.8	153.8	7.13	1.88	23.2	123	2.78	3.74	67.89
WT36	147.6	148.6	4.39	2.13	30.8	174	2.02	3.88	65.41
WT36	153.8	154.9	4.2	1.01	32.4	97	3.92	4	63.45
WT36	157.9	158.9	7.53	2.41	15.2	140	1.94	4.36	61.87
WT36	154.9	155.9	3.16	0.2	34.3	70	5.02	4.12	60.08
WT36	158.9	159.5	3.47	8.31	23.7	106	0.44	4.37	52.58
WT36	140.6	142.4	2.39	7.12	22.1	116	0.32	3.95	45.67
WT36	142.4	143.4	5.46	0.88	2.53	85	4.32	4.08	38.97
WT36	146.9	147.6	2.34	2.53	14.2	66	0.5	2.93	31.27
WT36	139.6	140.6	0.56	1.25	3.07	36	0.71	2.71	9.73
WT36	159.5	160.5	0.8	0.15	3.98	20	0.23	2.77	9.20
WT36	160.5	161.6	0.48	0.08	4.02	18	0.23	2.83	7.64
WT36	138.7	139.6	0.26	0.22	1.11	14	0.4	2.52	3.86
WT36	162.6	163.6	0.2	0.08	0.48	8	0.29	2.74	2.34
WT33A	297.8	298.5	1.89	2.84	20.1	79	0.71	3.86	36.49
WT33A	298.5	299.25	1.52	1.48	11.1	39	1.16	3.62	23.05
WT33A	299.25	300	1.46	0.13	5.11	17	5.08	3.35	20.16
WT33A	300	300.8	1.11	0.06	0.68	10	4.05	2.86	12.19
WT33A	300.8	301.8	0.28	0.02	0.15	4	0.71	2.95	2.69
WT32	219.6	220.3	0.65	2.35	3.31	33	0.28	2.67	10.41
WT32	218.6	219.6	0.53	1.6	4.32	26	0.36	2.75	10.00
WT32	222.3	223.5	0.26	0.34	0.76	25	2.7	3.11	7.62
WT32	223.5	224.7	0.3	0.22	0.41	16	0.91	2.98	4.21
WT31	241.6	242.7	3.6	3.3	29.7	70	0.71		53.53
WT31	242.7	243.7	4.6	1.54	12	57	2.96		41.44
WT31	243.7	245	0.45	0.05	2.5	7	0.74		6.05
WT31	248	249	0.04	0.68	1.9	10	0.06		3.29
WT31	239.6	240.6	0.46	0.02	0.02	8	0.34		3.06
WT30	143.2	144.5	3.56	2.01	13.2	121	1.38		39.90
WT30	144.5	145.5	0.79	0.95	5.12	49	0.74		13.40
WT30	142.7	143.2	0.65	0.22	2.72	64	1.12		11.26
WT30	145.5	146	0.43	0.56	3.93	34	0.41		8.92
WT30	141.7	142.7	0.25	0.06	0.1	12	0.44		2.62
WT29	127.4	128.2	0.35	1.5	7.74	198	1		23.80
WT29	126.4	127.4	0.77	0.56	3.06	78	0.51		12.35
WT29	125.4	126.4	1.12	0.21	1.67	45	0.7		10.55
WT29	123.7	124.3	0.15	0.76	2.39	10	0.22		4.57
WT29	123	123.7	0.13	0.09	1.27	8	0.28		2.81
WT27	115.4	116.3	8.53	1.37	29.2	123	9.55		89.62
WT27	116.3	116.95	5.64	1.58	39.5	122	7.7		84.43

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT27	116.95	118	13.84	0.82	12.98	62	1.65		81.47
WT27	118	118.4	4.17	12.5	27.2	254	2.64		74.52
WT27	113.2	114.2	3.99	4.89	38.9	94	1.41		68.16
WT27	114.2	115.4	4.89	3.64	39.1	50	0.62		67.62
WT27	118.4	119.6	0.51	0.65	1.91	29	1.25		8.25
WT27	112.6	113.2	0.45	0.09	0.19	36	0.61		5.32
WT27	120.3	122.9	0.11	0.1	2.93	9	0.51		4.78
WT27	119.6	120.3	0.12	0.06	1.15	8	0.36		2.74
WT27	122.9	126.4	0.05	0.03	1.13	6	0.34		2.23
WT22	282	282.5	3.58	0.53	2.62	315	2.21	3.25	41.12
WT22	283	284	0.06	0.28	1.36	5	0.34	2.97	2.64
WT21	313.45	314	1.61	0.58	1.91	57	1.02	2.98	14.45
WT21	306	306.8	0.38	0.7	5.2	76	0.25	3.58	12.36
WT21	303.5	304	0.26	0.65	1.36	20	0.52	3.23	4.98
WT21	290.7	293.85	0.14	0.09	2.84	5	0.21		4.14
WT21	304	305	0.15	0.51	1.03	18	0.48	3.42	3.87
WT21	305	306	0.03	0.08	0.09	5	1.95		3.43
WT21	288.5	290.7	0.14	0.31	1.28	7	0.25		2.93
WT21	239.6	245.55	0.35	0	1.03	3	0.07		2.87
WT21	306.8	307	0.15	0.09	0.38	19	0.21		2.56
WT21	303	303.5	0.05	0.08	0.32	15	0.64		2.44
WT21	307	308	0.09	0.08	0.47	12	0.39		2.22
WT20	184	185	0.65	1.09	7.61	26	0.38	3.13	13.46
WT20	139.5	140.3	2.42	0.02	1.42	7	0.1		12.79
WT20	185	186.6	0.1	1.57	6.06	23	0.22	2.86	9.42
WT20	183	184	0.36	1.12	3.86	12	0.13	3.01	7.24
WT2	425	426	0.59	0	0.37	1	0.08		3.18
WT19	179	179.25	1.66	0.94	9.78	41	0.78	2.95	21.51
WT19	160	160.2	1.04	1.04	14.4	18	0.38	3.5	21.47
WT19	178.6	179	0.53	0.09	5.34	22	0.66	2.84	10.06
WT19	160.2	161	0.92	0.92	4.58	6	0.17	2.9	10.00
WT19	159	159.5	0.03	0.03	5.06	4	0.17	3.11	5.71
WT19	179.25	180	0.23	0.09	1.26	7	0.12	2.78	2.95
WT19	161	162	0.08	0.54	1.39	6	0.13	2.96	2.71
WT19	159.5	160	0.04	0.03	2.03	1	0.11	2.93	2.45
WT19	158	159	0.07	0.01	1.8	1	0.1		2.33
WT19	157	158	0.15	0.05	1.17	1	0.11		2.10
WT18	305.1	305.45	5.77	0.91	15.4	46	0.26	3.81	44.97
WT18	307.75	308	2.15	1.82	20.5	115	1.6	3.62	40.73
WT18	309	309.3	1.06	6.92	19	74	0.22	3.92	33.82
WT18	311	311.1	2.31	0.5	5.22	38	1.1	3.82	19.79
WT18	308	309	1.37	1.63	9.07	37	0.65	3.81	19.60

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HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT18	278.1	278.8	3.73	0	0.34	7	0.128	3.61	17.58
WT18	307.25	307.75	1.63	0.06	2.74	27	0.59	3.94	12.54
WT18	306	307	0.9	0.02	0.19	11	0.28		5.29
WT18	276.5	278	1.01	0	0.1	1	0.05		4.74
WT18	309.3	309.9	0.43	0.23	1.24	13	0.42	3.25	4.73
WT18	309.9	311	0.35	0.03	0.36	13	0.61		3.61
WT18	305.45	306	0.3	0.09	0.5	9	0.18		2.71
WT17	108.3	108.8	6.89	1.91	16.6	105	1.36	3.93	57.09
WT17	106	106.3	1.65	5.54	34.2	50	1.79	4.4	51.44
WT17	109	110	1.2	0.04	0.64	18	0.5	3.28	7.83
WT17	113	114	1.02	0.24	0.93	8	0.26		6.52
WT17	112	113	0.37	1.11	2.79	12	0.15	3.11	6.23
WT17	114.2	115	0.08	0.16	0.43	18	2.55		5.71
WT17	111	112	0.24	0.48	3.34	11	0.1	3.13	5.59
WT17	115	116.3	0.31	0.63	1.78	12	0.3		4.81
WT17	108	108.3	0.21	0.06	0.02	32	1.28		4.79
WT17	114	114.2	0.18	0.26	1.66	11	0.74	2.96	4.40
WT17	110	111	0.05	0.38	2.96	10	0.16	3.07	4.31
WT17	108.8	109	0.29	0.16	0.25	18	0.25		3.11
WT17	106.3	107	0.12	0.2	0.36	11	0.91		3.04
WT15	77	77.7	1.81	2.37	0.5	491	17.95		66.06
WT15	76	77	0.1	0.3	0.09	8	4.11		7.25
WT15	78.9	79.4	0.07	2.86	0.03	4	0.45		3.44
WT15	79.4	81.5	0.11	1.09	0.16	3	0.75		2.76
WT14	129.3	130	0.31	0.01	0.02	5	0.29		2.13
WT13	236.6	237	2.08	0.97	39	8	0.05	3.3	49.58
WT13	237	237.85	1.65	0.65	26.1	8	0.05	2.9	34.51
WT13	235.3	236	2.41	0.19	4.13	6	0.04	3.13	15.44
WT13	236	236.6	0.64	0.03	0.72	2	0.02	3.57	3.75
WT12	259.8	260	1.29	0.35	5.7	20	0.82		14.12
WT11	50.3	51	0.23	1.4	0.02	2	4.73	2.73	9.15
WT11	51	51.7	0.33	2.2	0.02	4	0.528	2.68	4.20
WT10	195	196	7.42	3.34	25.2	99	1.38	4.27	68.82
WT10	192	193	4.51	4.22	28.4	114	0.65	3.97	59.55
WT10	196	196.5	4.73	3.2	24	69	0.27	4.26	52.09
WT10	193	193.35	2.6	5.04	30.5	67	0.28	4.41	50.41
WT10	194.7	195	4.84	0.5	16.6	63	2.1	3.91	45.42
WT10	191.85	192	5.2	0.34	10	60	2.06	3.81	40.06
WT10	199	199.5	1.82	0.96	9.7	48	1.09	3.39	23.03
WT10	193.35	194	1.63	2.13	5.12	62	0.54	3.48	18.54
WT10	194	194.7	2.42	0.26	1.92	36	1.15	3.47	16.75
WT10	198	199	1.2	0.37	3.84	35	1.28	3.32	13.45

HOLE_ID	DEPTH_FROM	DEPTH_TO	Cu%	Pb%	Zn%	Ag_ppm	Au_ppm	SG	Zn_Eq%
WT10	199.5	200	1.31	2.02	1.07	41	0.51	3.31	11.67
WT10	197	198	1.16	0.6	1.55	23	0.65	2.97	9.51
WT10	196.5	197	0.5	0.75	1.76	22	0.18	3.31	6.15
WT10	176	178	0.19	0.38	1.59	5	0.08		3.15
WT10	191	191.85	0.07	0.07	0.02	9	1.18		2.65
WT10	178	179	0.18	0.06	1.04	3	0.01		2.08

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APPENDIX 4

WATERLOO – DRILLHOLE COLLAR PLAN