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ASX Release

5 June 2023

Wilconi Nickel-Cobalt Project Mineral Resource upgraded.

HIGHLIGHTS:

- **Wilconi Mineral Resource Estimate upgraded to include a maiden Measured resource of 19 million tonnes (Mt) following infill drilling completed in 2022.**
- **Snowden Optiro reported resources within a RPEEE pit, using a cut-off grade of 0.5% Ni of 73Mt @ 0.79% Ni and 0.04% Co (570,000 tonnes contained nickel and 29,500 tonnes of contained cobalt).**
- **40 million tonnes (55%) of the Mineral Resource estimate is classified in Measured or Indicated categories;**
- **All on-going work at Wilconi are studies required for completion of a pre-feasibility study.**

A-Cap Energy Limited (ASX:ACB) has updated the JORC Mineral Resource Estimate (MRE) for its Wilconi Ni-Co Project near Wiluna in Western Australia, reporting a maiden Measured resource of 19Mt. 40Mt (55%) of the MRE is now classified in Measured or Indicated categories.

In addition to historical data, the MRE by independent resource estimation specialists, Snowden Optiro used data from an infill drilling program in 2022 over 217 reverse circulation (RC) and diamond holes for 9,536m. (see Table 1).

2023 Snowden Optiro Ni > 0.5% and within RPEEE pit					
Category	**Tonnes (Mt)**	**Ni %**	**Co %**	**Nickel metal (Tonnes)**	**Cobalt metal (Tonnes)**
Measured	19	0.88	0.06	160,000	11,200
Indicated	21	0.82	0.03	170,000	8,300
Inferred	33	0.73	0.04	240,000	10,000
Total	73	0.79	0.04	570,000	29,500

Table 1: *May 2023 Wilconi Nickel Cobalt Mineral Resource Estimate*

Rounding may cause minor inconsistencies

Grade-tonnage information at various other Ni cut-off grades are shown in Table 2.

2023 Snowden Optiro Ni > 0.5% and within RPEEE pit					
Cut-off (Ni %)	Tonnes (Mt)	Ni %	Co %	Nickel metal (Tonnes)	Cobalt metal (Tonnes)
0.5	73	0.79	0.04	570,000	29,500
0.6	61	0.84	0.04	510,000	24,400
0.7	30	1.03	0.06	300,000	17,700
0.8	20	1.18	0.07	230,000	13,700
0.9	18	1.21	0.07	220,000	12,500
1.0	17	1.22	0.07	210,000	12,100

Table 2: *Wilconi Nickel Cobalt grade-tonnage information at various Ni cut-off grades*

Rounding may cause minor inconsistencies

A-Cap Energy Deputy Chairman Paul Ingram said the MRE upgrade provided further evidence of the quality of nickel and cobalt at Wilconi.

"It confirms confidence in the high-grade mineralisation of the resource and it is particularly pleasing to see a 40% of the resource now being reported as Indicated and Measure Mineral Resources. This upgrade is of key importance as we continue pre-feasibility studies on the Project."

Figures 1 to 4 below show the location of the 2022 drilling completed at Wilconi, which was critical to improving the resource confidence in the Indicated and Measured categories. The figures show the spacing of the infill drilling within the resource area in relation to historical drilling and earlier phases completed by A-Cap. Figure 5 is a typical cross-section through the deposit showing the near surface and flat-lying nature of the nickel and cobalt mineralisation zones. Collar details and intercepts of all A-Cap's drill holes, including those shown in Figures 1 and 5 have been provided in earlier ASX announcements (see ASX release 23rd Nov 2022 and 24th Sept 2021).

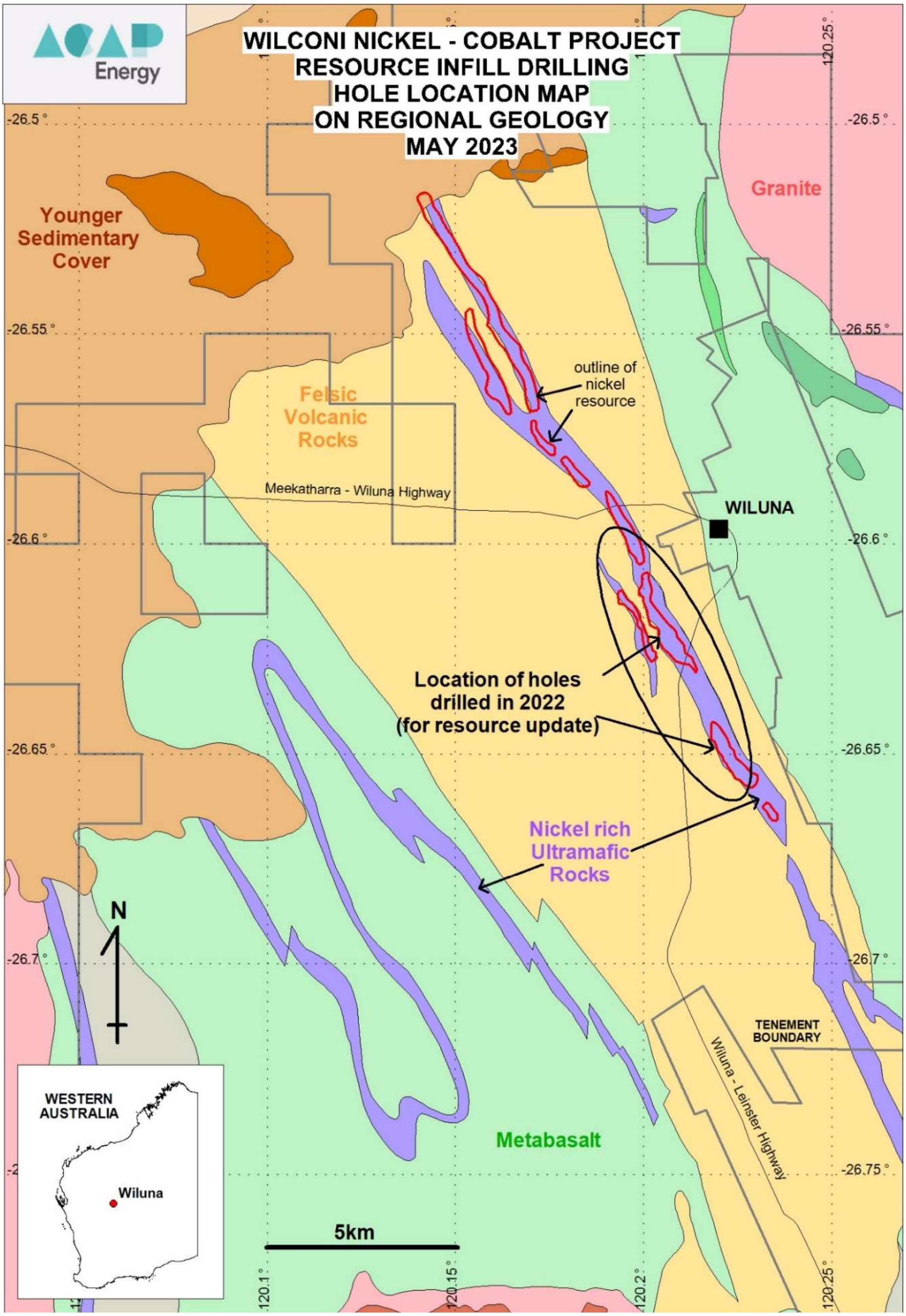

Figure 1: Regional geological setting of the Wilconi Nickel-Cobalt Project showing extent of nickel bearing ultramafic rocks, outline of the Wilconi nickel resource and location of recent RC and diamond drilling.

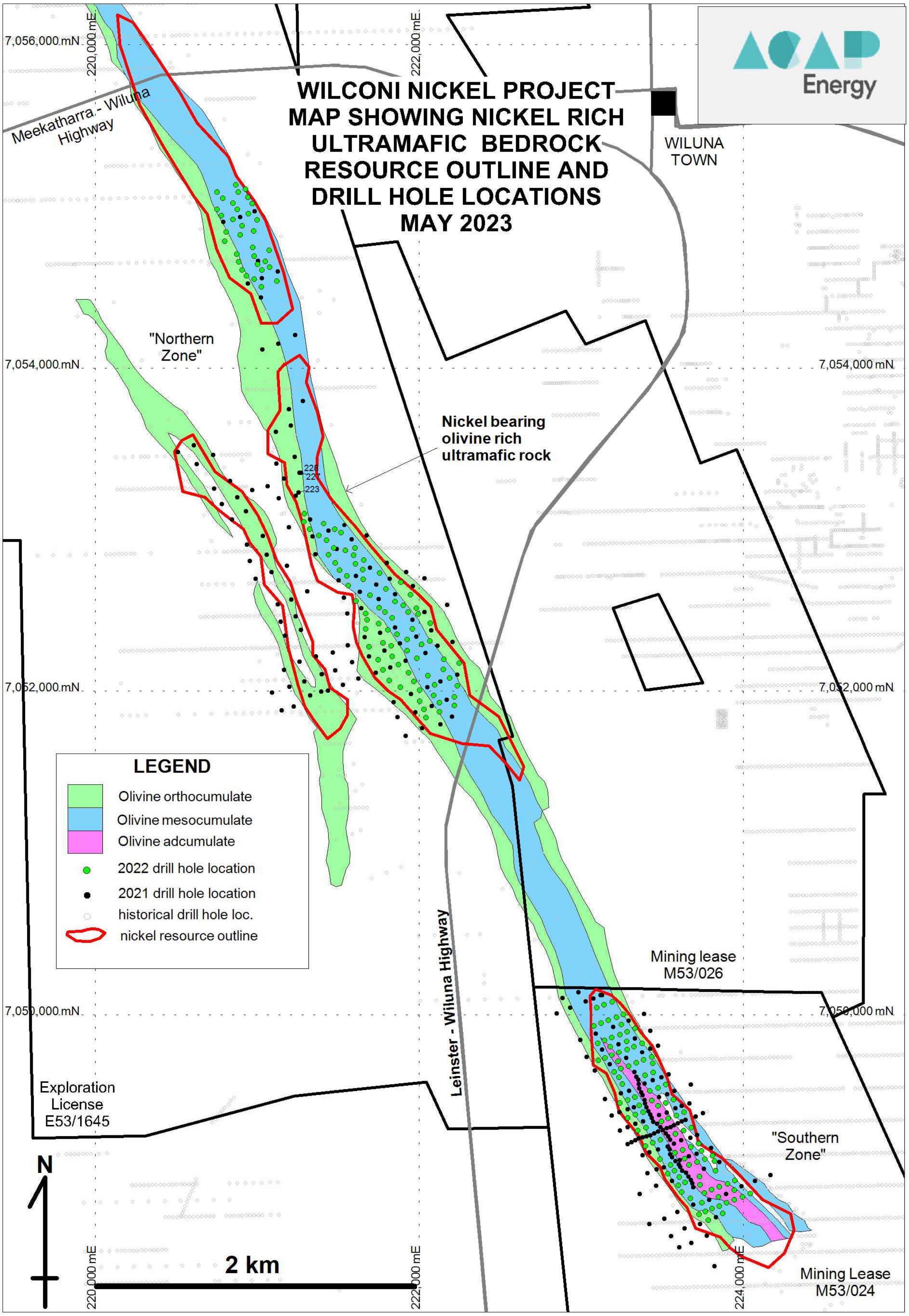

Figure 2: *Map showing nickel rich ultramafic bedrock, resource outline and location of A-Cap's infill RC and diamond drill holes.*

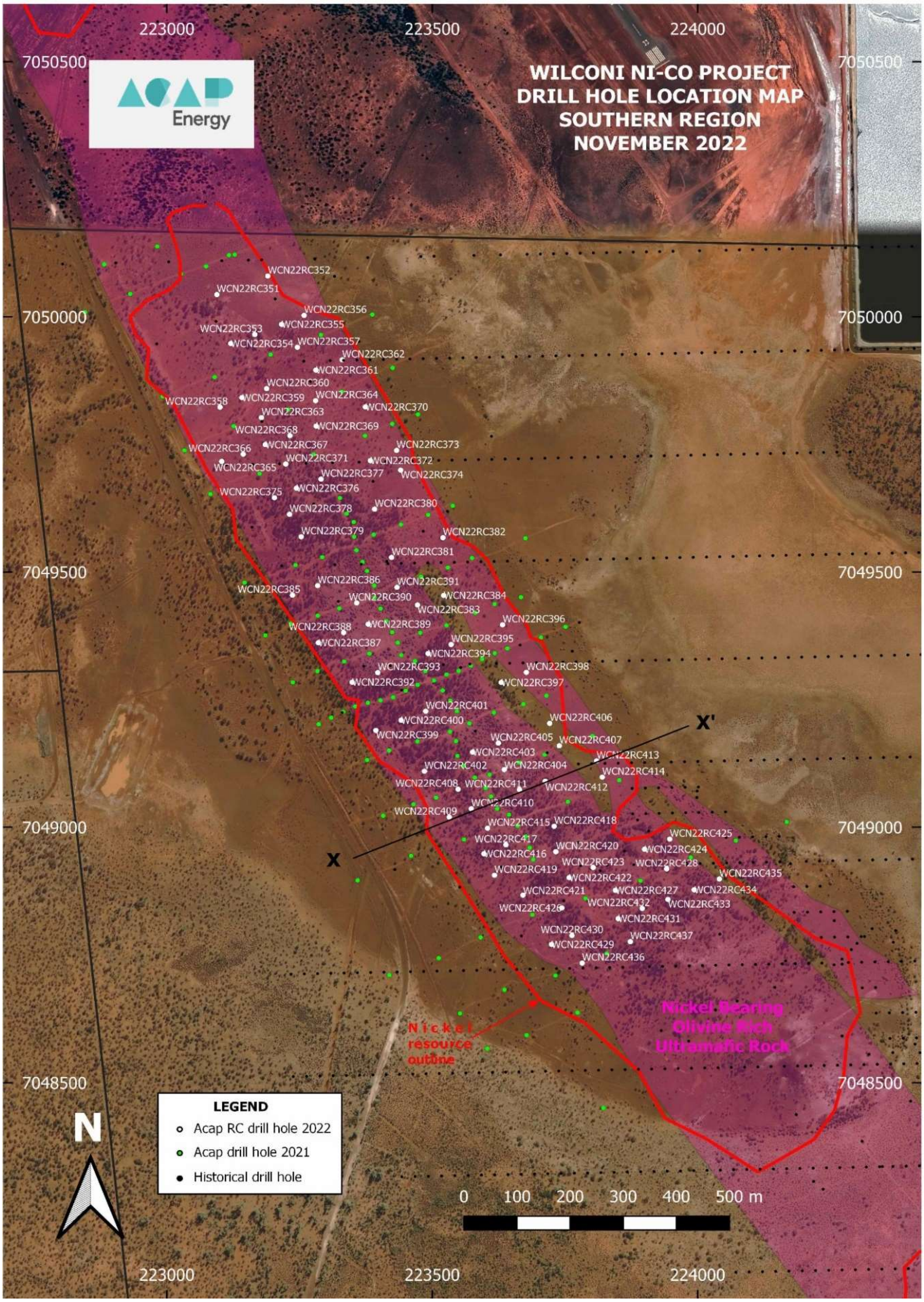

Figure 3: *Wilconi Southern Resource Area drilling showing underlying nickel bearing host rock, outline of the nickel resource, drill hole points and location of cross section X – X' shown in Figure 5.*

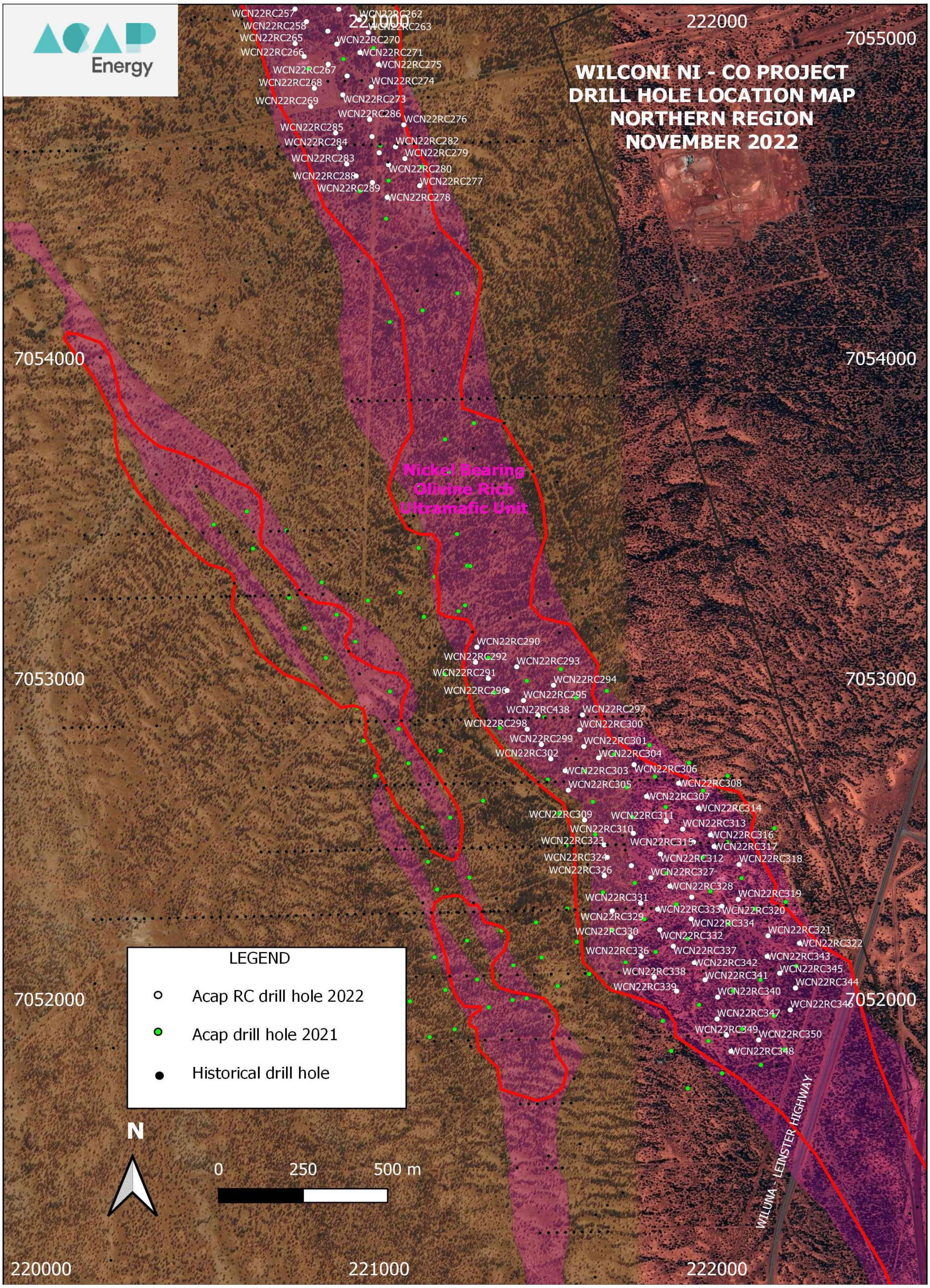

Figure 4: *Wilconi Northern Resource Area showing underlying nickel bearing host rock, outline of the nickel resource, historical and A-Cap drillhole locations.*

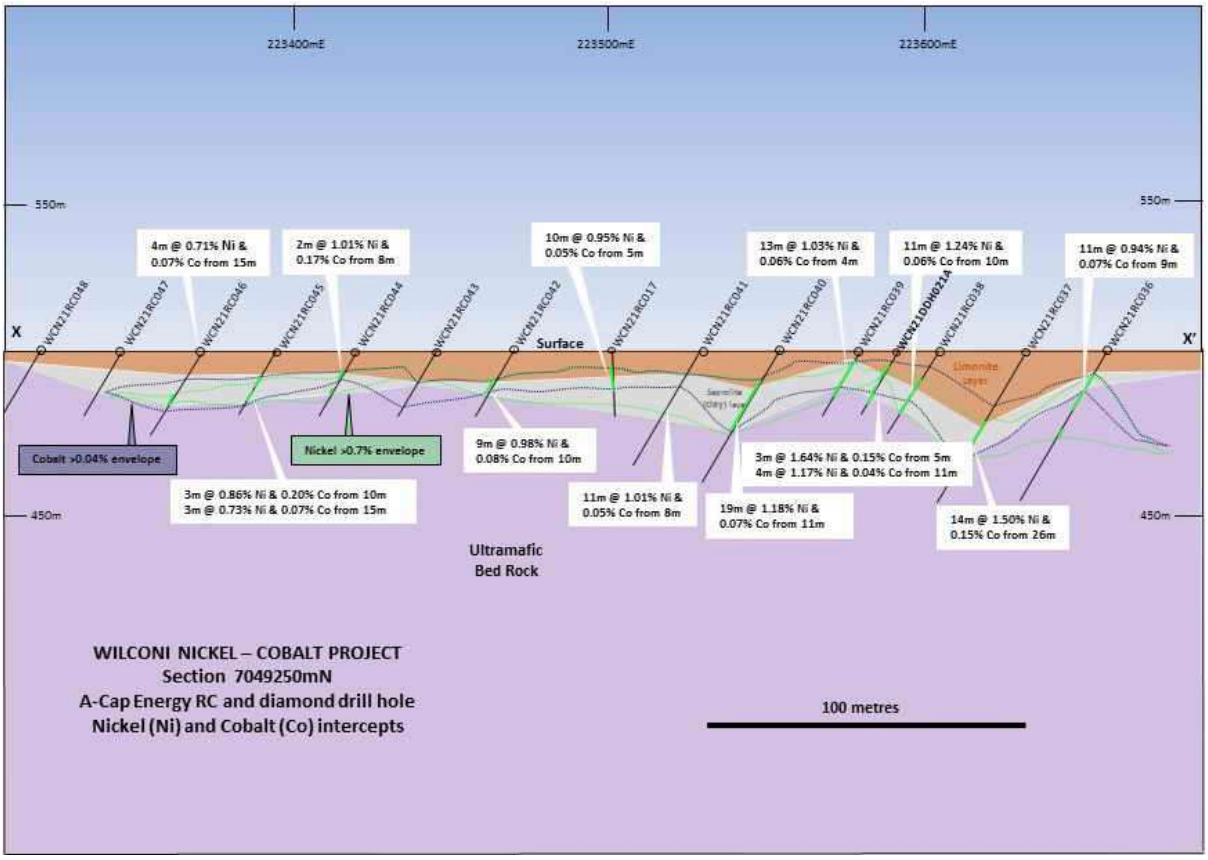

Figure 5: *Cross section X – X' showing the nickel and cobalt intercepts from the 2021 and 2022 infill drill hole programmes. The nickel – cobalt mineralisation forms a flat-lying zone, close to surface, concentrated where weathering of the ultramafic bedrock is most intense.*

MATERIAL INFORMATION SUMMARY

Pursuant to ASX Listing Rule 5.8.1, the following summary of information has been provided as material to understanding the Mineral Resource estimate.

GEOLOGY AND GEOLOGICAL INTERPRETATION

The Wiluna nickel-cobalt laterite deposit is located within the Archaean Norseman-Wiluna greenstone belt. The nickel-cobalt mineralisation has developed through lateritisation of the Perseverance ultramafic sequence. The sequence extends for around 20 km along strike and is up to 1,500 m wide.

The Perseverance ultramafic sequence trends NNW-SSE and dips steeply towards the east. Locally, the geology consists of a less continuous western ultramafic sequence, and a more continuous eastern ultramafic sequence (Figure 3). The eastern sequence is offset by a north-south trending fault at around 7,056,000 mN, interpreted from aeromagnetic data. Both the western and eastern sequences contain similar lithologies of olivine orthocumulate, olivine mesocumulate and minor olivine adcumulate rocks. Pyroxene cumulate and gabbro are generally located along the western margins, with olivine pyroxene cumulate found along the eastern margins. At the boundaries of the ultramafic sequence, the lithologies are generally intermediate and mafic volcanics and dolerite.

The region is covered by a thick blanket of lateritic regolith and outcrop is sparse. The detailed geological understanding is based primarily on the extensive drilling conducted over the deposit. Nickel and cobalt mineralisation has been formed by intense weathering (lateritisation) and has concentrated in a saprolite clay layer that overlies the ultramafic rock unit. The depth to significant (>0.5% Ni) mineralisation ranges from 2 m to 60 m. The nickel mineralisation zone can be up to 30 m thick, averaging around 7 m in thickness. Detailed studies have shown that cobalt has been preferentially enriched in the upper portion of the saprolite clay layer; this zone has been modelled independently and incorporated into the updated resource estimate.

DRILLING INFORMATION

The Wilconi deposit has been explored over a period of more than 50 years by Delhi Australian Petroleum (1967 – 1968), AMAX Exploration (1971 -1973), Trig Mineral Exploration (1972), Kennecot exploration (1971 – 1972), Asarco Australia (1992), CRA Exploration (1992 – 1997), Wiluna Mines (1998), Outokumpu Mining (1998), Agincourt Resources (2005 – 2006), Independence Group and Oxiana Limited (2005 – 2009) and A-Cap Energy Limited (2019-2023). During this period 14,378 holes for a total of 529,900m have been drilled in the Wilconi district.

Before A-Cap's tenure, drilling was conducted at 100 m intervals along lines spaced 400 m apart along the entire strike length of the deposit. The drill lines are orientated perpendicular to the strike of the mineralisation and holes have been drilled between -60˚ and -90˚ at a high angle to the flat-lying zones of mineralisation. In 2021, A-Cap infilled the drilling grid to a nominal 50 m by 100 m in two shallow areas of higher-grade Ni and Co mineralisation. Some 25 m spaced drilling was undertaken in the southern infill area to provide supporting information on lithology and grade continuity.

SnowdenOptiro extracted a sub-set of 948 holes, totalling 70,135 m from the main database that were considered to be of sufficient quality to support a Mineral Resource estimate. Drilling that intersected the mineralised zone used to complete the MRE included 606 reverse circulation (RC), 69 aircore (AC) and 273 diamond drill (DD) holes.

Historical collar survey methods have not been recorded in the database, although locations appear to be accurate as most hole collars can still be identified in the field. Local grids were used in the early 1968-71 drilling and were not picked up by GPS. Local co-ordinates have been converted to GDA94 Zone 51 co-ordinates using a grid transformation.

Holes drilled by Wiluna Mines were surveyed downhole by a Reflex multishot instrument. Agincourt, Independence and Oxiana used an Eastman single shot down hole camera to survey the collar and base of their drill holes. A-Cap used a Reflex Gyro north seeking survey tool for its drill campaigns. All A-Cap RC and diamond holes were surveyed at 5m intervals from top to bottom. Historical and recent logging of drill chips and core is of high quality and completed by experienced field geologists and personnel. In 2019, A-Cap drilled four RC holes that twinned historical RC holes (CRA 1995), which confirmed the original RC results.

SAMPLING AND SUB-SAMPLING

RC drill holes were sampled and geologically logged on 0.5 m, 1 m or 2 m intervals. Independence and Oxiana used a combination of riffle splitters or spears for collecting a subsample of drill chips for analysis. A-Cap rigs used a rig-mounted Metzke sampling system using an inverted cone-style splitter considered to provide a good subsample. Other companies did not record their method of sampling RC chips, however, it is expected that prevailing industry-standard practices were employed. CRA and A-Cap recorded recovered weights of all RC samples. Recoveries were believed to be in the order of 100%. Diamond core sampling varied between 1 m to 4 m intervals, with selective sampling at narrower intervals to geological/mineralisation boundaries. Wiluna Mines used a diamond saw to cut core in half lengthwise for sampling. A-Cap used core saws where core was competent enough to be sawn; in soft or clayey material steel spatulas were used.

For geochemical analyses, CRA used Analabs; Agincourt, Independence, Oxiana, and Wiluna Mines used Amdel (Welshpool, Perth); A-Cap used ALS (Perth), and Oxiana also used Genalysis on occasions. All laboratories were ISO accredited. It is assumed that standard dual stage crushing and pulverisation was employed for sample preparation. For Agincourt RC sampling, either a blank was inserted or a duplicate prepared every 1 in 20 samples. Oxiana inserted certified reference materials (CRMs) or prepared duplicates every 1 in 12 samples. Nickel assays were within 5% of recommended standard values and cobalt assays within 15% of recommended values. Historical records of quality control for other RC/RAB/AC drilling have not been sighted however, it is expected that prevailing industry standard QAQC practices were employed. A-Cap inserted CRMs, blanks or prepared duplicates every 10th sample. Duplicate samples were collected at the same time using a Metzke sampling system attached to the rig. QAQC results were considered acceptable for resource estimation purposes.

SAMPLE ANALYSIS METHODS

Agincourt drill samples were analysed using ICP, with parts per million accuracy. For Independence drilling, samples were analysed by using four-acid digest and ICP/OES finish (technique ICP102) to parts per million accuracy. Oxiana had samples analysed at Amdel by XRF at 0.001 % accuracy and Genalysis by ICP to ppm accuracy. In 2019, A-Cap used a four-acid digest with ICP/MS finish (48 elements) to ppm accuracy. For the 2021 infill drilling campaign, A-Cap used ALS (Perth) method ME-XRF12n (16 standard elements + Loss on Ignition).

ESTIMATION METHODOLOGY

Drillhole data was composited downhole to 1 m intervals prior to geological modelling, statistical analysis, variogram modelling, and block grade estimation process.
Three-dimensional wireframes were created using Leapfrog from Ni and Co drill hole composite assays. Separate wireframes were constructed for Ni>0.25%, Ni>0.5%, Ni>1.0% and Co> 400 ppm and were used as estimation domains.

Composites within each of the mineralised domains were analysed to ensure that the grade distribution was indicative of a single population, with no requirement for additional sub-domaining, and to identify any extreme values which could have an undue influence on the estimation of grade within the domain.

Variography for the mineralised domains was completed in Supervisor V8.15 using normal scores transformed data, with the variogram model back-transformed prior to grade estimation.

A range of block sizes was reviewed, and a parent cell block size of 50mE by 50mN by 1 mRL was selected. This block size represents approximately half the drill spacing in regions containing the Measured and Indicated material. The block model was constructed in Surpac v2023 software. Grade estimation was completed using ordinary kriging (OK) of the 1.0m composited samples. The model was validated by: (1) comparing the wireframe volumes with block model volumes; (2) comparing the mean input composite grade with the estimated block grade; (3) visual comparison of the drillholes and blocks, and ; (4) examining trend plots of the input data and estimated block grades.

Bulk density was measured for 429 physical core samples in ore and 1040 waste/low grade samples. Snowden Optiro developed surfaces for each lithologic /weathering boundary and assigned density values (determined by the Archimedes immersion method) provided by A-Cap. In-situ dry bulk density (DBD) values of 2.11 t/m3, 1.78 t/m3, and 1.81 t/m3 were assigned to limonitic saprolite, saprolite and saprock ores respectively. Waste and overburden was assigned a DBD value of 2.4 t/m3 and fresh rock a DBD value of 2.127 t/m^3.

CLASSIFICATION CRITERIA

The Mineral Resource has been classified by considering the confidence in the geological model, continuity of mineralised zones, drilling density, the underlying database, and the available bulk density information. The Wilconi Mineral Resource has been classified in accordance with JORC 2012 guidelines using drill density as follows:

- Measured Mineral Resources – 50 m by 50 m drill spacing
- Indicated Mineral Resources – 200m by 100m drill spacing
- Inferred Mineral Resource – up to 100 m by 400 m drill spacing
- Geological continuity was demonstrated by interpretation of lithology and weathering zones hosting the mineralisation and segregation of mineralisation into tabular zones within these.

MINING AND METALLURGICAL ASSUMPTIONS

Preliminary metallurgical test work has indicated that Ni and Co can be recovered by high-pressure acid leaching (HPAL), atmospheric leaching, and acid bake processing methods using sulphuric acid. Some of the mineralised material may be suitable for economic extraction by acid heap leach. Tests showed the preferred processing method (HPAL) returned metal recoveries in excess of 90%.

The parameters used to define the pit containing material with a reasonable probability of eventual economic extraction (RPEEE) are listed in Table 3.

CUT-OFF GRADE

Nickel and cobalt prices assumed for the Mineral Resource estimate are US$23,000/t and US$34,000/t respectively, with an assumed exchange A$/US$ rate of 0.70. Feasibility work is yet to determine an economic cut-off grade, which will vary depending on the processing method chosen. A cut-off grade of 0.5% nickel was assumed for the deposit, which is appropriate for most of the likely processing options under consideration.

OPTIMISATION PARAMETERS FOR USE IN WILCONI RPEEE PIT			
Basis of optimisation	**Unit**	**Value**	**Comment**
Bench Height	m	10	
Berm Width	m	4	
Face Angle	deg	60	
Benches	#	10	
Overall Angle	deg	45.7	
Ramp width	m	22	
Ramp Passes	#	1	
Pit depth	m	50	
Overall angle inc. ramp	deg	40.8	
Overall angle exc. ramp	deg	46.9	Rounded to 45 for optimisation
Mining Dilution	%	0.05	
Mining Recovery	%	0.95	
Operating Cost	A$/t	5	
Contingency	%	0	
Total Mining Cost	A$/t	5	
Process recovery - Ni	%	90	
Process recovery - Co	%	90	
Processing cost	A$/t ore	55.3	
G&A	A$/t ore	5.75	
Contingency	%	0	
Total ore cost	A$/t ore	61.05	
Price – Ni	US$/t	23000	
Price – Co	US$/t	34000	
Govt. royalty - Ni	%	0.025	
Govt. royalty - Co	%	0.025	
Tenement royalty	%	0	
Selling costs	US$/t	0	
Exchange rate	USD:AUD	0.7	
Price – Ni	A$/t	32857	
Price – Co	A$/t	48571	
Selling cost - Ni	A$/t	821	
Selling Cost - Co	A$/t	1214	
Cut-off grade - Ni	%	0.22	
Cut-off grade - Co	%	0.15	

Table 3: *Parameters used for the RPEEE pit shell determination*

COMPARISON TO HISTORICAL MINERAL RESOURCE ESTIMATES

A-Cap completed a Mineral Resource estimate for Wilconi in January 2022 using a similar approach to the current Mineral Resource estimate but with 217 fewer holes. The 2022 Mineral Resource estimate is shown in Table 4 below for comparative purposes only.

Category	Cut-off	Tonnes (Mt)	Ni %	Co %	Ni Metal (Tonnes)	Co Metal (Tonnes)
Indicated	0.5	29	0.80	0.06	230,000	17,900
Inferred	0.5	62	0.70	0.05	430,000	28,500
Total		90	0.73	0.05	660,000	46,400

Table 4: *Summary of previous MRE*

Infill drilling in 2022 better defined the margins of the resource and reduced the overall tonnes while at the same time increasing the average nickel grade.

The Wilconi Project is a farm-in joint-venture project with Wiluna Mining Corporation Limited (ASX:WMC), with A-Cap earning 75% equity in the project under the terms outlined on 20 December 2018. The Company is continuing is negotiations with the Administrators of Wiluna Mining Corporation Limited[1] *for the 100% acquisition of the Wilconi Project.*

A-Cap Energy's Board has authorised the release of this announcement to the market.

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About A-Cap Energy

A-Cap Energy is an Australian resources company focused on the development of critical minerals serving the world's path to carbon net zero. Amid renewed global focus on nuclear energy, the company's flagship Letlhakane Uranium Project in Botswana hosts one of the world's top 10 undeveloped uranium resources – 365.7 million pounds of contained U_3O_8 (100ppm U_3O_8 cut-off). A-Cap's Wilconi Project, which represents the company's first nickel-cobalt laterite project interest, is being advanced in response to the significant growth expectation in the supply of battery materials to the OEM automotive and battery industries. The company aims to establish key strategic and commercial relationships to take advantage of material processing and refinery technologies according to the highest Environmental, Social and Governance (ESG) standards.

[1] ASX:ACB 25/May/23 A-Cap Energy position with Wiluna Mining in Administration.

Competent person's statement

Information in this report relating to mineral resources is based on information compiled by Mr Rowdy Bristol, a full time employee of Snowden Optiro and a Member of AusIMM. Mr Bristol has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and the activity he is undertaking to qualify as a Competent Person under the 2012 Edition of the Australasian Code for reporting Exploration Results Mineral Resources and Ore Reserves. Mr Bristol consents to the inclusion of the data in the form and context in which it appears.

Information in this report relating to exploration drill results, is based on information compiled by Mr Harry Mustard, a full-time employee of A-Cap Energy Limited and a member of the Australian Institute of Geoscientists (AIG). Mr Mustard has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person under the 2012 Edition of the Australasian Code for reporting of Exploration Results Mineral Resources and Ore Reserves. Mr Mustard consents to the inclusion of the data in the form and context in which it appears.

ACAP Energy

JORC Code, 2012 Edition – Table 1 report

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	Commentary
Sampling techniques	• The Wilconi database comprises 70 Auger (AUG) holes for 465m, 1,479 Aircore (AC) holes for 99,213m, 11,614 Rotary Air Blast (RAB) holes for 326,412m, 1,403 Reverse Circulation (RC) holes for 104,840m and 99 Diamond core (DD) holes for 11,550.4m. Of these 443 RC holes for 19,300m and 61 DD holes for 2815.4m were drilled by A-Cap from 2019 to 2022. • Samples used in this Wiluna Nickel-Cobalt Laterite resource estimate were restricted to 948 RC and DD holes, with many historical holes excluded owing to a lack of clarity on sampling methods, QA/QC and collar locations. • The drill results used in this report were from drilling undertaken by Amax Exploration (1972), Wiluna Mines Ltd (Wiluna Mines) 1998, CRA Exploration Pty Ltd (CRAE) 1992 -1997, Outokumpu Exploration Australia Pty Ltd (Outokumpu) 1998, Agincourt Resources Ltd (Agincourt) 2005 –2006, Independence Group NL (Independence) 2005 –2009, Oxiana Minerals (Oxiana) 2007 - 2008 and A-Cap Energy Ltd (A-Cap) 2019-2023. • RC drill holes were sampled and geologically logged on 0.5m, 1m or 2m intervals. Wiluna Mines, Independence and Oxiana used a combination of riffle splitters or spears for collecting a sub-sample of drill chips for analysis. A-Cap samples were collected at 1m intervals in 600mm x 900mm plastic bags under a rig mounted Metzke cyclone and cone splitter. Sub-samples for analysis were collected in numbered calico bags from the cone splitter attached to the base of the cyclone. Between 1 and 3 kilogrammes of sample was collected for analysis. The cone splitter was adjustable so that the size of split samples could be controlled. Other companies did not record their method of sampling RC chips, however, it is expected that industry-standard practices at the time were employed. • All A-Cap's sampling intervals were recorded in standard sample record spreadsheets. Sample condition and recoveries were recorded for all samples. • Diamond core sampling varied between 1m to 4m intervals, with selective sampling at narrower intervals to geological/ mineralisation boundaries. Independence drilling utilised 4m composites with subsequent 1m re-sampling through higher-grade zones. • Wiluna Mines (1998) used a diamond saw to cut core in half lengthwise for sampling. Although not recorded, it is expected that CRAE and all other later companies used a similar method. A-Cap used a diamond saw to cut core in half lengthwise where possible. In saprolite rock where the core was clayey and soft a spatula/paint scraper was used to split the core in half. • Sample preparation employed prevailing industry standard methods. • The diamond core sampling and RC methods are considered appropriate for the style of mineralisation.

Criteria	Commentary
Drilling techniques	• The Wilconi database comprises 14,156 holes with Ni assays, including 70 Auger (AUG) holes for 465m, 1,479 Aircore (AC) holes for 99,213m, 11,614 Rotary Air Blast (RAB) holes for 326,412m, 1,403 Reverse Circulation (RC) holes for 104,840m and 99 Diamond core (DD) holes for 11,550.4m. • Little information is available on drilling techniques for historical AC, RAB and RC drilling. However, much of this drilling was excluded from the database used for the resource model due to uncertainty in the sampling quality and collar locations. • Diamond core was typically NQ except for diamond drilling by A-Cap who used a larger diameter coring system (PQ) to improve recovery in the soft laterite profile. • RC drilling in 2019 by A-Cap was completed using a 146mm face-sampling bit attached to a down the hole hammer. • RC drilling in 2021 and 2022 by A-Cap used an Atlas Copco L8 RC rig with 1,000cfm at 435psi compressor with a 133mm diameter face sampling bit for holes WCN21RC001 –178 and a Schramm T4 rig using a 2,300cfm at 850psi compressor & booster with a 140mm face sampling bit for holes WCN21RC00179 – 443 • Diamond drilling conducted by A-Cap in 2021 (WCNDDH001 – 31) was completed using a Desco 7000 rig drilling PQ (85mm) sized core. Diamond drilling conducted by A-Cap in 2022 (WCNDDH32-61) was completed using a Boart Longyear LF90 drilling PQ (85mm) sized cores. The larger diameter cores were drilled to enable better recovery in soft, clayey material, commonly found in laterite deposits. • A-Cap's drill holes were designed to infill between lines of historical holes spaced 100 metres apart. The infill drilling closed up the drill spacing to 50 metre centres over shallower, better grade portions of the resource. • A-Cap's holes were shallow, ranging between 15m and 72m depth and averaged 44m depth. Most samples were dry, sometimes becoming moist or wet at the base of the deeper holes. • Upon completion, all A-Cap's drill holes were surveyed from the top to bottom of the hole at 5m intervals using a Reflex, north seeking Gyro.

Criteria	Commentary
Drill sample recovery	• CRAE recorded recoveries of all RC samples based on sample weights. Recoveries were typically in the order of 100%. • A-Cap weighed and recorded recoveries for each sample interval. Recoveries were typically better than 95%. In damp clay zones the Metzke sampling system on the L8 rig could get clogged and required cleaning on occasions. • Other historical sample recovery data has not been sighted. • In A-Cap's RC drill programmes, sample recoveries were considered good as nearly all samples were dry with only some fines lost out the top of the cyclone and around the outside of the hole (anulus). • Moist and wet samples were noted in the sample record sheets and drill hole lithology logs. <2% of samples were recorded as moist or wet. • All 1m samples were weighed to help assess recoveries. Some intervals returned lower than expected volumes but the lost material was often captured in the following sample. This occasional variability in sample weights may have been caused by clays temporarily restricting the return of sample to surface. • There is no known or reported relationship or bias between sample recovery and grade with the RC or diamond drilling.
Logging	• All company drill logs included colour, weathering, lithology, mineralogy, alteration and veining. In addition, Wiluna Mines drill logs included wet/dry sample records and magnetic susceptibility readings. • For A-Cap, all RC holes were logged in detail by geologists on site during the drill programme. Data was recorded for each 1m sample interval and included colour, hardness, lithology, texture, weathering and alteration minerals and intensity, fracture and vein mineral types and %, level of dryness i.e. dry, moist, wet. • Logging is both qualitative and quantitative depending on the criteria being logged. All holes were logged in their entirety. • Logging is appropriate for the stage of the project and sufficiently detailed to support further studies. • Representative chips from each 1m and drill hole interval were selected and placed in chip storage trays for future reference. All chip trays were photographed. • A-Cap diamond core logging was conducted by entering geological and geotechnical data directly into digital logging templates installed on field tablets. Cores were marked out at 1m intervals and criteria recorded included, core recovery, RQD index, hardness, structure/fracture type and density, grain size, weathering intensity, colour, lithology, mineralisation, alteration type and intensity. • For A-Cap cores, a 10cm to 20cm core specimen was selected every 1m interval for bulk density readings using an electronic hydrostatical balance.
Sub-sampling techniques and sample preparation	• RC and RAB samples were routinely composited in the field to 4 m, with zones of mineralisation subsequently resubmitted at 1m intervals. • Independence and Oxiana RC samples were tube-speared, Wiluna Mines used a combination of tube-spearing and riffle splitting of RC samples.

Criteria	Commentary
	• A-Cap one metre samples were recovered using a Metzke rig mounted cone splitter attached below a cyclone into a numbered calico bag. Sample target weight was between 2 and 3 kg. Sampling and splitting methods are unknown for other operators. Whether samples were wet or dry were recorded by Wiluna Mines and A-Cap. • For A-Cap, RC samples outside the mineralised intervals were combined into 4 x 1m composites the field. Hand held XRF readings were made to support the visual identification of the non-mineralised intervals. Composite samples were prepared by combining samples from the 1m green bags using a tube-spear. • Diamond drill sampling was predominantly half core and was cut lengthwise using a diamond saw. Historical core diameters were typically NQ, however A-Cap recovered larger diameter PQ cores to enhance recoveries. • A-Cap cores were cut lengthwise using a diamond saw where possible. In very soft, clayey intervals samples were split in half lengthways using a steel paint scraper. • A-Cap RC and core samples were analysed at ALS Perth, a NATA and ISO accredited lab. Sample preparation consisted of crushing the entire sample to 70% passing 2mm (CRU-21), followed by a 250g split pulverised to 85% passing 75 microns (PUL-24). • Agincourt, Independence and Wiluna Mines used either Amdel (Welshpool, Perth) for their geochemical analysis. ON occasions, Oxiana also used Genalysis, both ISO accredited labs. It is assumed that standard dual -stage crushing and pulverisation was employed prior to digest. • RAB and RC drilling is considered appropriate for first-pass exploratory and RC and DD are considered appropriate for resource definition drilling at Wiluna. • For Agincourt, RC sampling, either a blank was inserted or a duplicate prepared very 1 in 20 samples. Oxiana inserted standards or prepared duplicates every 12 samples. Nickel assays were within 5% of recommended standard values and cobalt assays within 15% of recommended values. • During RC and diamond drilling, A-Cap inserted standards, blanks or prepared duplicates were every 10th sample. Duplicate samples were collected every 30th sample during RC drilling using a Metzke sampling system (cyclone & cone splitter combination attached to the rig). For diamond cores, quarter cores were split off to make duplicate samples every 30th sample. Nickel duplicate assays were within 5% and cobalt assays were within 10%. Historical records of quality control for other RC/RAB/AC drilling have not been sighted however, it is expected that industry-standard practices were employed. • Duplicate sample analyses were within 10% for the main elements targeted. • Analysis of standards and blanks inserted were all within +/- 10% of the recommended value for the main elements targeted. • Sample sizes are considered appropriate for the grain size of the material being sampled and the nature of mineralisation.

Criteria	Commentary
Quality of assay data and laboratory tests	• The project has a 50-year history since discovery which has included being managed by numerous companies. The changes in ownership mean that much of the past work, particularly prior to 1990, has often been poorly documented or archived. • For CRA drilling, the laboratory used was Analabs, the method is not recorded. For Agincourt drilling the lab was Amdel and technique ICP, with parts per million accuracy. For Independence drilling, samples were analysed by Amdel using four acid digest and ICP/OES finish (technique ICP102) to part per million accuracy. Oxiana had samples analysed at Amdel by XRF at 0.001 % accuracy and Genalysis by ICP to ppm accuracy. A-Cap used ALS (Perth) and had samples analysed using a 4 acid digest with ICP-MS finish (48 elements) to ppm accuracy. These are considered to be industry-renowned labs using standard analytical methods for this style of mineralisation. The ICP techniques used are considered to be a near total (95% to 99%) digest. • ALS (Perth) method ME-XRF12n (16 standard elements + Loss on Ignition) was used for the 2021 -2022 A-Cap drilling campaigns. Scandium was included for a small number of drill holes. This normalized XRF method utilises a 0.7g fused disc and is considered to be a total digest. • ALS also ran their own laboratory internal checks via repeat analyses, standards and blanks. • No data from geophysical tools or hand-held assay devices have been reported. • Agincourt inserted a blank or collected a duplicate sample every 20th sample. Blanks showed consistently low and precise cobalt and nickel values. Duplicate samples showed reasonable correlation. Oxiana inserted standards or prepared duplicates every 12 samples. Nickel assays were within 5% of recommended standard values and cobalt assays within 15% of recommended values. Oxiana duplicate samples showed a range from good to poor correlation. • Duplicate sample analyses were within 10% for the main elements targeted. • Internal ALS laboratory standards and repeats demonstrated a high level of accuracy and precision in the analysis. • For the four hole RC programme drilled in 2019, A-Cap inserted standards, blanks or a duplicate sample every 20th sample. Duplicate samples were collected at the same time using a Metzke sampling system attached to the RC rig. Nickel duplicate assays were within 5% and cobalt assays were within 10%. Blanks samples (OREAS 22d) all returned extremely low Ni and Co values and had good precision to the recommended blank values. A-Cap inserted 2 Ni & Co standards in the RC stream (OREAS73a & 45p). Assays of the standards were all within 5% of the recommended values. • For the 2021 & 2022 RC and DD programmes A-Cap inserted a blank, standard or duplicate every 10th sample. • For the 2021 RC and DD programmes geostat standards included GBM908-8, GBM309-6, GBM315-1, GBM315-2 and GBM913-3 (blank) were certified for 4 acid digest -ICP assay methods, with XRF typically returning Ni & Co assays ~5% higher than the certified value. ICP check assays on pulp duplicates by ALS were 7% lower for Ni and 4% lower than the corresponding XRF assays. A small number of sample submission issues were identified i.e. blanks submitted in error for CRM's. • For the 2022 RC and DD programmes Ni standards certified for XRF assay methods were used (OREAS180, OREAS183 & OREAS192). All assays of the standards were within 5% of the certified value for the main metals targeted.

Criteria	Commentary
Verification of sampling and assaying	• A-Cap Energy geological personnel and independent consultants have validated the database from paper records where possible primarily A-Cap and CRA records. Verification of sampling methods and assaying for older (pre-1990) historical databases has not been possible. • Significant intercepts for A-Cap's RC drilling has been verified by independent consultants by downloading assay results directly from ALS. • Scissored drill holes (pairs of holes drilled in opposing directions) are present on multiple sections. • RC drilling in 2019 conducted by A-Cap involved the twinning of 4 historical (1995 CRAE RC holes). Intercepts of the twinned holes possessed a good match as shown in following table.

CRA HoleID	From	To	Int (m)	Co %	Ni %	ACAP Hole ID	from	to	int (m)	Co %	Ni%
95WJV P128	27	35	8	0.09	0.69	AEWRCM 003	26.5	30.5	4.0	0.09	0.78
95WJV P140	6	14	8	0.17	0.99	AEWRCM 004	4.5	12.5	8	0.16	1.01
95WJV P227	42	54	12	0.12	0.73	AEWRCM 002	42	50	8	0.17	0.82
95WJV P260	27	39	12	0.23	0.6	AEWRCM 001	25	34	9	0.17	0.67

- For A-Cap RC drilling primary log data was recorded on hard copy logs in the field. Field log data was entered into an excel template on a laptop computer using lookup codes. For core logging, data was directly entered into tablets with lookup tables to prevent errors. All A-Cap data was sent for validation and compilation using acQuire software.
- Historical data collection procedures are not well documented. Historical annual reports submitted to DMIRS have been obtained from the WAMEX website. Scanned and digital copies of drill logs of RAB, RC and DD holes completed by Amax, CRAE, Delhi and Wiluna Mines, Oxiana and Independence group (IGO) were assessed.
- A study conducted by A-Cap on the comparison of recent XRF analyses compared to historical ICP methods showed a 4.7% increase in Ni assays and 5.2% increase for cobalt assays. The study showed that historical ICP assaying underestimated the actual grade. A-Cap performed XRF analyses on 268 historical ICP samples of low to high grade ores across the entire deposit. Snowden Optiro evaluated the data and agreed to apply a factor of 1.047 to nickel ICP assays and 1.052 to all cobalt ICP assays.

Criteria	Commentary
Location of data points	• The bulk of historical holes were located along grid lines surveyed by theodolite. Many of the historical holes have been identified in the field, picked up by GPS and the historical grids translated into MGA'94 zone 51. More recent drill hole collars (post 1990) have coordinates recorded to cm or mm scale suggesting collars were picked up using DGPS. • All A-Cap drill holes have been surveyed by a professional using real time differential DGPS to cm accuracy. Once completed, all A-Cap drill holes were surveyed from top to bottom at 5m intervals using a Reflex, north seeking gyro. • Holes drilled by Wiluna Mines were surveyed downhole by a Reflex multishot instrument. Agincourt, Independence and Oxiana used an Eastman single shot down hole camera to survey the collar and base of their drill holes. • In August 2021 A-Cap completed a LiDAR survey over the entire resource area. This surface was used to adjust elevations of historical holes. • The grid system for the Wiluna Nickel Project is Map Grid of Australia GDA 94, Zone 51. • A DGPS survey of drill hole collar locations is considered sufficiently accurate for reporting of resources, but is not suitable for mine planning and reserves.
Data spacing and distribution	• The spacing of the drill holes varies from 100m spacings along lines 400m apart (along strike) down to 25m by 50m centres. Recent drilling by A-Cap was designed to increase the drill hole density of the near surface, better grade portions of the resource to 50m x 50m drill spacings. • This drill spacing is considered sufficient to establish confidence in geology and grade continuity between the holes to enable a mineral resource estimate with the resource classifications applied. • Sample compositing outside of the mineralised intervals was conducted.
Orientation of data in relation to geological structure	• Drill holes were angled to match orientations of previous drilling and to cover the possibility of steep dipping structures being present that may focus deeper laterite development i.e. mineralised "keels". • Drilling has been done along lines perpendicular to the strike of the mineralisation and host ultramafic unit. The nickel bearing ultramafic unit has been defined by drilling and geophysical surveys. • Angled holes (-60˚) have been drilled at a high angle to the mineralisation which is known to be broadly horizontal. The down hole intercept widths maybe 15% longer than true widths, however there is not considered to be any bias in grade.

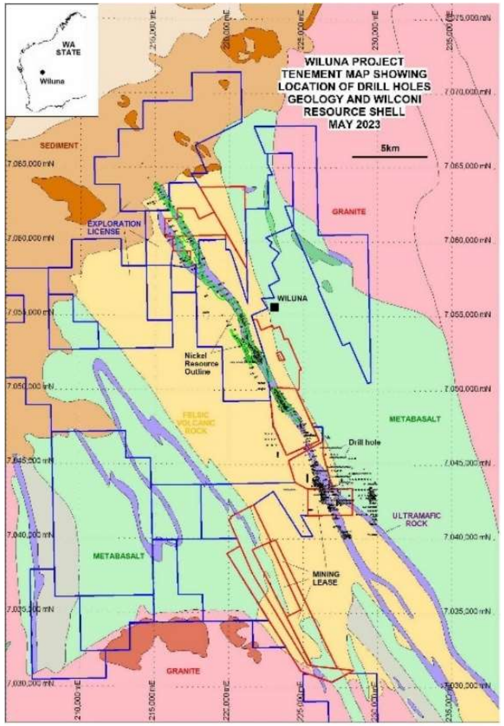
Criteria	Commentary
Sample security	• There is no documentation on sample security for the historical drilling. • For A-Cap samples, once a drill hole was completed all selected 1m calico samples and 4m composites were immediately bagged in polyweave bags and zip tied ready for shipment. Samples were always under the care and supervision of A-Cap geologists until samples were loaded onto trucks for shipment to ALS Perth laboratory by A-Cap personnel. Upon receipt ALS verified sample numbers against the sample submission sheet/manifest, and confirmed receipt. After verification the samples were bar coded and tracked through the entire analytical process.
Audits or reviews	• Drilling and sampling methods have been inspected on site by independent consultants. The methods are considered suitable for the style of mineralisation being tested. Snowden Optiro validated the drill hole database using Surpac software. Several overlapping samples were found and removed.

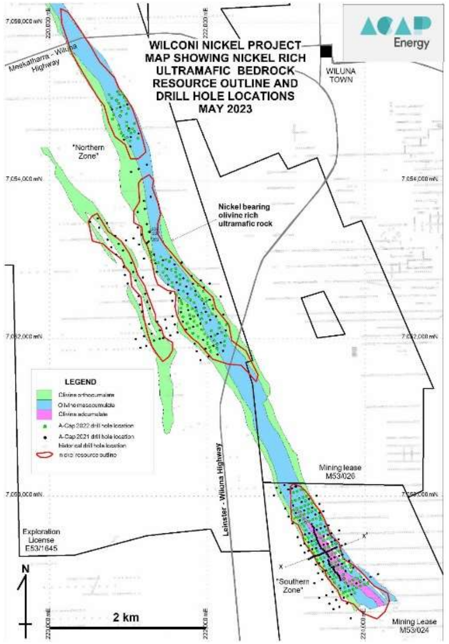
Section 2 Reporting of Exploration Results

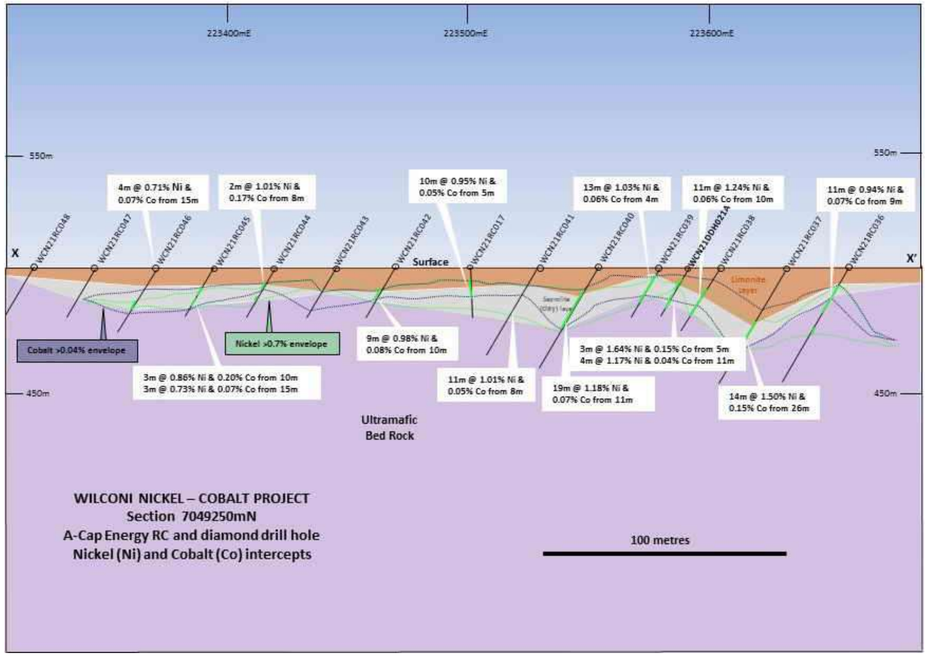
(Criteria listed in the preceding section also apply to this section.)

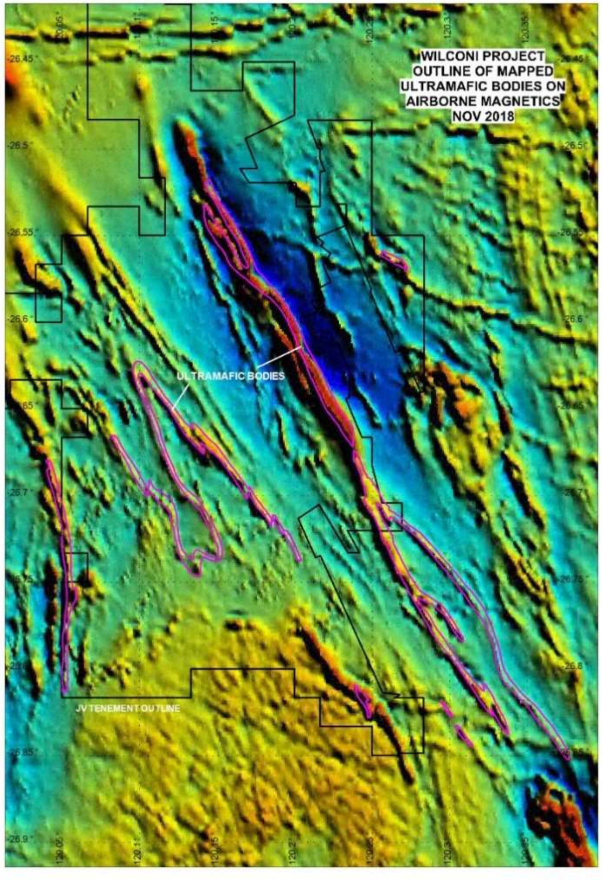
Criteria	Commentary
Mineral tenement and land tenure status	• A-Cap Energy Ltd and Wiluna Mining Corp. have entered into a definitive Farm-in and Joint Venture Agreement (JVA). • Tenements in the JVA consist of the following exploration tenements: E53/1794, E53/1645, E53/1908, E53/1803, E53/1864, E53/2048, E53/1852, E53/2050, E53/1791, E53/1853, E53/1912, E53/2054, E53/2053, E53/2076, R53/0001. • Tenements in the JVA consist of the following mining leases: M53/0092, M53/0139, M53/0026, M53/0024, M53/1098, M53/0049, M53/0071, M53/00131, M53/00034, M53/00052, M53/00041, M53/00188. • All the JVA tenements are held in the name of Kimba Resources Pty Ltd and Matilda Operations Pty Ltd both companies are subsidiaries of Wiluna Mining Corp. All tenements are current except exploration licenses E53/2053, E53/2054, E53/1803, E53/1864, E53/2048 and E53/2050 which are pending grant. • Most tenements are contiguous and cover an 747 km² area around the town of Wiluna. • Franco Nevada Australia Pty Ltd hold a 2% net smelter return royalty over nickel metal produced from the existing mining leases only. • The tenements are located on the traditional lands of the Tarlka, Matuwa and Piarku people (NTA ID WR2016/001). Wiluna Mining Corp. currently have an agreement with the traditional owners that requires any areas within the JVA tenements be cleared by cultural heritage survey prior to any surface disturbance. • There are no known impediments to obtaining a license to operate in the area outside of standard landholder, traditional owner and Western Australia Department of Mines & Petroleum (DMP) regulations.
Exploration done by other parties	• Delhi 1968 conducted initial costeaning and sampling for Ni gossans and Kambalda type Ni sulphides. Numerous assays >2% Ni were returned from laterite. Kennecott 1969-1972 completed further soil sampling and pitting which identified coincident Ni+Cu anomalies. This was followed up by a percussion drilling program that covered several kilometres of strike length with 850 holes to a typical depth of 10-15m, which confirmed the previously identified soil geochemical targets. • Kennecott conducted extensive RC drilling of the laterite profile, which has subsequently formed part of the laterite Ni resource. Kennecott followed up by drilling 2 diamond holes, which from the sections and plans it appears have failed to test the targeted ultramafic basal contact, due to structural complexity. Despite failing to directly detect the targeted Mount Keith-style mineralisation, this drilling does not preclude the possibility that some laterite Ni mineralisation has resulted from weathering of an underlying Ni sulphide body • During 1973-1976 WMC followed up with IP and EM geophysical surveys and drilled 4 further percussion holes and 1 diamond hole testing the resulting anomalies. There are no significant assays reported and the source of geophysical anomalism was attributed to variably massive and disseminated pyrrhotite and pyrite logged in association with amphibolites.

Criteria	Commentary
	• In 1993-4 the CSIRO and Asarco Australia conducted mapping and petrographic analysis of ultramafic rocks at several prospects. These researchers recommended further drilling to determine whether the Perseverance ultramafics were extrusive or intrusive as per the high-energy extrusives / sub-volcanic intrusives around Agnew - Leinster, and therefore prospective for Ni sulphide deposits. • In 1995 Wiluna Mines intersected Ni sulphide and PGE mineralisation of up to 2m @ 2.15%Ni + 1g/t Pd+Pt from 74m in hole 95WJVP251 at Bodkin prospect. The massive sulphide is located within an interpreted thermally eroded footwall basalt unit. This was the first recorded massive sulphide occurrence in the Perseverance ultramafics and has major implications for the prospectivity of the immediate Bodkin area and the wider ultramafic stratigraphy. (Wiluna Mining Corp, Wiluna Nickel Project- Information Memorandum Oct 2014). • Between 1992 and 1997, CRA in joint venture with Wiluna Mines drilled 372 holes (mostly RC) totalling 41,273 metres over the extent of the ultramafic units. Much of the data collected from this drilling has been used in the JORC nickel laterite resource estimates completed by Snowden for Agincourt Resources in 2005 and by Mining Plus for A-Cap Energy in 2019.
Geology	• The Wilconi project is located on the north eastern edge of the Archaean Yilgarn Block, in the Wiluna Greenstone Belt. The Wiluna Greenstone Belt can be divided into two metamorphic domains, the Wiluna domain in the east and the Matilda domain in the west. The major north west trending Perseverance Fault separates the domains. • The Wiluna domain is a low grade, prehnite-pumpellyite facies, metamorphic terrain comprising mafic to ultramafic lavas with intercalated sedimentary units, felsic volcanics and dolerite sills overlain by a thick pile of felsic volcanics, tuffaceous sediments, and sedimentary rocks, interrupted by extrusion of a large volume of komatiitic lava. Primary igneous textures and structures are well preserved, and deformation is predominantly brittle. • The Matilda domain is a medium to high grade, greenschist to lower amphibolite facies, metamorphic terrain with predominantly ductile deformation. It consists of a volcano sedimentary sequence in an interpreted major northwest trending synclinal structure, with the axis close to the Perseverance Fault. The sequence comprises basal banded iron formation in the west, overlain by komatiitic volcanics with limited basal peridotite members. These grades upwards into high magnesium basalt and basalt with interflow chert and graphitic sediments. Metabasalt predominates in the project area. Felsic volcanic rocks and sediments are interpreted to form the core of the syncline. • A number of granite plutons intruded both domains during the very latest stages of volcanism, or the earliest stages of subsequent compressional deformation and regional metamorphism. Emplacement was essentially along the contact between the greenstones and the unknown substrate. • Exposure at the Wiluna Nickel-Cobalt Project ground is virtually non-existent and the geology of the Wiluna ultramafic rocks has been largely determined from previous drilling results aided by an interpretation of magnetic surveys. Approximately 10km northwest of Wiluna the ultramafics are buried under Proterozoic cover. • Drilling has shown that the ultramafics form the base part of a differentiated igneous intrusion which is represented by serpentinised dunite, serpentinised peridotite, pyroxenite and gabbro. The intrusion appears to be conformable or slightly discordant and is thought to have been emplaced as a dyke or sill. • Near Wiluna, this ultramafic unit is between 200-300m wide at the surface but thins rapidly south to less than 100m at the surface before disappearing under the surficial cover. The ultramafic rocks are dislocated by a number of faults trending north and northeast.

Criteria	Commentary
	• Nickel – cobalt mineralisation is concentrated in laterite profiles developed over units of the Perseverance ultramafic sequence. Previous drilling has shown that the mineralisation forms a thin, generally <10m thick laterally extensive blanket. Where cut by steep structures, intense lateritisation and mineralisation can extend down to 100 metres depth. • From the top of the profile magnesium levels typically increase from less than 1% to 20% at the saprock interface. This typically occurs within approximately 6 metres allowing an Mg discontinuity surface to be easily identified. This discontinuity is a redox front which forms between the reduced water table and the overlying oxidised saprolite. In many locations the nickel and cobalt peak values occur above this surface. 
Drill hole Information	• See Appendix 1.

Criteria	Commentary
Data aggregation methods	• Appendix 1 includes all drill hole intercepts used for the Wilconi Mineral Resource Estimate based that fall within the 0.5% Ni mineralised shell. No cutting of high grades were done for these calculations. • Metal equivalents were not used.
Relationship between mineralisation widths and intercept lengths	• The Laterite is flat lying and drilling is either vertical or at a 60 degree angle. The intersections are a reasonable approximation of the mineralization thickness.
Diagrams	 Plan showing nickel rich ultramafic bedrock, location of A-Cap's 2021 & 2022 drill holes, historical holes, outline of the nickel resource and location of section X – X'.

Criteria	Commentary
	 Cross section X – X' showing nickel and cobalt intercepts from A-Cap's 2021 and 2022 infill drill programmes. The Ni - Co mineralisation forms a flat-lying zone, close to surface, concentrated where weathering of the ultramafic bedrock is most intense.
Balanced reporting	• The large volume of data makes reporting of all exploration results is not practical. All drill hole intercepts have been reported in previous ASX reports (See ASX release 23rd Nov 2022 and 24th Sept 2021). • The plan and sections shows holes with and without significant intercepts.
Other substantive exploration data	• Ultramafic units in the Wiluna region are strongly magnetic and show up as conspicuous linear magnetic highs in the ground and airborne magnetic survey data (see Figure). The magnetic data highlights the continuity of the ultramafic units over which the cobalt and nickel rich laterite deposits are developed.

Criteria	Commentary
	
Further work	• Future work will consist of closer spaced drilling in areas where drill holes are sparse to upgrade the resource from inferred and indicated, to indicated and measured. • More density measurements should be taken with the aim of reducing the risk in the estimated tonnages.

Criteria	Commentary
	• Other work planned as part of the DFS includes: Cultural heritage surveys, design and geotechnical assessment of constructed landforms including waste dumps, open cuts and tailings storage facilities, soil, waste rock and tailings characterisation studies, noise and greenhouse gases assessment.

Section 3 Estimation and Reporting of Mineral Resources
(Criteria listed in Section 1 and where relevant in Section 2, also apply to this section.)

Criteria	Commentary
Database Integrity	• The original Wiluna Ni Co drill hole database was acquired from Wiluna Mining Corporation (ex Blackham Resources) as part of the JV process. The bulk of this drill hole data (of which only parts were used in this mineral resource estimate) was collected by CRA between 1992 and 1997. Hard copies of the all the original log sheets and assays for this drilling has been obtained and reviewed by A-Cap and independent consultants. No discrepancies have been encountered in the data. • Most of the CRA drill hole collars can still be identified in the field and match their listed coordinates. • Drill hole geology and assay data have been viewed in plan, section and 3D to identify any discrepancies in the data. • 2021 and 2022 drilling information has been added to the original Wiluna Ni Co drill hole database after internal validation by A-Cap, and external validation by independent consultants. • Snowden Optiro undertook some additional validation checks after importing the data into Surpac software. These checks included, missing assays and collars, below detection limit values, overlapping and duplicated sample intervals, comparison of geology and assay depth against collar end of hole depths. Several overlapping samples were found and removed. Laboratory error codes for lost or missing samples were modified in the estimation drillhole file to absent. It is assumed that missing samples within mineralisation zones represent lost or insufficient volume samples rather than a conscious decision not to assay; as such they have not been replaced with default low grades.
Site Visits	• The competent person has managed the exploration and drilling at Wilconi and has visited the site on numerous occasions. • The competent person has reviewed the sampling, analytical methods, QA/QC procedures and the database. • The competent person for the MRE has not visited the site.
Geological Interpretation	• The confidence in the geological interpretation of the mineral deposit is high. Mineralisation consists of supergene enrichment of nickel and cobalt formed during lateritisation of an ultramafic protolith. • Hundreds of holes drilled through mineralisation into fresh basement rock have provided a good understanding of the geology. • Magnetic surveys of the highly magnetic ultramafic rocks help to confirm continuity between drill sections. • The current resource estimate used detailed modelling of the regolith and ore types including overburden, limonitic saprolite, saprolite and saprock ores and fresh bedrock lithologies. • The flat-lying blanket of enriched nickel and cobalt mineralisation generally overlies ultramafic rocks but can extend beyond the margins of the ultramafic units. This feature is thought to be caused by the lateral movement of nickel and cobalt bearing solutions along the water table. • Mineralisation can be found at surface or down to 100m depth. In many places the mineralised zone has been buried by Tertiary age

Criteria	Commentary
	sediment. The ultramafic body is layered and known to be composed of a variety of mineral cumulate phases. Better grade mineralisation is often found overlying olivine rich adcumulate layers. • The thickness of the mineralised zone is generally relatively constant but has been shown to suddenly thicken, forming “keels” in some drill holes, thought to reflect deeper lateritisation of the ultramafic unit along steep structures. More work is required to determine how significant these structures are.
Dimensions	• The nickel and cobalt mineralisation that hosts the Wilconi deposit has a strike length of 19km and is up to 1300m in width. The average thickness of the mineralisation is 12m. The zone of mineralisation is open along strike.
Estimation and modelling techniques	• Drillhole data was composited downhole to 1 m intervals prior to geological modelling, statistical analysis, variogram modelling, and block grade estimation process. • Three-dimensional wireframes were created using Leapfrog from Ni and Co drill hole composite assays. Separate wireframes were constructed for Ni>0.25%, Ni>0.5%, Ni>1.0% and Co> 400 ppm and were used as estimation domains. • Composites within each of the mineralised domains were analysed to ensure that the grade distribution was indicative of a single population, with no requirement for additional sub-domaining, and to identify any extreme values which could have an undue influence on the estimation of grade within the domain. • Hard boundary conditions were applied for grade estimation within each of the domains. • Variography for the mineralised domains was completed in Supervisor V8.15 using normal scores transformed data, with the variogram model back-transformed prior to grade estimation. • A range of block sizes was reviewed, and a parent cell block size of 50mE by 50mN by 1 mRL was selected. This block size represents approximately half the drill spacing in regions containing the Measured and Indicated material. The block model was constructed in Surpac v2023 software. Grade estimation was completed using ordinary kriging (OK) of the 1.0m composited samples. • The model was validated by: (1) comparing the wireframe volumes with block model volumes; (2) comparing the mean input composite grade with the estimated block grade; (3) visual comparison of the drillholes and blocks, and ; (4) examining trend plots of the input data and estimated block grades.
Moisture	• Tonnages are reported on a dry basis.
Cut-off parameters	• Ni and Co prices assumed for the Mineral Resource are $23,000/t and US$34,000/t respectively, with an assumed exchange A$/US$ rate of 0.70. • The Mineral Resource is reported above a pit defined as the 0.22% nickel equivalent grade which was selected to represent the portion of the resource that may be considered for eventual economic extraction by open pit mining methods.

Criteria	Commentary
	• At A-Cap's request, the tonnes and grades are reported for blocks where the nickel grade is greater than 0.5%. Given the stage of the Project and classification applied to the Mineral Resource, the cut-off grade is considered reasonable. • The 0.5% Ni cut-off grade will require confirmation through feasibility work.

Mining factors or assumptions	• It is assumed that mining will be by bulk open pit methods commensurate with the blocks sizes employed in the resource model.
	• The parameters used to define the pit containing material with a reasonable probability of economic extraction (RPEEE) were:
	  • US$23,000/t Ni and US$34,000/t Co prices
	  • A$:US$ exchange rate of 0.70
	  • Ni and Co recoveries of 90%
	  • Mining cost of A$5/t
	  • Processing cost of A$55.30/t ore
	  • General and administration (G&A) costs of $5.75/t ore
	  • Royalties of 2.5% for Ni and 2.5% for Co
	  • Mining dilution of 5%
	  • Mining recovery of 95%
	• Overall slope angles of 45.7 degrees Mining, processing, and G&A costs as well as metal recoveries are consistent with other Ni laterite projects in Australia that have been publicly reported on the ASX.
	• The parameters above are preliminary in nature and are subject to confirmation by feasibility work on the project.

Metallurgical factors or assumptions	• An approximate metallurgical recovery of 90% has been assumed for both nickel and cobalt in determining reasonable prospects of eventual economic extraction and for the calculation of a nickel equivalent formula. Simulus labs have identified an average metallurgical recovery of 93% Ni and >91% Co using a High Pressure Acid Leach bench test (A-Cap ASX Release 30th January 2023). • Atmospheric leach (>77% Ni & >71% Co) and acid bake (>66% Ni & >76% Co) methods also showed high metal recoveries (A-Cap ASX Release 30th January 2023).
Environmental factors or assumptions	• To the best of Snowden Optiro's knowledge, at the time of estimation there are no known environmental, permitting, legal, title, taxation, socio-economic, marketing, political or other relevant issues that could materially impact the eventual extraction of the Mineral Resource.
Bulk Density	• Bulk density was measured for 429 physical core samples in ore and 1040 waste/low grade core samples using the Archimedes water immersion method. The core samples are being used in the MRE. Downhole geophysical density readings collected by Abims Solutions

Criteria	Commentary
	(ABIMS) were used as a check for the densities.
Classification	• Resource classifications were defined by a combination of data including; drillhole spacing, geological confidence, and mineralisation continuity of domains. • Further considerations of resource classification include; data type and quality (drilling type, drilling orientations, down hole surveys, sampling and assaying methods); geological mapping and understanding; bulk density, statistical performance. • Measured mineral resources have been applied to the Wiluna deposit at a nominal drill spacing of 50 m x 50 m. • Indicated material has been applied to the Wiluna deposit at a nominal drill spacing of 50 m x 100 m. • Inferred mineral resources have been applied at drill spacings up to 100 m x 400 m. • The Competent Person considers the applied resource classifications to be appropriate for the Wiluna deposit.
Audits or reviews	• The Mineral Resource estimate was internally peer reviewed by Snowden Optiro and modifications made where appropriate.
Discussion of relative accuracy/confidence	• The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code. • Historical drilling forms a large part of the data used to calculate the Inferred areas of the Mineral Resource estimate. • Further drilling should enable the development of more robust geological and mineralisation interpretations and geostatistical analysis, and upgrade Inferred resources to Indicated. • Historical QA/QC procedures associated with this drilling is not available to form a view on their reliability. However, infill drilling by A-Cap in measured and Indicated areas of the Mineral Resource estimate indicates that a material bias is unlikely. • More density measurements should be taken with the aim of reducing the risk in the estimated tonnages, and potentially estimating density using ordinary kriging. • Undertake QAQC on density data, including the use of a density standard and umpire checks at an assay laboratory. • The cut-off used to determine the Mineral Resources was based on assumed mining and metallurgical factors that are preliminary in nature and require confirmation through feasibility work. • The statement relates to the global estimates of tonnes and grade. There is no production data to make comparisons.

Appendix 1

Wilconi Drill Hole Intercepts within the 0.5 % Nickel shell

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
92WJVD001	216010.69	7062520.90	503.73	248.46	-60	232	39	49	10	0.050	0.79
92WJVD002	215188.43	7063425.57	527.04	248.46	-60	375.2	28	30	2	0.064	0.65
92WJVP002	215908.24	7062458.95	508.94	248.46	-60	119	31	45	14	0.065	0.98
92WJVP004	215473.36	7063131.52	510.79	248.46	-60	119	36	50	14	0.049	1.00
92WJVP005	215588.88	7063188.96	522.72	248.46	-60	116	25	35	10	0.07	1.04
92WJVP007	215292.82	7063483.98	531.01	248.46	-60	119	10	38	28	0.027	0.65
92WJVP009	215379.72	7063067.67	518.51	248.46	-60	119	33	35	2	0.031	0.62
92WJVP010	215147.14	7063865.27	542.49	248.46	-60	119	21	33	12	0.073	1.05
95WJVP054	220912.55	7052999.24	450.77	248.46	-60	123	60	67	7	0.105	0.66
95WJVP058	221362.10	7053179.71	456.95	248.46	-60	117	50	65	15	0.110	1.04
95WJVP061	220324.58	7053630.52	474.63	248.46	-60	159	33	39	6	0.101	0.76
95WJVP062	220439.96	7053676.06	482.12	248.46	-60	99	27	29	2	0.053	0.57
95WJVP066	221130.84	7053948.79	454.23	248.46	-60	111	59	67	8	0.043	0.75
95WJVP067	221242.96	7053993.05	455.49	248.46	-60	99	59	65	6	0.041	0.69
95WJVP073	220800.70	7054678.83	493.89	248.46	-60	75	15	27	12	0.032	0.57
95WJVP074	220912.83	7054723.09	494.55	248.46	-60	75	11	29	18	0.036	0.63
95WJVP075	220989.60	7054753.40	463.47	248.46	-60	123	28	82	54	0.057	1.09
95WJVP077	219286.00	7056662.02	460.86	248.46	-60	96	44	80	36	0.074	1.06
95WJVP079	219526.99	7056757.15	494.50	248.46	-60	87	22	26	4	0.035	0.51
95WJVP082	220149.29	7056142.43	481.71	248.46	-60	201	33	43	10	0.026	0.53
95WJVP085	218562.75	7057236.89	457.47	248.46	-60	99	57	73	16	0.070	0.90
95WJVP087	218680.92	7057283.53	470.75	248.46	-60	99	49	53	4	0.026	0.60
95WJVP092	218164.70	7057940.12	472.92	248.46	-60	75	47	51	4	0.025	0.65
95WJVP094	217405.62	7058500.85	517.99	248.46	-60	81	8	10	2	0.017	0.6
95WJVP096	217966.70	7058722.32	480.69	248.46	-60	105	34	52	18	0.036	0.69
95WJVP097	218073.70	7058764.57	471.89	248.46	-60	99	51	55	4	0.050	0.94
95WJVP102	217669.13	7059465.24	477.11	248.46	-60	117	44	58	14	0.086	0.88
95WJVP103	217771.95	7059505.83	469.28	248.46	-60	117	57	63	6	0.06	0.77
95WJVP106	216637.43	7059918.34	495.40	248.46	-60	81	36	38	2	0.051	0.58
95WJVP107	216748.62	7059962.24	493.80	248.46	-60	99	29	47	18	0.035	0.66
95WJVP108	217175.24	7060130.64	489.66	248.46	-60	99	35	47	12	0.056	0.70
95WJVP109	217285.51	7060174.16	486.75	248.46	-60	117	30	58	28	0.038	0.33
95WJVP110	217383.67	7060212.92	470.23	248.46	-60	117	58	68	10	0.133	1.13
95WJVP117	216951.66	7060902.74	486.01	248.46	-60	111	43	57	14	0.045	1.23
95WJVP118	217047.49	7060940.59	473.75	248.46	-60	117	53	75	22	0.046	0.67

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
95WJVP121	220456.62	7055403.38	510.75	248.46	-60	110	2	16	14	0.027	0.78
95WJVP122	220567.81	7055447.27	513.31	248.46	-60	129	6	14	8	0.189	0.78
95WJVP123	220663.19	7055484.92	478.95	248.46	-60	111	44	46	2	0.027	0.55
95WJVP127	221216.53	7052261.87	466.35	248.46	-60	99	27	57	30	0.107	0.95
95WJVP128	221603.60	7052414.67	477.50	248.46	-60	81	29	31	2	0.136	0.63
95WJVP129	221706.89	7052455.44	463.02	248.46	-60	99	37	59	22	0.170	1.30
95WJVP130	221819.94	7052500.07	465.38	248.46	-60	99	38	52	14	0.071	0.96
95WJVP131	221937.18	7052546.35	475.60	248.46	-60	73	31	35	4	0.059	0.66
95WJVP132	222044.65	7052588.77	467.52	248.46	-60	99	38	46	8	0.032	0.56
95WJVP133	223151.62	7049584.27	481.84	248.46	-60	81	18	20	2	0.096	0.61
95WJVP134	223269.32	7049630.73	487.22	248.46	-60	93	12	20	8	0.064	0.72
95WJVP135	223373.53	7049671.87	470.05	248.46	-60	93	12	52	40	0.036	0.50
95WJVP139	223659.46	7048924.37	495.50	248.46	-60	93	4	14	10	0.082	0.73
95WJVP140	223768.33	7048967.34	488.13	248.46	-60	99	6	24	18	0.094	0.89
95WJVP143	224023.65	7048637.95	483.72	248.46	-60	93	15	29	14	0.050	0.96
95WJVP144	224134.38	7048681.66	480.30	248.46	-60	87	12	36	24	0.053	0.87
95WJVP145	224249.75	7048727.20	483.51	248.46	-60	44	12	20	8	0.017	0.67
95WJVP149	220681.22	7055059.81	497.94	248.46	-60	99	12	24	12	0.091	0.82
95WJVP150	220783.30	7055099.30	493.71	248.46	-60	105	10	37	27	0.041	0.81
95WJVP151	220891.06	7055144.69	468.87	248.46	-60	99	50	52	2	0.027	0.54
95WJVP153	220235.04	7055799.87	509.29	248.46	-60	99	5	15	10	0.065	0.63
95WJVP154	220337.91	7055851.23	500.15	248.46	-60	105	10	32	22	0.033	0.60
95WJVP160	218931.13	7056952.12	455.01	248.46	-60	123	67	71	4	0.024	0.62
95WJVP161	219034.41	7056992.89	439.79	248.46	-60	129	76	98	22	0.032	0.69
95WJVP172	216473.76	7060283.92	500.17	248.46	-60	99	28	38	10	0.062	0.64
95WJVP175	217043.68	7060508.88	485.63	248.46	-60	99	41	55	14	0.06	1.10
95WJVP176	217156.27	7060553.33	487.14	248.46	-60	111	42	50	8	0.038	0.87
95WJVP185	216782.87	7061266.31	482.28	248.46	-60	141	49	65	16	0.03	0.71
95WJVP193	220659.46	7053332.53	461.24	248.46	-60	111	49	55	6	0.091	1.02
95WJVP196	221312.06	7053588.57	450.26	248.46	-60	129	59	75	16	0.076	0.84
95WJVP197	221430.91	7053635.12	463.55	248.46	-60	111	47	57	10	0.048	1.00
95WJVP200	221097.99	7052645.26	468.63	248.46	-60	99	32	50	18	0.030	0.66
95WJVP202	221411.55	7052769.04	481.28	248.46	-60	105	19	35	16	0.042	0.77
95WJVP204	221515.77	7052810.18	466.41	248.46	-60	99	40	50	10	0.058	0.79
95WJVP205	221626.96	7052854.07	467.00	248.46	-60	99	36	52	16	0.041	1.16
95WJVP207	221156.61	7052668.39	473.84	248.46	-60	99	22	48	26	0.07	0.86
95WJVP208	221369.50	7051892.07	458.93	248.46	-60	111	40	58	18	0.101	1.03
95WJVP209	221480.22	7051935.78	457.21	248.46	-60	105	43	59	16	0.058	0.73
95WJVP211	221959.41	7052124.94	467.76	248.46	-60	99	35	47	12	0.058	1.06

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
95WJVP212	222072.47	7052169.57	471.34	248.46	-60	111	35	41	6	0.137	1.06
95WJVP213	222189.24	7052215.66	480.73	248.46	-60	99	17	37	20	0.048	0.80
95WJVP216	223063.32	7049979.60	442.40	248.46	-60	111	40	86	46	0.040	0.51
95WJVP217	223185.21	7050027.71	460.64	248.46	-60	99	35	47	12	0.052	0.74
95WJVP219	223435.31	7049266.07	489.81	248.46	-60	105	11	19	8	0.080	0.56
95WJVP220	223545.58	7049309.60	482.84	248.46	-60	105	10	26	16	0.046	0.82
95WJVP221	223648.86	7049350.37	464.75	248.46	-60	93	28	44	16	0.022	0.60
95WJVP223	220164.17	7053997.38	485.26	248.46	-60	105	20	30	10	0.064	0.76
95WJVP227	221026.25	7054337.69	464.11	248.46	-60	117	48	56	8	0.133	1.01
95WJVP228	221139.31	7054382.31	466.96	248.46	-60	117	46	52	6	0.025	0.60
95WJVP234	219601.34	7056356.31	461.91	248.46	-60	120	52	68	16	0.042	0.79
95WJVP240	218316.74	7057569.95	481.11	248.46	-60	99	29	47	18	0.083	0.89
95WJVP247	218084.31	7058338.57	476.48	248.46	-60	99	33	59	26	0.04	0.60
95WJVP248	218193.17	7058381.55	471.23	248.46	-60	111	45	59	14	0.047	0.71
95WJVP251	217098.66	7058809.85	522.15	248.46	-60	120	2	4	2	0.023	0.5
95WJVP255	217907.71	7059129.23	472.67	248.46	-60	111	49	59	10	0.101	1.11
95WJVP256	218019.37	7059173.30	472.70	248.46	-60	123	47	61	14	0.036	0.81
95WJVP259	216769.93	7059540.46	485.60	248.46	-60	93	30	66	36	0.056	0.70
95WJVP260	216888.56	7059587.29	497.87	248.46	-60	111	27	39	12	0.229	0.60
95WJVP263	217512.44	7059833.57	477.90	248.46	-60	117	44	60	16	0.047	0.82
95WJVP264	217620.38	7059876.17	470.72	248.46	-60	123	54	66	12	0.026	0.59
95WJVP265	217732.04	7059920.24	470.70	248.46	-60	117	57	63	6	0.056	0.64
95WJVP270	216472.19	7061573.84	491.85	248.46	-60	117	45	53	8	0.050	0.78
95WJVP271	216581.52	7061617.00	487.49	248.46	-60	99	42	66	24	0.061	0.81
95WJVP272	216688.06	7061659.06	477.80	248.46	-60	99	58	72	14	0.034	0.74
96WJVD003	216941.37	7060899.24	482.82	248.46	-60	283.2	45	61.4	16.4	0.035	0.82
96WJVD004	217004.71	7060923.76	479.57	248.46	-60	325	42	72	30	0.034	0.66
96WJVD005	220594.62	7055457.87	509.47	248.46	-60	250	10	14	4	0.075	0.87
96WJVD008	217142.39	7058827.12	509.46	248.46	-60	196	12	26	14	0.052	0.75
96WJVD009	217990.08	7058731.97	469.57	248.46	-60	175.7	42	68	26	0.040	0.85
96WJVP292	216012.72	7062252.84	501.10	248.46	-60	99	38	52	14	0.106	0.97
96WJVP293	216121.12	7062295.63	495.12	248.46	-60	123	44	60	16	0.068	0.86
96WJVP296	215726.23	7062569.93	522.35	248.46	-60	159	24	26	2	0.039	0.68
96WJVP298	215942.10	7062655.15	507.59	248.46	-60	123	36	46	10	0.027	0.67
96WJVP301	215501.15	7062911.28	518.27	248.46	-60	99	30	36	6	0.036	0.66
96WJVP302	215610.48	7062954.44	513.53	248.46	-60	123	36	40	4	0.045	0.91
96WJVP303	215720.86	7063004.45	519.03	248.46	-60	115	26	42	16	0.072	0.76
96WJVP306	215263.97	7063247.84	526.68	248.46	-60	99	18	36	18	0.043	0.52
96WJVP307	215370.51	7063289.88	517.36	248.46	-60	141	34	42	8	0.047	0.86

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
96WJVP308	215484.05	7063340.09	525.81	248.46	-60	111	19	37	18	0.039	0.72
96WJVP312	215173.34	7063642.25	533.40	248.46	-60	135	18	34	16	0.031	0.60
96WJVP313	215283.26	7063692.08	536.03	248.46	-60	111	21	29	8	0.034	0.92
96WJVP315	215981.17	7062670.57	505.86	248.46	-60	93	36	50	14	0.040	0.70
96WJVP316	216988.77	7060487.21	480.67	248.46	-60	147	45	63	18	0.124	0.91
96WJVP317	217289.91	7060175.90	485.53	248.46	-60	147	28	63	35	0.047	0.80
96WJVP322	219238.53	7056643.28	465.91	248.46	-60	123	50	62	12	0.017	0.69
96WJVP323	219530.14	7056328.21	472.56	248.46	-60	147	43	51	8	0.094	0.88
96WJVP325	217274.51	7058879.28	513.41	248.46	-60	111	10	20	10	0.062	0.57
96WJVP327	221127.96	7053513.99	458.16	248.46	-60	147	55	59	4	0.183	1.05
96WJVP328	221293.65	7051862.13	459.78	248.46	-60	147	44	52	8	0.072	0.70
96WJVP330	223935.71	7048603.23	489.86	248.46	-60	135	2	16	14	0.059	0.67
97WP350	224596.86	7048003.85	475.28	248.46	-60	117	10	33	23	0.019	0.65
AEWRCM001	216886.00	7059587.25	498.59	248	-60	48	26	37.5	11.5	0.135	0.64
AEWRCM002	221025.55	7054335.28	466.03	248	-60	60	46	54	8	0.150	1.01
AEWRCM003	221608.07	7052414.01	478.81	248	-60	31	26.5	30.5	4	0.093	0.78
AEWRCM003A	221601.16	7052414.38	478.66	248	-60	48	26.5	30.5	4	0.045	0.58
AEWRCM004	223764.80	7048967.92	486.25	248	-60	30	4.5	30	25.5	0.068	0.79
AMAXW008	224185.90	7048437.58	487.85	0	-90	128.02	3.04	12.19	9.15	-	0.67
AMAXW009	222570.55	7051335.73	466.97	0	-90	152.4	28.95	42.67	13.72	-	0.80
AMAXW011	221089.70	7053476.48	461.71	0	-90	152.4	44.19	47.24	3.05	-	0.69
RWD00026	217166.47	7058796.46	504.79	0	-90	111.6	16	28	12	0.032	0.55
RWR00159	217074.15	7058877.76	511.94	90	-50	24	12	20	8	0.022	0.63
RWR00165	216954.75	7058822.91	495.74	0	-90	60	24	31	7	0.017	0.45
RWR00167	217175.01	7058756.06	516.49	90	-50	186	4	24	20	0.064	0.68
RWR00180	217156.04	7059154.87	514.30	248.5	-60	258	12	16	4	0.049	0.72
RWR00181	217342.13	7058583.50	513.11	248.5	-60	108	4	28	24	0.037	0.52
WA000053	224266.23	7048735.31	481.84	223.76	-60	45	12	22	10	0.06	0.96
WA000054	224267.83	7048726.75	485.46	223.76	-60	29	8	18	10	0.035	0.84
WA000324	220587.51	7053257.63	452.24	268.76	-60	81	60	64	4	-	0.72
WA000325	220584.48	7053257.56	443.43	88.76	-60	81	70	74	4	-	0.59
WA000377	221290.08	7051871.91	459.67	268.76	-60	77	46	50	4	0.044	0.73
WA000378	221339.09	7051872.96	457.98	268.76	-60	71	46	54	8	0.028	0.74
WA000379	221391.60	7051874.12	462.35	268.76	-60	76.5	36	54	18	0.046	0.63
WA000380	221439.11	7051875.14	458.05	268.76	-60	66	46	54	8	0.034	0.79
WA000381	221493.12	7051876.32	464.95	268.76	-60	60	40	44	4	0.155	0.78
WA000389	221897.21	7051885.10	472.78	268.76	-60	48	32	36	4	0.041	0.54
WA000391	221993.24	7051887.19	466.57	268.76	-60	59	34	50	16	0.075	0.94
WA000393	222096.26	7051889.42	472.80	268.76	-60	48	30	42	12	0.037	0.81

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WA000394	222149.77	7051890.58	479.45	268.76	-60	55	24	34	10	0.058	0.73
WCN21RC001	223687.42	7048939.38	493.19	338	-60	30	4	18	14	0.037	0.71
WCN21RC002	223681.69	7048960.39	494.74	338	-60	24	4	16	12	0.070	0.79
WCN21RC003	223674.10	7048982.26	497.90	338	-60	24	3	11	8	0.091	1.17
WCN21RC004	223660.79	7049004.45	497.25	338	-60	24	3	13	10	0.059	0.67
WCN21RC005	223643.53	7049024.09	495.82	338	-60	24	3	16	13	0.045	0.74
WCN21RC006	223621.53	7049037.27	495.93	338	-60	24	2	16	14	0.050	0.63
WCN21RC007	223610.62	7049058.16	498.54	338	-60	24	1	11	10	0.049	0.60
WCN21RC008	223599.86	7049077.64	499.46	338	-60	24	1	10	9	0.079	0.90
WCN21RC009	223580.29	7049097.96	496.63	338	-60	24	2	16	14	0.077	0.94
WCN21RC010	223559.69	7049119.97	497.25	338	-60	24	4	12	8	0.102	0.96
WCN21RC011	223546.64	7049138.76	495.48	338	-60	24	5	14	9	0.085	0.96
WCN21RC012	223543.23	7049165.97	497.91	338	-60	24	2	12	10	0.054	0.79
WCN21RC013	223531.72	7049189.10	494.82	338	-60	30	5	16	11	0.075	0.79
WCN21RC015	223533.16	7049251.35	489.49	338	-60	24	6	20	14	0.057	0.92
WCN21RC016	223517.46	7049270.49	491.82	338	-60	24	6	14	8	0.065	0.73
WCN21RC017	223500.21	7049288.94	490.11	338	-60	24	5	20	15	0.043	0.82
WCN21RC018	223485.26	7049306.75	494.76	338	-60	24	0	15	15	0.043	0.56
WCN21RC019	223467.76	7049329.35	488.43	338	-60	24	8	23	15	0.068	0.72
WCN21RC020	223440.77	7049341.54	489.43	338	-60	24	7	21	14	0.061	0.89
WCN21RC021	223432.79	7049364.26	489.17	338	-60	24	8	19	11	0.087	0.73
WCN21RC022	223422.80	7049387.23	488.68	338	-60	42	9	19	10	0.184	1.08
WCN21RC023	223413.48	7049409.85	489.06	338	-60	42	9	17	8	0.176	0.82
WCN21RC024	223401.57	7049431.27	489.26	338	-60	42	9	15	6	0.121	0.88
WCN21RC025	223389.88	7049454.33	487.06	338	-60	42	8	21	13	0.141	0.95
WCN21RC026	223387.00	7049478.73	489.08	338	-60	36	9	15	6	0.131	0.98
WCN21RC027	223375.33	7049506.81	485.73	338	-60	30	10	22	12	0.083	1.06
WCN21RC028	223366.35	7049524.78	489.14	338	-60	36	8	17	9	0.121	0.76
WCN21RC029	223353.00	7049549.23	483.18	338	-60	42	11	31	20	0.045	0.69
WCN21RC031	223343.35	7049601.92	478.89	338	-60	42	16	36	20	0.166	1.11
WCN21RC032	223332.84	7049625.14	477.92	338	-60	42	15	39	24	0.051	0.66
WCN21RC033	223321.26	7049651.41	482.67	338	-60	42	12	28	16	0.076	0.92
WCN21RC036	223629.63	7049346.46	473.69	248	-60	54	8	44	36	0.039	0.70
WCN21RC037	223602.35	7049335.38	468.12	248	-60	54	25	41	16	0.137	1.38
WCN21RC038	223586.75	7049325.04	483.63	248	-60	30	9	22	13	0.064	1.14
WCN21RC039	223565.87	7049311.94	485.78	248	-60	24	4	24	20	0.044	0.86
WCN21RC040	223538.64	7049301.23	480.27	248	-60	48	10	33	23	0.066	1.06
WCN21RC041	223516.08	7049295.90	483.23	248	-60	42	8	30	22	0.038	0.76
WCN21RC042	223463.89	7049276.27	490.77	248	-60	24	7	20	13	0.067	0.85

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN21RC043	223442.77	7049265.21	492.46	248	-60	24	10	14	4	0.096	0.60
WCN21RC044	223419.92	7049251.67	488.48	248	-60	24	7	24	17	0.042	0.56
WCN21RC045	223395.82	7049245.29	488.40	248	-60	24	10	19	9	0.097	0.73
WCN21RC046	223371.79	7049238.94	486.62	248	-60	30	11	20	9	0.126	0.67
WCN21RC055	223820.22	7048747.84	485.17	248	-60	30	8	26	18	0.032	0.72
WCN21RC056	223727.27	7048708.86	487.02	248	-60	30	1	23	22	0.068	0.57
WCN21RC061	223978.75	7048940.36	485.84	248	-60	24	3	23	20	0.020	0.50
WCN21RC062	223884.49	7048893.90	487.32	248	-60	36	6	26	20	0.061	0.91
WCN21RC063	223785.03	7048858.34	491.80	248	-60	30	5	18	13	0.028	0.62
WCN21RC064	223685.72	7048824.87	489.64	248	-60	24	5	15	10	0.063	0.93
WCN21RC068	223849.09	7049093.03	492.52	248	-60	24	0	8	8	0.06	0.57
WCN21RC069	223746.81	7049047.54	483.54	248	-60	36	9	28	19	0.065	0.88
WCN21RC070	223554.99	7048971.48	492.01	248	-60	24	1	18	17	0.051	0.70
WCN21RC074	223696.69	7049134.09	473.69	248	-60	60	8	48	40	0.039	0.67
WCN21RC075	223650.01	7049120.00	482.48	248	-60	36	10	30	20	0.062	0.71
WCN21RC076	223602.30	7049100.51	498.24	248	-60	24	0	14	14	0.071	0.74
WCN21RC077	223505.30	7049059.21	495.99	248	-60	24	2	8	6	0.042	0.58
WCN21RC081	223657.39	7049236.12	473.17	248	-60	48	22	34	12	0.029	0.54
WCN21RC082	223605.12	7049221.22	477.37	248	-60	48	11	39	28	0.078	1.01
WCN21RC083	223565.83	7049204.53	489.78	248	-60	30	7	17	10	0.071	0.74
WCN21RC084	223464.14	7049165.44	491.02	248	-60	24	10	18	8	0.092	0.76
WCN21RC085	223414.50	7049147.63	492.04	248	-60	24	7	10	3	0.284	0.65
WCN21RC087	223602.48	7049428.27	466.16	248	-60	42	27	42	15	0.034	0.91
WCN21RC088	223565.29	7049413.86	472.24	248	-60	72	10	47	37	0.045	0.99
WCN21RC089	223516.73	7049393.51	483.65	248	-60	42	5	30	25	0.033	0.82
WCN21RC090	223472.38	7049378.58	490.21	248	-60	30	7	13	6	0.051	0.80
WCN21RC091	223374.52	7049341.62	489.02	248	-60	24	10	16	6	0.279	0.85
WCN21RC092	223322.11	7049321.82	484.92	248	-60	30	14	21	7	0.213	0.66
WCN21RC098	223509.18	7049500.61	459.84	248	-60	48	38	47	9	0.067	1.04
WCN21RC099	223469.01	7049488.44	480.67	248	-60	30	9	30	21	0.049	0.71
WCN21RC100	223312.34	7049423.23	478.22	248	-60	36	17	32	15	0.080	0.90
WCN21RC101	223272.20	7049409.77	481.23	248	-60	36	17	25	8	0.165	0.80
WCN21RC105	223475.70	7049607.36	470.17	248	-60	54	15	47	32	0.06	1.09
WCN21RC106	223425.87	7049587.88	472.51	248	-60	36	23	36	13	0.054	0.94
WCN21RC107	223381.39	7049571.32	484.68	248	-60	36	9	27	18	0.047	0.71
WCN21RC108	223280.07	7049525.16	481.12	248	-60	30	15	30	15	0.05	0.68
WCN21RC109	223232.20	7049508.39	480.73	248	-60	36	17	26	9	0.083	0.73
WCN21RC112	223410.88	7049786.84	472.75	248	-60	54	20	34	14	0.036	0.51
WCN21RC113	223362.31	7049764.89	478.91	248	-60	30	13	30	17	0.060	0.68

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN21RC114	223265.49	7049727.25	480.11	248	-60	30	14	29	15	0.059	0.73
WCN21RC115	223160.86	7049689.17	475.43	248	-60	48	21	33	12	0.078	0.95
WCN21RC118	223315.01	7049849.41	474.74	248	-60	42	13	38	25	0.035	0.56
WCN21RC119	223215.42	7049815.01	474.69	248	-60	48	19	33	14	0.073	0.79
WCN21RC120	223115.43	7049778.48	474.93	248	-60	48	20	32	12	0.153	0.76
WCN21RC123	223281.65	7049959.00	478.73	248	-60	54	10	30	20	0.032	0.61
WCN21RC124	223182.12	7049919.20	470.16	248	-60	36	24	36	12	0.069	0.72
WCN21RC125	223075.67	7049875.80	465.89	248	-60	42	31	42	11	0.118	0.92
WCN21RC133	223051.89	7050091.32	456.69	248	-60	54	44	49	5	0.033	0.55
WCN21RC134	222181.64	7051837.64	474.55	248	-60	48	29	40	11	0.046	0.91
WCN21RC135	222114.56	7051792.85	471.16	248	-60	60	29	44	15	0.055	0.90
WCN21RC138	221962.90	7051862.31	474.96	248	-60	48	26	37	11	0.141	0.76
WCN21RC141	222059.88	7051900.68	475.39	248	-60	48	25	40	15	0.052	0.8
WCN21RC142	221923.78	7051977.13	463.40	248	-60	48	42	48	6	0.073	1.07
WCN21RC143	222148.56	7051938.42	475.10	248	-60	42	32	42	10	0.119	0.94
WCN21RC144	222106.86	7052050.52	472.05	248	-60	48	35	48	13	0.203	1.02
WCN21RC145	222031.63	7052018.25	470.61	248	-60	48	34	43	9	0.257	1.37
WCN21RC146	222214.61	7052094.19	474.07	248	-60	54	27	47	20	0.038	0.69
WCN21RC150	221892.62	7052177.62	466.88	248	-60	54	35	48	13	0.062	1.05
WCN21RC151	221798.35	7052138.01	461.28	248	-60	54	42	53	11	0.07	0.86
WCN21RC152	221710.67	7052106.74	465.14	248	-60	54	40	46	6	0.056	0.75
WCN21RC155	221410.00	7051991.86	456.48	248	-60	54	49	54	5	0.033	0.50
WCN21RC156	222018.27	7052229.27	469.76	248	-60	54	35	43	8	0.127	1.02
WCN21RC158	222096.34	7052277.39	476.39	248	-60	42	22	40	18	0.088	0.97
WCN21RC159	222057.23	7052369.77	475.83	248	-60	42	25	39	14	0.079	0.84
WCN21RC160	221958.75	7052329.99	473.88	248	-60	48	29	40	11	0.039	0.81
WCN21RC161	221831.82	7052387.77	466.42	248	-60	54	36	51	15	0.069	1.00
WCN21RC162	221940.55	7052437.20	469.70	248	-60	48	32	47	15	0.056	0.83
WCN21RC163	222008.28	7052481.75	463.39	248	-60	54	42	50	8	0.124	0.92
WCN21RC166	221943.19	7052647.18	472.70	248	-60	48	33	39	6	0.054	0.58
WCN21RC167	221828.56	7052592.76	468.40	248	-60	48	34	48	14	0.034	0.70
WCN21RC169	221799.29	7052688.69	471.81	248	-60	54	33	42	9	0.062	0.93
WCN21RC172	221264.84	7052050.32	454.33	248	-60	66	47	62	15	0.101	1.14
WCN21RC176	221668.02	7052206.03	459.81	248	-60	60	42	56	14	0.037	0.72
WCN21RC178	221861.30	7052289.26	480.44	248	-60	48	27	34	7	0.026	0.62
WCN21RC180	221241.04	7052175.04	460.54	248	-60	66	41	54	13	0.097	1.26
WCN21RC181	221348.33	7052210.20	480.07	248	-60	48	21	30	9	0.055	0.67
WCN21RC184	221636.50	7052323.31	456.32	248	-60	66	47	62	15	0.093	1.42
WCN21RC185	221737.77	7052355.89	468.86	248	-60	48	35	46	11	0.112	1.09

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN21RC190	221218.56	7052457.51	473.43	248	-60	48	32	36	4	0.033	0.56
WCN21RC192	221202.34	7052563.14	489.72	248	-60	30	6	26	20	0.026	0.56
WCN21RC194	221617.67	7052505.68	476.49	248	-60	54	32	41	9	0.087	0.99
WCN21RC196	221612.85	7052606.49	469.12	248	-60	60	28	53	25	0.193	0.72
WCN21RC197	221713.31	7052653.81	465.09	248	-60	66	36	54	18	0.047	0.83
WCN21RC198	221733.96	7052558.73	471.16	248	-60	48	33	44	11	0.058	0.85
WCN21RC200	221485.39	7052676.02	476.20	248	-60	48	24	40	16	0.060	0.88
WCN21RC201	221591.62	7052703.62	470.29	248	-60	48	36	44	8	0.071	1.10
WCN21RC202	221684.00	7052752.84	477.34	248	-60	48	23	40	17	0.077	1.46
WCN21RC203	221343.09	7052834.39	473.08	248	-60	48	30	43	13	0.072	1.11
WCN21RC204	221468.72	7052869.98	467.67	248	-60	60	35	52	17	0.083	1.22
WCN21RC205	221563.78	7052931.14	468.55	248	-60	60	32	52	20	0.103	1.15
WCN21RC207	221325.48	7052945.69	473.87	248	-60	54	29	44	15	0.053	0.07
WCN21RC208	221417.85	7052984.75	466.44	248	-60	54	39	51	12	0.097	1.01
WCN21RC209	221520.37	7053021.52	468.82	248	-60	60	32	52	20	0.035	0.71
WCN21RC210	221012.79	7052947.01	463.11	248	-60	54	43	54	11	0.028	0.82
WCN21RC212	221304.82	7053053.04	468.32	248	-60	54	36	51	15	0.099	0.85
WCN21RC215	221069.93	7052725.51	473.66	248	-60	54	20	51	31	0.066	0.67
WCN21RC217	221033.52	7052829.95	459.05	248	-60	60	46	59	13	0.054	0.63
WCN21RC222	221216.24	7053202.16	463.27	248	-60	60	48	51	3	0.199	0.70
WCN21RC223	221281.49	7053238.04	457.74	68	-60	66	50	62	12	0.072	1.10
WCN21RC227	221233.17	7053339.70	453.19	248	-60	72	56	68	12	0.085	1.16
WCN21RC228	221295.87	7053361.61	455.34	68	-60	66	54	64	10	0.161	1.21
WCN21RC229	221256.09	7053460.06	457.43	68	-60	66	52	62	10	0.129	1.05
WCN21RC231	221238.07	7053654.80	460.21	68	-60	66	50	61	11	0.032	1.04
WCN21RC232	221146.68	7053616.16	448.56	68	-60	78	62	73	11	0.141	0.81
WCN21RC233	221170.48	7053736.96	458.53	248	-60	66	52	62	10	0.085	0.92
WCN21RC234	221260.33	7053790.73	461.38	248	-60	72	40	67	27	0.038	0.65
WCN21RC236	220999.97	7054428.41	471.91	248	-60	48	39	47	8	0.159	1.08
WCN21RC237	221007.23	7054546.54	464.20	248	-60	60	45	60	15	0.130	0.80
WCN21RC238	221107.64	7054593.75	470.37	248	-60	54	38	54	16	0.040	0.67
WCN21RC239	221105.85	7054144.75	461.27	248	-60	66	50	58	8	0.050	0.64
WCN21RC240	221212.30	7054194.01	470.99	248	-60	60	40	48	8	0.024	0.65
WCN21RC241	220986.99	7054649.77	474.09	248	-60	66	24	61	37	0.027	0.69
WCN21RC242	220750.87	7053147.69	447.20	248	-60	78	60	74	14	0.110	1.22
WCN21RC243	220845.35	7053188.85	450.48	248	-60	66	60	66	6	0.019	0.58
WCN21RC244	220712.81	7053247.50	462.51	248	-60	60	41	58	17	0.121	1.73
WCN21RC246	220602.86	7053398.04	463.59	248	-60	60	45	52	7	0.104	1.07
WCN21RC248	220489.18	7053477.99	466.53	248	-60	54	41	49	8	0.051	0.96

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN21RC249	220589.66	7053514.77	471.45	248	-60	54	30	50	20	0.100	1.25
WCN21RC250	220926.37	7054515.71	486.29	248	-60	48	23	31	8	0.082	0.95
WCN21RC251	220789.69	7054901.76	507.12	248	-60	42	7	8	1	0.23	0.64
WCN21RC252	220887.23	7054932.85	499.18	248	-60	36	12	20	8	0.037	0.65
WCN21RC253	220972.30	7054965.45	492.95	248	-60	36	20	24	4	0.052	0.61
WCN21RC254	218174.32	7057702.74	495.70	248	-60	42	12	34	22	0.038	0.74
WCN21RC255	221371.23	7051989.65	457.55	248	-60	60	50	51	1	0.032	0.56
WCN21RC256	223098.94	7050113.95	459.44	248	-60	60	36	51	15	0.031	0.58
WCN21DDH001	220952.50	7054875.38	512.17	248	-60	52.8	26	51	25	0.062	0.98
WCN21DDH002	220952.79	7054762.76	511.54	248	-60	43.8	14	24	10	0.025	0.79
WCN21DDH003	221057.10	7054573.94	510.12	0	-90	60.4	27	43	16	0.034	0.84
WCN21DDH004	221241.17	7053777.58	508.69	248	-60	66.1	57.2	62.9	5.7	0.056	1.23
WCN21DDH005	221174.67	7053635.34	508.13	68	-60	76.6	57	66	6	0.063	1.17
WCN21DDH006	220783.81	7053272.48	506.23	248	-60	60	39	55	16	0.040	1.21
WCN21DDH007	221555.71	7052918.27	505.55	248	-60	60	39	48	9	0.115	1.11
WCN21DDH008	221585.43	7052748.79	505.01	248	-60	60	29	52	23	0.119	0.95
WCN21DDH011	222020.57	7052360.44	503.89	248	-60	49.6	31	42	11	0.123	1.12
WCN21DDH012	221717.20	7052359.74	503.94	248	-60	66.1	42	50	8	0.046	0.80
WCN21DDH013	222154.79	7051997.52	505.12	248	-60	60	40	48	8	0.045	1.00
WCN21DDH014	223688.82	7048939.63	502.99	248	-60	31.6	4	11	7	0.100	0.82
WCN21DDH015	223827.97	7048988.37	498.59	248	-60	40	20	39	19	0.060	1.14
WCN21DDH016	223796.29	7049068.02	498.15	248	-60	40	12	29	17	0.055	0.85
WCN21DDH017	223716.70	7049035.44	501.39	248	-60	40	8	18	10	0.030	0.78
WCN21DDH018	223596.25	7049099.01	504.41	248	-60	30.1	3	10	7	0.160	0.94
WCN21DDH019	223679.57	7049133.27	498.75	248	-60	50	12	23	11	0.059	1.06
WCN21DDH020	223641.87	7049230.16	498.65	248	-60	50	5	26	21	0.056	0.66
WCN21DDH021A	223581.84	7049324.47	497.65	248	-60	26.1	4	8	4	0.165	1.39
WCN21DDH021A	223581.84	7049324.47	497.65	248	-60	26.1	11	15	4	0.036	1.17
WCN21DDH022A	223424.91	7049361.79	501.20	248	-60	30.1	7	18	11	0.074	0.65
WCN21DDH023	223554.12	7049409.45	497.86	248	-60	53.2	12	25	13	0.028	0.97
WCN21DDH024	223508.10	7049502.36	497.05	248	-60	50	26	43	17	0.079	1.15
WCN21DDH025A	223458.33	7049597.71	497.62	248	-60	54	22	42	20	0.079	1.02
WCN21DDH026	223419.06	7049581.76	498.83	248	-60	40	20	37	17	0.088	1.21
WCN21DDH027	223349.03	7049585.08	501.67	248	-60	40.6	13	21	8	0.095	0.72
WCN21DDH028	223323.48	7049744.87	498.81	248	-60	38.4	15	31	16	0.063	1.02
WCN21DDH029	223232.02	7049820.84	497.48	248	-60	50	16	32	16	0.070	0.86
WCN21DDH030	223142.13	7049904.11	496.99	0	-90	50	24	33	9	0.070	0.94
WCN21DDH031	223147.76	7050014.41	496.61	248	-60	60	34	48	14	0.083	0.93
WCN22DDH032	223810.09	7048806.70	501.78	248	-60	24.6	5	24	19	0.062	0.98

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN22DDH033	223850.66	7048935.91	499.65	248	-60	20.1	8	19	11	0.022	0.71
WCN22DDH034	223832.49	7049039.72	497.48	248	-60	30.9	13	23	10	0.028	0.74
WCN22DDH035A	223752.71	7049105.92	498.20	248	-60	36.1	22	27	5	0.037	0.72
WCN22DDH036	223673.98	7049177.51	498.15	248	-60	30.1	6	28	22	0.055	0.90
WCN22DDH037	223589.64	7049256.73	499.97	248	-60	35.1	9	26	17	0.044	1.02
WCN22DDH038	223584.93	7049372.67	497.97	248	-60	35	14	25	11	0.024	0.82
WCN22DDH039	223571.99	7049472.99	496.55	248	-60	43.9	14	43.9	29.9	0.029	0.86
WCN22DDH040	223476.13	7049547.51	497.73	248	-60	50.2	22	45	23	0.057	0.85
WCN22DDH041	223340.62	7049491.87	500.75	248	-60	45.1	13	27	14	0.130	0.88
WCN22DDH042	223448.24	7049645.67	497.93	248	-60	50.1	23	41	18	0.063	1.16
WCN22DDH043	223346.99	7049704.17	497.98	248	-60	40.1	14	26	12	0.061	0.77
WCN22DDH043	223325.49	7049802.60	497.93	248	-60	45.8	29	36	7	0.017	0.60
WCN22DDH044	223242.16	7049875.97	497.14	248	-60	45.1	26	39	13	0.075	1.08
WCN22DDH045	223075.50	7049925.34	497.51	248	-60	49.8	20	33	13	0.095	0.90
WCN22DDH046	223144.76	7050063.08	496.56	248	-60	53.1	37	49.8	12.8	0.049	0.82
WCN22DDH047	222217.70	7051915.13	505.36	248	-60	42.4	40	49	9	0.057	0.93
WCN22DDH048	222125.16	7051931.58	504.64	248	-60	45	31	40	9	0.147	1.05
WCN22DDH049	222101.93	7051969.67	504.94	248	-60	42.2	25	37	12	0.094	0.87
WCN22DDH050	222101.87	7052038.08	505.18	248	-60	55	29	42.2	13.2	0.099	1.04
WCN22DDH051	222054.09	7052094.78	504.71	248	-60	50	33	46	13	0.056	0.71
WCN22DDH052	221991.85	7052196.72	503.39	248	-60	46.9	29	40	11	0.144	1.17
WCN22DDH053	221480.64	7053003.50	505.90	248	-60	60	29	36	7	0.028	0.54
WCN22DDH054	221361.56	7052837.88	505.13	248	-60	44.7	47	53	6	0.193	1.36
WCN22DDH055	221534.91	7052877.29	505.68	248	-60	58	31	43	12	0.058	1.02
WCN22DDH056	221658.51	7052811.54	505.27	248	-60	50.3	41	48	7	0.078	0.83
WCN22DDH057	221653.01	7052688.98	505.09	248	-60	58	24	39	15	0.079	1.23
WCN22DDH058	221753.19	7052514.91	504.76	248	-60	36.1	40	52	12	0.068	0.66
WCN22DDH060	221958.33	7052381.12	504.29	68	-60	50	28	39	11	0.100	1.09
WCN22DDH061	221709.19	7052606.04	504.86	248	-60	52	36	48	12	0.064	0.73
WCN22RC257	220751.83	7055086.65	513.65	248	-60	30	10	14	4	0.12	1.01
WCN22RC258	220785.13	7055046.56	513.87	248	-60	30	11	14	3	0.04	0.81
WCN22RC259	220862.57	7055134.49	513.38	248	-60	30	20	30	10	0.1	1.02
WCN22RC266	220777.09	7054940.10	513.53	248	-60	30	6	9	3	0.07	0.83
WCN22RC267	220844.43	7054915.70	513.90	248	-60	30	15	17	2	0.02	0.83
WCN22RC269	220797.84	7054786.57	513.30	248	-60	30	22	28	6	0.04	0.86
WCN22RC272	220905.22	7054867.93	512.63	248	-60	30	17	19	2	0.03	0.85
WCN22RC273	220884.71	7054815.21	512.60	248	-60	42	11	18	7	0.03	0.91
WCN22RC274	220981.28	7054845.94	511.53	248	-60	60	33	52	19	0.1	1.18
WCN22RC276	221073.89	7054723.63	510.50	248	-60	54	34	54	20	0.09	1.04

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN22RC277	221123.87	7054535.85	509.89	248	-60	60	35	43	7	0.06	0.95
WCN22RC279	221076.02	7054623.04	510.23	248	-60	54	34	40	6	0.06	1.19
WCN22RC280	221030.14	7054606.02	510.26	248	-60	66	27	40	13	0.04	1.13
WCN22RC281	220998.68	7054639.05	510.38	248	-60	60	30	40	10	0.06	1.40
WCN22RC282	221048.80	7054665.22	510.35	248	-60	60	26	36	10	0.03	1.20
WCN22RC283	220899.40	7054613.64	510.82	248	-60	36	18	30	12	0.06	0.81
WCN22RC284	220877.98	7054651.82	511.44	248	-60	30	19	26	7	0.03	0.72
WCN22RC285	220872.71	7054700.83	511.79	248	-60	36	12	15	3	0.37	1.15
WCN22RC286	220974.90	7054742.10	511.07	248	-60	54	24	32	8	0.03	0.92
WCN22RC288	220939.30	7054562.41	510.19	248	-60	54	21	24	3	0.12	0.88
WCN22RC289	220973.50	7054545.60	509.94	248	-60	42	25	29	4	0.05	1.03
WCN22RC291	221322.93	7053003.47	505.98	248	-60	54	36	39	3	0.15	0.91
WCN22RC292	221282.58	7053050.84	506.24	248	-90	48	27	36	9	0.07	0.88
WCN22RC293	221411.41	7053037.46	506.02	248	-60	54	43	51	8	0.16	1.35
WCN22RC294	221510.64	7052982.76	505.69	248	-60	54	40	50	10	0.11	1.38
WCN22RC295	221424.02	7052929.01	505.63	248	-60	60	33	44	11	1.00	1.03
WCN22RC296	221382.39	7052961.60	505.79	248	-60	54	34	42	8	0.23	1.42
WCN22RC297	221600.95	7052886.31	505.34	248	-60	60	33	47	14	0.1	1.16
WCN22RC298	221440.34	7052842.25	505.00	248	-60	54	33	42	9	0.17	1.36
WCN22RC299	221485.90	7052796.54	505.01	248	-60	54	31	37	6	0.09	1.04
WCN22RC300	221595.36	7052838.76	505.04	248	-60	60	40	47	7	0.11	1.31
WCN22RC301	221606.29	7052788.51	504.99	248	-60	60	37	45	8	0.06	1.29
WCN22RC302	221503.72	7052747.67	504.78	248	-60	60	40	52	12	0.36	1.51
WCN22RC303	221547.50	7052717.10	504.57	248	-60	60	43	52	9	0.07	1.17
WCN22RC304	221647.14	7052755.75	504.97	248	-60	57	40	44	4	0.15	0.91
WCN22RC305	221559.41	7052656.12	504.18	248	-60	60	34	51	17	0.07	1.23
WCN22RC306	221746.44	7052731.16	504.55	248	-60	60	48	57	9	0.15	1.26
WCN22RC307	221790.07	7052635.85	504.44	248	-60	54	34	40	6	0.09	0.98
WCN22RC308	221886.00	7052673.18	504.09	248	-60	54	28	33	5	0.08	1.15
WCN22RC309	221608.79	7052558.87	503.97	248	-60	54	23	35	12	0.07	1.05
WCN22RC310	221759.14	7052515.23	504.65	248	-60	60	38	54	16	0.06	0.82
WCN22RC311	221844.89	7052561.01	504.23	248	-60	54	32	40	8	0.07	1.19
WCN22RC312	221833.51	7052453.05	504.40	248	-60	54	38	46	8	0.08	1.03
WCN22RC313	221901.50	7052532.20	504.08	248	-60	54	28	33	5	0.08	0.98
WCN22RC314	221946.09	7052597.10	504.20	248	-60	48	34	40	6	0.27	1.23
WCN22RC316	221981.32	7052510.77	503.78	248	-60	54	36	40	4	0.04	0.82
WCN22RC317	221993.20	7052474.24	503.84	248	-60	48	31	37	6	0.11	1.34
WCN22RC318	222066.92	7052417.15	503.56	248	-60	48	33	38	5	0.21	1.27
WCN22RC319	222059.53	7052313.09	503.52	248	-60	47	30	39	9	0.15	1.07

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN22RC320	222012.36	7052287.44	503.40	248	-60	48	31	40	9	0.24	1.47
WCN22RC321	222153.25	7052203.40	503.96	248	-60	48	25	39	14	0.06	1.46
WCN22RC322	222245.02	7052154.45	504.34	248	-60	54	29	36	7	0.27	1.52
WCN22RC323	221674.73	7052479.39	504.22	248	-60	60	44	51	7	0.18	1.38
WCN22RC324	221676.57	7052442.22	503.95	248	-60	60	47	51	4	0.21	1.26
WCN22RC325	221748.29	7052407.79	504.28	248	-60	60	39	50	11	0.15	1.11
WCN22RC326	221667.77	7052387.42	503.79	248	-60	66	47	61	14	0.1	0.91
WCN22RC327	221802.19	7052379.45	504.22	248	-60	60	43	50	7	0.15	1.19
WCN22RC329	221689.01	7052269.62	503.07	248	-60	60	42	53	11	0.07	0.93
WCN22RC331	221775.01	7052294.08	503.64	248	-60	42	33	38	5	0.02	0.80
WCN22RC332	221829.56	7052211.74	503.30	248	-60	54	36	43	7	0.03	0.84
WCN22RC333	221824.38	7052279.32	503.73	248	-60	42	29	33	4	0.02	1.06
WCN22RC334	221924.55	7052252.66	503.61	248	-60	48	32	40	8	0.07	1.25
WCN22RC335	221920.78	7052319.65	504.04	248	-60	48	30	34	4	0.07	0.83
WCN22RC336	221774.92	7052131.41	502.73	248	-60	60	38	43	5	0.06	1.03
WCN22RC337	221874.08	7052166.55	503.14	248	-60	54	32	45	13	0.05	1.17
WCN22RC338	221809.60	7052069.79	502.61	248	-60	54	40	46	6	0.11	0.94
WCN22RC339	221878.92	7052013.24	502.47	248	-60	54	35	46	11	0.04	1.04
WCN22RC340	221999.57	7052010.02	503.48	248	-60	60	42	48	6	0.04	1.33
WCN22RC341	221972.48	7052067.14	503.04	248	-60	60	40	46	6	0.06	1.50
WCN22RC342	221933.48	7052113.28	502.96	248	-60	54	32	45	13	0.04	1.09
WCN22RC343	222135.79	7052139.88	504.46	248	-60	60	34	52	18	0.17	1.13
WCN22RC344	222234.74	7052043.60	505.39	248	-60	60	39	52	13	0.12	1.37
WCN22RC345	222185.39	7052076.70	505.04	248	-60	60	42	53	11	0.14	1.43
WCN22RC346	222214.49	7051960.30	505.25	248	-60	54	41	49	8	0.08	1.26
WCN22RC347	222006.04	7051936.55	503.25	248	-60	54	34	40	6	0.09	1.12
WCN22RC348	222037.70	7051830.06	502.67	248	-60	54	28	37	9	0.06	1.06
WCN22RC349	222035.88	7051881.71	503.09	248	-90	47	23	34	11	0.05	1.15
WCN22RC350	222125.18	7051874.03	504.03	248	-60	48	28	35	7	0.11	1.26
WCN22RC351	223092.54	7050040.34	496.97	248	-60	60	42	51	9	0.05	1.06
WCN22RC352	223188.34	7050079.00	496.26	248	-60	60	42	48	6	0.08	1.17
WCN22RC353	223166.23	7049953.95	496.57	248	-60	54	28	36	8	0.11	0.89
WCN22RC354	223119.66	7049946.90	496.87	248	-60	54	36	41	5	0.27	1.04
WCN22RC355	223216.72	7049985.72	496.19	248	-60	48	29	39	10	0.1	1.02
WCN22RC356	223257.66	7050002.11	495.81	248	-60	54	27	41	14	0.05	1.16
WCN22RC357	223234.93	7049936.94	496.24	248	-60	42	22	30	8	0.11	0.99
WCN22RC358	223100.31	7049823.02	497.56	248	-60	48	27	33	6	0.08	0.88
WCN22RC359	223140.14	7049841.91	497.10	248	-60	48	27	38	11	0.12	1.02
WCN22RC360	223184.74	7049860.06	496.90	248	-60	48	28	30	2	0.12	1.60

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN22RC361	223280.63	7049897.12	496.51	248	-60	42	15	19	4	0.08	0.89
WCN22RC363	223177.44	7049802.89	497.30	248	-60	42	23	31	8	0.14	0.94
WCN22RC364	223277.57	7049837.72	497.47	248	-60	36	17	24	7	0.12	1.01
WCN22RC365	223099.93	7049715.31	497.98	248	-60	42	19	29	10	0.11	0.93
WCN22RC366	223142.66	7049731.92	498.12	248	-60	42	20	27	7	0.11	1.13
WCN22RC367	223181.53	7049749.64	498.18	248	-60	42	15	19	4	0.14	1.11
WCN22RC369	223279.76	7049785.23	498.30	248	-60	46	22	26	4	0.13	0.91
WCN22RC371	223219.11	7049717.23	499.09	248	-60	36	12	20	8	0.08	1.00
WCN22RC372	223382.75	7049716.76	497.50	248	-60	48	13	19	6	0.1	1.06
WCN22RC373	223430.55	7049735.78	496.24	248	-60	36	12	27	15	0.13	0.85
WCN22RC374	223437.09	7049697.93	496.65	248	-60	48	36	44	8	0.1	0.14
WCN22RC376	223243.51	7049663.59	500.39	248	-60	36	14	19	5	0.07	0.78
WCN22RC377	223287.01	7049679.06	499.41	248	-60	36	18	22	4	0.08	1.08
WCN22RC378	223228.44	7049613.63	500.31	248	-60	36	14	16	2	0.07	0.78
WCN22RC379	223252.01	7049569.33	500.30	248	-60	36	16	28	12	0.06	1.05
WCN22RC380	223390.90	7049622.95	499.39	248	-60	42	17	22	5	0.16	1.34
WCN22RC381	223424.51	7049526.31	499.07	248	-60	36	16	22	4	0.06	1.34
WCN22RC382	223519.91	7049568.48	496.50	248	-60	48	21	42	21	0.08	1.20
WCN22RC383	223469.43	7049432.01	498.29	248	-60	36	18	23	5	0.02	0.79
WCN22RC384	223519.53	7049453.88	497.61	248	-60	48	10	22	12	0.06	1.02
WCN22RC386	223282.92	7049471.43	499.88	248	-60	30	17	25	8	0.1	1.01
WCN22RC388	223330.87	7049383.55	499.99	248	-60	36	17	24	7	0.11	1.12
WCN22RC389	223374.44	7049397.98	500.33	248	-60	30	10	14	4	0.09	1.14
WCN22RC390	223355.91	7049435.81	500.13	248	-60	30	12	16	4	0.14	1.18
WCN22RC391	223432.86	7049470.75	498.04	248	-60	42	7	19	12	0.18	1.16
WCN22RC393	223403.70	7049310.02	500.90	248	-60	30	7	13	6	0.25	1.06
WCN22RC394	223494.44	7049335.23	500.77	248	-60	30	10	18	8	0.08	1.02
WCN22RC395	223536.48	7049356.72	499.38	248	-60	36	9	21	12	0.07	1.06
WCN22RC396	223630.99	7049396.60	496.09	248	-60	42	11	24	13	0.06	0.85
WCN22RC397	223627.19	7049288.03	497.95	248	-60	36	16	23	7	0.04	1.05
WCN22RC398	223672.60	7049304.72	496.17	248	-60	42	12	15	3	0.03	0.77
WCN22RC400	223441.97	7049206.91	501.89	248	-60	30	14	19	5	0.08	0.89
WCN22RC401	223485.82	7049226.41	503.22	248	-60	30	5	11	6	0.08	0.95
WCN22RC403	223577.82	7049145.14	502.59	248	-60	24	4	12	8	0.08	1.10
WCN22RC404	223637.29	7049116.27	500.02	248	-60	30	6	9	3	0.2	1.35
WCN22RC405	223618.47	7049162.75	498.58	248	-60	36	9	26	17	0.22	1.22
WCN22RC406	223716.89	7049200.74	496.68	248	-60	30	14	18	4	0.02	0.80
WCN22RC407	223737.71	7049159.54	498.12	248	-60	42	28	35	7	0.76	1.01
WCN22RC408	223544.54	7049071.51	502.02	248	-60	30	5	12	7	0.15	1.20

Hole ID	East	North	RL	Azimuth	Dip	Depth (m)	From (m)	To (m)	Length (m)	Co (%)	Ni (%)
WCN22RC409	223531.96	7049017.13	499.71	248	-60	30	2	8	6	0.05	0.91
WCN22RC410	223573.68	7049035.65	501.69	248	-60	30	2	12	10	0.17	1.27
WCN22RC411	223661.49	7049066.78	500.86	248	-60	30	5	18	13	0.09	1.33
WCN22RC412	223712.58	7049087.65	499.61	248	-60	30	8	20	12	0.08	1.03
WCN22RC414	223818.21	7049096.80	496.73	248	-60	36	12	33	21	0.04	0.88
WCN22RC415	223604.08	7048997.59	503.14	248	-60	30	5	8	3	0.11	1.10
WCN22RC416	223595.28	7048957.53	501.35	248	-60	24	3	11	8	0.09	1.23
WCN22RC417	223637.26	7048965.95	503.96	248	-60	24	6	9	3	0.18	1.19
WCN22RC418	223727.31	7049000.85	501.20	248	-60	30	8	15	7	0.14	1.35
WCN22RC419	223617.12	7048906.04	501.66	248	-60	30	4	17	13	0.08	0.91
WCN22RC420	223731.26	7048951.92	502.18	248	-60	30	12	19	7	0.04	0.86
WCN22RC421	223669.92	7048864.92	500.38	248	-60	30	6	14	8	0.08	1.38
WCN22RC423	223804.64	7048916.14	501.64	248	-60	24	8	12	4	0.07	1.12
WCN22RC424	223898.51	7048952.05	497.90	248	-60	36	31	34	3	0.09	1.09
WCN22RC425	223946.53	7048974.81	496.60	248	-60	48	14	42	28	0.07	1.23
WCN22RC426	223738.79	7048839.46	499.97	248	-60	30	7	25	18	0.1	1.14
WCN22RC427	223841.83	7048874.20	502.95	248	-60	15	5	9	4	0.13	1.11
WCN22RC428	223939.37	7048915.68	499.52	248	-60	42	13	23	10	0.08	1.11
WCN22RC429	223722.92	7048769.32	498.52	248	-60	24	9	18	9	0.07	1.47
WCN22RC430	223762.47	7048788.56	500.42	248	-60	30	9	20	11	0.08	1.20
WCN22RC432	223894.01	7048841.36	503.32	248	-60	24	9	16	7	0.09	1.04
WCN22RC433	223942.52	7048859.46	503.28	248	-60	24	6	14	8	0.06	1.05
WCN22RC434	223992.42	7048874.99	500.63	248	-60	42	17	19	2	0.03	0.76
WCN22RC435	224038.22	7048895.98	498.05	248	-60	54	14	41	27	0.06	1.04
WCN22RC436	223779.07	7048732.87	498.87	248	-60	30	7	18	11	0.07	1.14
WCN22RC437	223868.82	7048775.74	501.39	248	-60	30	10	22	12	0.04	1.15
WCN22RC438	221469.09	7052880.96	505.99	248	-90	48	33	42	9	0.11	1.27
WCN22RC440	217159.87	7058831.71	525.91	248	-60	42	20	25	5	0.07	0.94
WCN22RC441	217928.81	7059145.07	519.27	248	-60	72	50	57	7	0.15	1.36
WCN22RC443	218011.02	7058734.49	517.75	248	-60	72	41	58	17	0.04	0.99
WNP013	217437.63	7060027.98	474.76	0	-90	72	37	61	24	0.026	0.60
WNP014	217474.30	7060049.02	477.78	0	-90	72	41	51	10	0.054	0.75
WNP015	221583.36	7052749.20	464.51	0	-90	48	37	44	7	0.055	0.87
WNP016	221904.58	7052465.75	471.75	0	-90	70	29	36	7	0.026	0.53
WR01518	221296.89	7052272.34	479.26	269	-60	60	22	32	10	0.027	0.43