



LARGEST AUSTRALIAN INDICATED HEAVY REE RESOURCE CONFIRMED

Rapidly emerging as Australia's premier heavy REE and critical defence minerals supplier

Victory Metals Limited (**ASX: VTM**) (**Victory or the Company**) is pleased to announce an updated Mineral Resource Estimate (**MRE**) for its North Stanmore Heavy Rare Earth Elements (**HREE**) dominant Project (**North Stanmore**).

Key Highlights:

- **Total updated MRE of 235Mt, of which 149Mt (63%) resides in the indicated category, representing the largest Indicated Mineral Resource of Australian HREE-dominant deposits:**
 - **79,200t** contained Indicated MRE Total Rare Earth Oxides (TREO)¹
 - **28,000t** contained Indicated MRE Heavy Rare Earth Oxides (HREO)²
 - **3,010t** contained Indicated MRE Dy₂O₃ + Tb₄O₇.
- **Near surface higher-grade domain of 45.9Mt at 1,050ppm TREO** (Figure 3), supports a development strategy designed to rapidly deliver new HREE supply to address global demand³.
- **Premium HREE ratio of 35% HREO/TREO for the Resource.**
- **High-value by-product Hafnium (Hf) confirmed, a critical metal with key applications in defence functions and the aerospace industry.**
- Beneficiation amenability demonstrated, with **+60% feed grade uplift enabling the potential for further upgrade of higher-grade domain material to an average of 1,662ppm TREO⁴.**
- Significant additional Resource growth potential, with mineralisation open in all directions and **92% of the tenement area remaining unexplored.**
- Initial process test work achieves **high REE recoveries with low temperature, short leach time, low acid consumption, low-cost acids, low radioactivity, and low impurities⁵.**
- **Set to contribute to the global drive for new, ethically sourced non-Chinese heavy rare earth supply options.**
- The Australian domiciled North Stanmore project **benefits from political stability and a supportive Government that offers numerous attractive funding initiatives.**
- July 2024 updated MRE set to **underpin the completion of a Scoping Study** (expected Q3 2024), support the application of a Mining Licence, and accelerate ongoing strategic partnership and offtake discussions.

¹ TREO (Total Rare Earth Oxide) = La₂O₃ + CeO₂ + Pr₆O₁₁ + Nd₂O₃ + Sm₂O₃ + Eu₂O₃ + Gd₂O₃ + Tb₄O₇ + Dy₂O₃ + Ho₂O₃ + Er₂O₃ + Tm₂O₃ + Yb₂O₃ + Lu₂O₃ + Y₂O₃ + Sc₂O₃.

² HREO (Heavy Rare Earth Oxide) = Eu₂O₃ + Gd₂O₃ + Tb₄O₇ + Dy₂O₃ + Ho₂O₃ + Er₂O₃ + Tm₂O₃ + Yb₂O₃ + Lu₂O₃ + Y₂O₃.

³ 600ppm TREO cut-off

⁴ Refer VTM ASX release dated 19 March 2024, Rare Earth Grades Significantly Increase From Low-Cost Method

⁵ Refer VTM ASX release dated 14 May 2024, North Stanmore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries

Victory’s CEO and Executive Director Brendan Clark, commented:

“Our July 2024 MRE serves as confirmation of our superb mineral endowment and spotlights our significant potential to deliver future Australian production of high-value, critical materials required for the energy transition, national defence and beyond.

North Stanmore’s location in the Mid-West region of Western Australia, along the Great Northern Highway and just 6km from the Cue township, enables access to excellent established infrastructure, providing significant potential economic benefits and opportunities to expedite any potential future mine development.

Critically, North Stanmore’s regolith clay-hosted mineralisation overlying an alkaline intrusion is expected to allow for highly efficient mixed rare earth carbonate production that is heavy rare earth dominant, and therefore significantly more valuable than the majority of REE projects currently in development globally.

This dynamic has driven significant interest from potential off-take partners seeking primarily heavy rare earth element (vs light rare earth element) security of supply who have compared the North Stanmore HREE enriched deposit to existing world class HREE operations in southern China.

Our successful exploration and advancement efforts to date are set to be supported by the completion of a Scoping Study during Q3 2024. This preliminary technical and economic evaluation of North Stanmore is expected to highlight the clear potential for Victory to become a future supplier of choice for HREE, scandium, and hafnium, as well as an important and preferred partner for the global defence industry. This latter dynamic has been recognised via our approved registration as a NATO Commercial and Government Entity, which enables us to apply for US Department of Defence funding grants and other future funding support.

We are excited about the future of North Stanmore with multiple strategic commercial discussions currently underway”.

Australia’s premier HREE deposit: North Stanmore June 2024 updated MRE composition

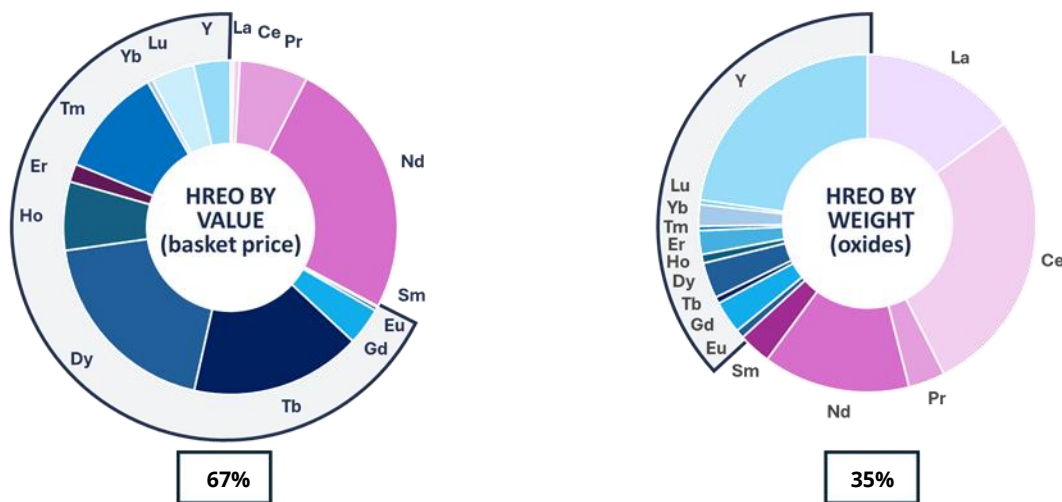


Figure 1: North Stanmore July 2024 updated MRE composition by percentage value (left hand side) and percentage weight (right hand side)^{6,7}

⁶ Mineral Resource composition by value uses based on 2025 forecast by Statistica and from Asian Metal Exchange, Argus and Rare Metal Tech.
⁷ Basket prices per kg US\$ are La₂O₃: \$1.23, CeO₂: \$1.28, Pr₆O₁₁: \$108.17 Nd₂O₃: \$105.90 + Sm₂O₃: \$2.52 + Eu₂O₃: \$27.58 Gd₂O₃: \$66.59 + Tb₄O₇: \$1,810.65, Dy₂O₃: \$329.34, Ho₂O₃: \$531.00, Er₂O₃: \$46.00, Tm₂O₃: \$1,893.00, Yb₂O₃: \$14.00, Lu₂O₃: \$756.00 + Y₂O₃: \$9.14

North Stanmore July 2024 updated Mineral Resource Estimate

The July 2024 updated North Stanmore MRE was completed by leading geological consultancy, MEC Mining.

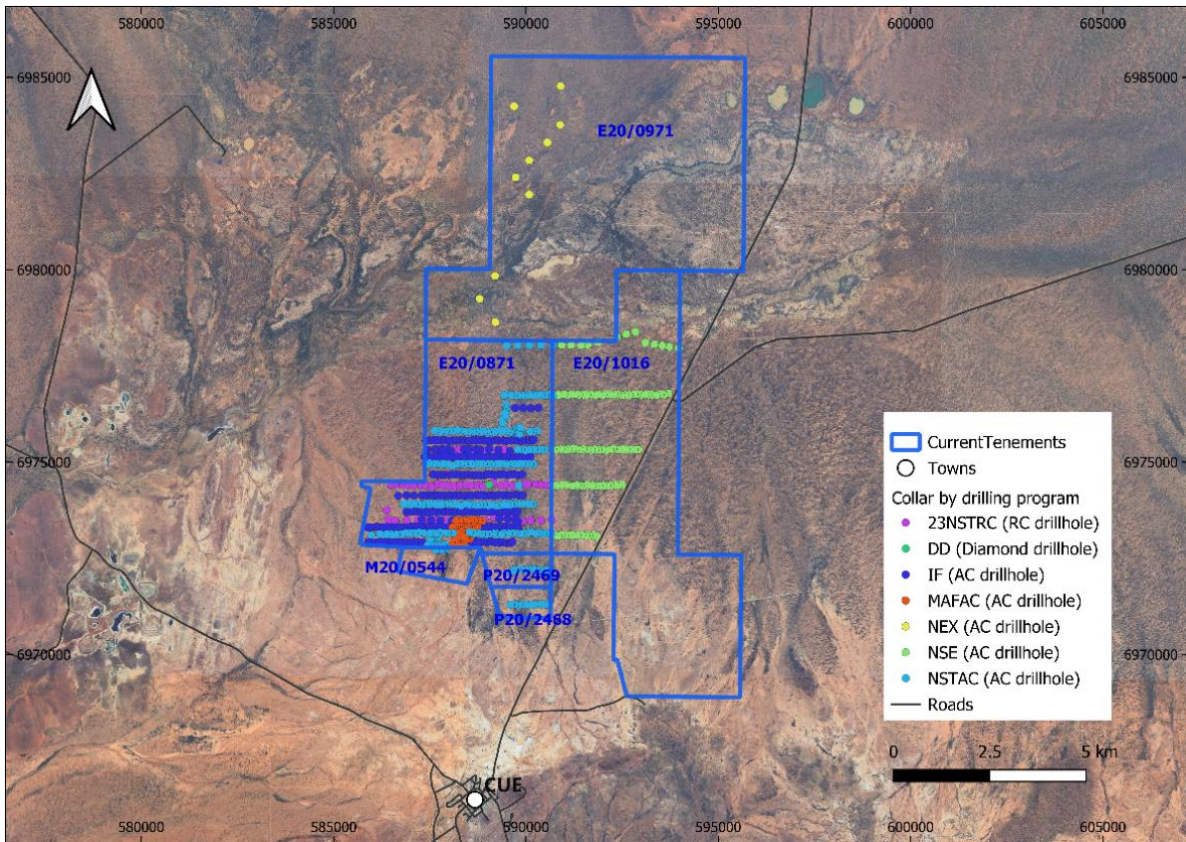


Figure 2: Victory drill holes at North Stanmore completed between 2022 and 2023

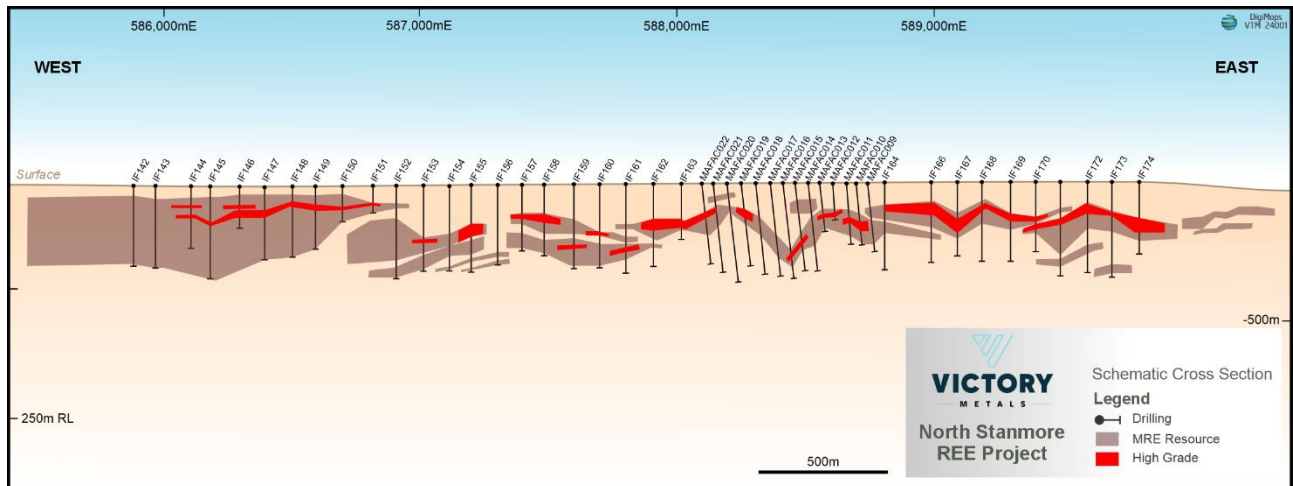


Figure 3: Schematic Cross Section of the July 2024 updated MRE showing drill hole locations and high-grade mineralised zone (red)

The July 2024 updated MRE (refer Table 1) is stated at an economic cut-off grade of ≥ 330 ppm TREO, with no top cuts (as no extreme values that could bias the estimation were apparent). Table 1 is the summary report for the grouped REO, Table 2 outlines the higher-grade domain and associated classification, and Table 3 outlines the lower-grade domain by classification.

Table 1: North Stanmore July 2024 MRE ($\geq 330\text{ppm}$ TREO cut-off grade)

RESOURCE CLASSIFICATION	MRE TONNES (t)	TREO (ppm)	HREO (ppm)	LREO (ppm)	HREO/TREO (%)	Sc ₂ O ₃ (ppm)
INDICATED	149,020,000	532	188	316	35	31
INFERRED	86,130,000	500	165	310	33	24
TOTAL	235,150,000	520	180	314	35	29

Numbers are rounded to reflect they are an estimate.

Numbers may not sum due to rounding.

Table 2: North Stanmore July 2024 MRE higher-grade domain only ($\geq 600\text{ppm}$ TREO cut-off grade)

RESOURCE CLASSIFICATION	MRE TONNES (t)	TREO (ppm)	HREO (ppm)	Eu ₂ O ₃ (ppm)	Gd ₂ O ₃ (ppm)	Tb ₄ O ₇ (ppm)	Dy ₂ O ₃ (ppm)	Ho ₂ O ₃ (ppm)	Er ₂ O ₃ (ppm)	Tm ₂ O ₃ (ppm)	Yb ₂ O ₃ (ppm)	Lu ₂ O ₃ (ppm)	Y ₂ O ₃ (ppm)
INDICATED	32,780,000	1,025	338	8.1	32	5.3	33	6.8	20	2.9	19	2.8	208
INFERRED	13,110,000	1,113	374	9.0	35	5.8	35	7.4	22	3.1	20	2.8	234
TOTAL	45,890,000	1,050	338	8.3	33	5.4	33	7.0	21	3.0	19	2.8	215

Numbers are rounded to reflect they are an estimate.

Numbers may not sum due to rounding.

Table 3: North Stanmore July 2024 MRE lower-grade domain only ($\geq 330\text{ppm}$ TREO cut-off grade)

RESOURCE CLASSIFICATION	MRE TONNES (t)	TREO (ppm)	HREO (ppm)	Eu ₂ O ₃ (ppm)	Gd ₂ O ₃ (ppm)	Tb ₄ O ₇ (ppm)	Dy ₂ O ₃ (ppm)	Ho ₂ O ₃ (ppm)	Er ₂ O ₃ (ppm)	Tm ₂ O ₃ (ppm)	Yb ₂ O ₃ (ppm)	Lu ₂ O ₃ (ppm)	Y ₂ O ₃ (ppm)
INDICATED	116,240,000	392	146	2.5	12	2.1	13	2.9	9	1.3	9	1.4	92
INFERRED	73,020,000	390	128	2.4	11	1.9	12	2.6	8	1.2	8	1.2	80
TOTAL	189,260,000	391	139	2.5	12	2.0	13	2.8	9	1.3	9	1.3	87

Numbers are rounded to reflect they are an estimate.

Numbers may not sum due to rounding.

The July 2024 updated MRE includes a higher-grade domain containing Indicated Mineral Resources of **32.8Mt at 1,025ppm TREO (refer Table 2).**

Approximately 63% of the July 2024 MRE is classified as Indicated, with the remainder being classified as Inferred Mineral Resources (refer Figure 4).

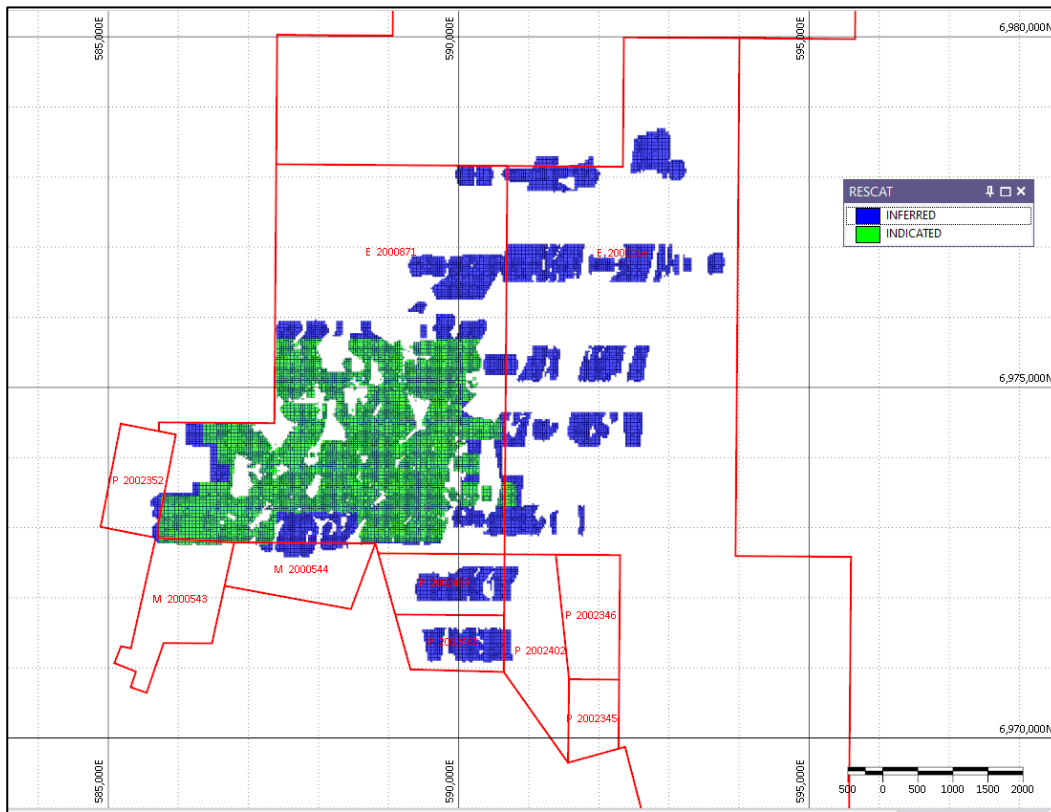


Figure 4. Plan view surface projection of the June 2024 updated MRE by classification type (Green = Indicated, Blue = Inferred)

The light rare earth oxides (LREO) for the July 2024 North Stanmore MRE are reported by individual elements in Tables 4. Table 5 reports the nickel, cobalt, copper, and hafnium by-products.

Table 4 July 2024 MRE LREO Grades by domain and classification (≥ 330 ppm TREO cut-off grade)

DOMAIN	RESOURCE CLASSIFICATION	TONNES (t)	LREO (ppm)	La ₂ O ₃ (ppm)	CeO ₂ (ppm)	Pr ₆ O ₁₁ (ppm)	Nd ₂ O ₃ (ppm)	Sm ₂ O ₃ (ppm)
Higher-grade	INDICATED	32,780,000	656	154	280	38	150	32
Higher-grade	INFERRED	13,110,000	716	187	285	43	166	35
Higher-grade	TOTAL	45,890,000	673	164	281	40	155	33
Lower-grade	INDICATED	116,240,000	220	50	99	12	48	11
Lower-grade	INFERRED	73,020,000	237	56	108	13	50	11
Lower-grade	TOTAL	189,260,000	227	52	102	12	49	11
Total	TOTAL	235,150,000	314	74	137	18	69	15

Numbers are rounded to reflect they are an estimate.

Numbers may not sum due to rounding.

Table 5: July 2024 updated MRE Ni, Co, Cu, Hf ($\geq 330\text{ppm}$ TREO cut-off grade)

DOMAIN	RESOURCE CLASSIFICATION	Tonnes (Mt)	Ni	Co	Cu	Hf
			(ppm)	(ppm)	(ppm)	(ppm)
Higher-grade	INDICATED	33	36	32	43	6
Higher-grade	INFERRED	13	42	25	54	5
Higher-grade	TOTAL	46	38	30	46	6
Lower-grade	INDICATED	116	26	17	28	6
Lower-grade	INFERRED	73	33	16	35	6
Lower-grade	TOTAL	189	29	16	31	6
Total	INDICATED	149	28	20	31	6
Total	INFERRED	86	34	17	38	6
Total	TOTAL	235	30	19	34	6

Numbers are rounded to reflect they are an estimate.
Numbers may not sum due to rounding.

Total contained Indicated and Inferred estimated rare earth oxides in the updated July 2024 MRE include:

- **42,200t HREO** including:
 - 4,000t Dy_2O_3
 - 600t Tb_4O_7
- **73,800t LREO** including:
 - 16,300 Nd_2O_3
 - 4,200 Pr_6O_{11}

Figure 5 is a cross-section view through North Stanmore (looking north) showing the updated July 2024 MRE Ore Block Model (OBM) by TREO grade.

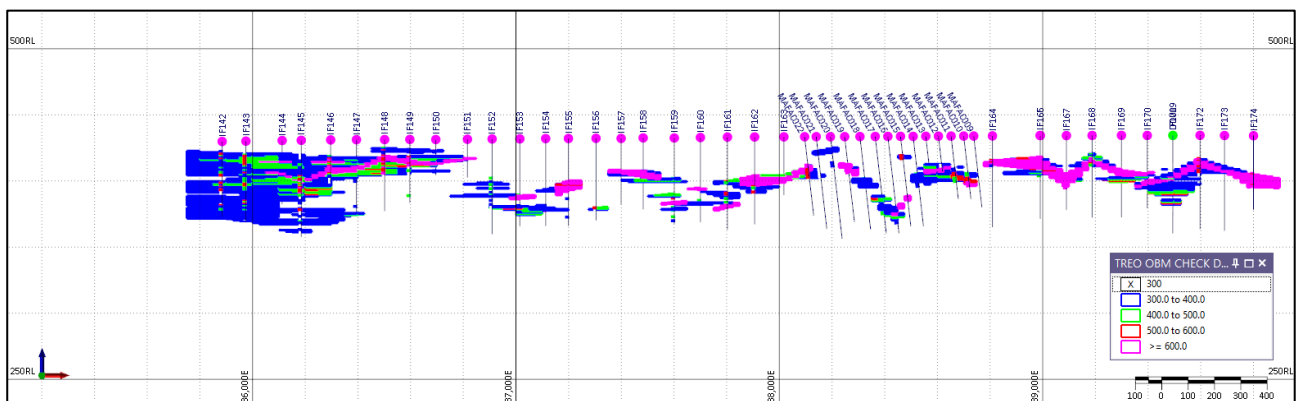


Figure 5: Cross section view of North Stanmore deposit by Ore Block Model grade designation (Section line 6,973,310N, VE x5)

The North Stanmore deposit benefits from low concentrations of the radioactive elements uranium (U) and thorium (Th). The mineralisation has average sample grades of 2ppm U (maximum value of 24ppm) and 7ppm Th (maximum values of 68ppm).

The grade-tonnage curve for the updated July 2024 MRE (Indicated and Inferred) is shown below in Figure 6.

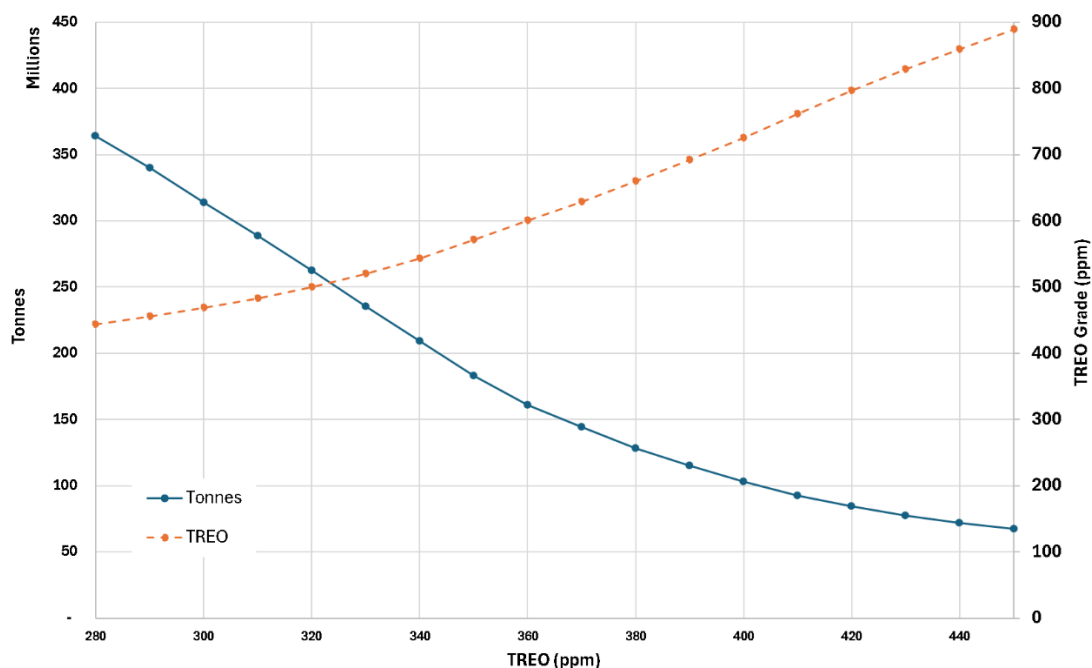


Figure 6: Grade-tonnage curve for North Stanmore updated July 2024 MRE Indicated and Inferred Mineral Resources

Summary of key material information used to estimate the Mineral Resources

The following is a summary of material information used to update the estimate of Mineral Resources as required by Listing Rule 5.8.1 and JORC 2012 Reporting Guidelines.

Additional July 2024 MRE detail

Project background

The 100%-owned North Stanmore Project is located in Western Australia, approximately 6km north of Cue, with sealed road access via the Great Northern Highway, Figure 7.



Figure 7: North Stanmore Project plan overview

The July 2024 MRE has been estimated within the boundary of six tenements; E20/0971, E20/1016, E20/0871, M20/0544, P20/2468, and P20/2469. All tenements are held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory.

Regional Geology

Victory's tenements lie within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgarranga greenstone belts, the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late faults. The greenstone belts were intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. Two large Archaean gabbroic intrusions occur south of Cue. These are the Dalgarranga-Mount Farmer gabbroic complex in the southwest, and the layered Windimurra gabbroic complex in the southeast.

Project Geology

Victory's REE discovery occurs in regolith above the North Stanmore alkaline intrusion, discovered north of Cue. Despite its magnetic signature, the North Stanmore intrusion had not been recognised previously on regional geological maps. Petrological data⁸ for samples of diamond core indicate that the intrusion is post-tectonic and hence post-Archean in age.

The North Stanmore Intrusion is a large (approximately 16km by 5 km) differentiated ultramafic to felsic intrusion. Lithologies identified in thin section include kaersutite and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro (ijolite), diorite, monzonite and syenite. Some regolith samples are strongly LREE enriched indicating that the intrusion also contains carbonatite. However, the uniformly high HREO/TREO of the regolith (of approximately 34% to 38%) indicates that carbonatite represents a subordinate phase in the intrusion.

The North Stanmore Intrusion is interpreted to be associated with an early Proterozoic plume track that was responsible for alkaline magmatism extending in a broad belt from Mt Weld carbonatite near Laverton through Leonora to Cue⁹.

Deposit Type

The rare earth element mineralisation occurs in a relatively flat-laying saprolite-rich clay horizon beneath a veneer of unconsolidated colluvium that ranges in thickness from 0m to 36m. The uniformity of Nb/Ta ratios (Nb/Ta 16±4) in the regolith above the North Stanmore Intrusion indicates that the regolith developed *in situ*. Importantly, studies have shown that Nb/Ta ratio of regolith over carbonatites and other alkaline intrusions closely resembles the Nb/Ta ratio of their source plume generated lithologies¹⁰.

Mineralised REE saprolite horizons above the North Stanmore Intrusion occur at depths between 12m and 77m. Ce/Ce* tracks regolith oxidation, and the upper parts of regolith enrichment zones have Ce/Ce* >1 reflecting gain of mobile Ce⁴⁺, while the lower parts of enrichment zones have Ce/Ce* <1. Leachable clay REE deposits all have Ce/Ce* <1. The Ce/Ce* of the June 2024 updated MRE in the Indicated category is 0.86 (Tables 1 to 4).

REEs are complexed with carbonate ions [CO₃²⁻] and bicarbonate ions [HCO₃⁻] or occur as REE³⁺ ions in soil as groundwater migrates downwards during tropical weathering. Based on Ce/Ce* systematics¹¹ and TREO concentrations, there appear to be four zones of REE enrichment at North Stanmore. These are 15m to 25m, 28m to 37m, 41m to 46m and a deeper zone between 53m and 77m. The regolith is complex and importantly some cores exhibit two zones of REE enrichment.

REEs are adsorbed onto kaolinite or form secondary REE phosphates, rhabdophane (after monazite), churchite (after xenotime), and florencite. QEMSCAN mineralogical studies show that the REEs are mainly hosted by <20-µm particles.

Scandium is enriched throughout the regolith profile due to the breakdown of pyroxene in the North Stanmore source lithologies. Sc is generally considered to behave differently to the REEs, which are adsorbed as outer-sphere complexes on clay surfaces, found in Al(OH)₂SiO sites, or occur as

⁸ Refer VTM ASX release dated 10 August 2022, *Major Alkaline Igneous Complex Discovered*

⁹ Fiorentini et al., (2020) Nature Sci. Repts. 10:19729

¹⁰ Cornelius et al, (2005) Geochemistry: Exploration, Environment, Analysis, Vol. 5, 291–310; Zhukova et al., (2021) Ore Geology Reviews 139, 104539

¹¹ Ce/Ce* = (2*(Ce_N)/(La_N+Pr_N)), where Ce_N, La_N and Pr_N are chondrite normalised values; La_N = La concentration /0.237,

Ce_N = Ce concentration /0.613 and Pr_N = Pr concentration/0.0928; Ce/Ce* ratios >1 reflect the gain of Ce⁴⁺ at shallower regolith depths while Ce/Ce* ratios <1 reflect the loss of mobile Ce⁴⁺ from deeper parts of weathering profiles that contain Ce³⁺.

hydrated REE bearing phosphates. However, Sc^{3+} behaves like the transition metals (Ni^{2+} , Co^{2+} , Cu^{2+}) and, due to its smaller ionic radius, it adsorbs onto vacancy sites in clay lattices or attaches to the surface of Mn oxides¹². Sc is enriched throughout the regolith profile.

REOs

Yttrium is classified as a REE because of its similar ionic radius to the lanthanides, and similar chemical properties to the HREEs.

Scandium, a highly valuable critical element occurs in the same Group of the Periodic Table (Gp. 3) as the lanthanides. It occurs predominantly in HREE bearing ultramafic and mafic igneous like the North Stanmore Intrusion. By contrast, felsic alkaline rocks and granitoids are more LREE enriched and contain negligible amounts of Sc contents. The chemical properties of Sc are distinct from the other REEs, and Sc has recently been recognised to have superconducting properties. Sc has been deemed a critical mineral due to current Chinese and Russian control of the supply chain.

REE analytical data was determined by ALS using the ME-MS81 technique of fusion digestion followed by ICPMS analysis. Results were returned in elemental form and were converted to oxides.

TREO (Total Rare Earth Oxides), LREO (Light Rare Earth Oxides), HREO (Heavy Rare Earth Oxides), MREO (Magnet Rare Earth Oxides), and the ratio of HREO/TREO were calculated as follows:

- **TREO** is the sum of La_2O_3 , CeO_2 , Pr_6O_{11} , Nd_2O_3 , Sm_2O_3 , Eu_2O_3 , Gd_2O_3 , Tb_4O_7 , Dy_2O_3 , Ho_2O_3 , Er_2O_3 , Tm_2O_3 , Yb_2O_3 , Lu_2O_3 , Y_2O_3 , and Sc_2O_3 . This follows the protocol recommended by the International Union of Pure and Applied Chemistry.¹³ Yttrium and Scandium are included as they share Group IIIA properties in the Periodic Table with the lanthanides. Importantly, yttrium exhibits similar geochemical properties to the HREOs.
- **HREO** is the sum of Eu_2O_3 , Gd_2O_3 , Tb_4O_7 , Dy_2O_3 , Ho_2O_3 , Er_2O_3 , Tm_2O_3 , Yb_2O_3 , Lu_2O_3 , and Y_2O_3 .
- **LREO** is the sum of La_2O_3 , CeO_2 , Pr_6O_{11} , Nd_2O_3 , and Sm_2O_3 .
- **MREO** (Magnet Rare Earth Oxides) are the rare earths used in the production of magnets predominantly, Nd_2O_3 , Pr_6O_{11} (**NdPr**) and Dy_2O_3 , Tb_4O_7 (**DyTb**).
- HREO/TREO is the ratio of the sum of Eu_2O_3 , Gd_2O_3 , Tb_4O_7 , Dy_2O_3 , Ho_2O_3 , Er_2O_3 , Tm_2O_3 , Yb_2O_3 , Lu_2O_3 , and Y_2O_3 / sum of La_2O_3 , CeO_2 , Pr_6O_{11} , Nd_2O_3 , Sm_2O_3 , Eu_2O_3 , Gd_2O_3 , Tb_4O_7 , Dy_2O_3 , Ho_2O_3 , Er_2O_3 , Tm_2O_3 , Yb_2O_3 , Lu_2O_3 , Y_2O_3 , and Sc_2O_3 .

Drilling techniques

Drilling at North Stanmore to support the June 2024 updated MRE includes five hundred and twenty-two (522) drill holes for 31,190m, inclusive of 462 Air-core (AC) drillholes for 27,347m, 49 Reverse Circulation (RC) drillholes for 3,076m, and 11 diamond drill holes for 765m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2023. The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m (Figure 2 and Figure 3).

Sampling and sample analysis

AC and RC sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. Most 1-meter samples were dry and weighed between 1.5kgs and 2.5 kgs. Samples from the cyclone were

¹² Zhang et al., (2024) Am. Mineralogist

¹³ Williams Jones and Vasyukova (2018) Economic Geology

placed into green drill bags in laid out orderly rows on the ground. Using a hand-held trowel, 1m samples were collected from the one-meter drill bags after splitting of the sample. These samples were placed into calico bags and weighed between 1.5kgs and 2.5 kgs. Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory.

Lithology

Logging was completed for 90% of the sample intervals and used to produce surfaces to delineate the colluvium, saprolite, and basement.

The basement source lithologies include kaersutite and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro (ijolite), diorite, monzonite and syenite. Carbonatite represents a subordinate phase in the intrusion.

Domaining

The TREO grade distribution was reviewed and assessed spatially and 150ppm TREO was identified as the on-set of TREO mineralisation within the saprolite profile. Within the 150ppm envelope, there was a discrete high-grade population at approximately ≥ 600 ppm TREO.

Density

Regression analysis was performed to compare the in situ downhole geophysical density to the dry bulk density determinations from the diamond core and obtain a calibration factor to convert the downhole geophysical density to a dry bulk density value. Samples were grouped and analysed by mineralised domain and categorised as higher-grade, lower-grade and waste. A mean regressed density for the high-grade domain was calculated to be 1.75t/m^3 , with 2.02t/m^3 calculated for the lower-grade domain

Estimation Methodology

A geological cutoff grade of 150ppm TREO was used to separate mineralised from unmineralised material for the low-grade domain. A high-grade domain was modelled above a TREO 600ppm cut-off.

The updated July 2024 MRE is reported above an economic cut-off grade of 330ppm TREO, no top cuts were applied as no extreme values that could bias the estimation were apparent.

Assays samples were composited to 1-metre lengths, with the geology model wireframes assigned to the assay file. The composite grade within the wireframes was used to model the experimental variogram using two components to fit spherical models.

Ordinary Kriging (OK) was used to estimate all rare earth oxides as individual elements. Inverse Distance Cubed was then used to estimate remaining potential credit elements (scandium, nickel, cobalt, copper, and hafnium).

The OBM parent blocks were 50m x 50m east/west and north/south, and 1-metre in elevation, sub celled to 25m by 25m east/west and north/south, and 0.5-metre elevation. All blocks were restricted to the geological wireframes.

Mineral Resource Classification

Mineral Resources are classified as Indicated and Inferred. Unclassified material has been included in an Exploration Target. Indicated Mineral Resource classification was based on drillhole spacing

(250m by 100m, closing to 50m by 50m), acceptable underlying QAQC, and a DGPS survey of drillhole collars.

The DGPS survey provided increased certainty regarding the drillhole collar location and compensated for a low-resolution topography survey. The topographical surface was adjusted to include the DGPS surveyed drillhole collar coordinates.

Approximately 63% by tonnage of the updated July 2024 MRE is classified as Indicated Mineral Resources and approximately 37% by tonnage is classified as Inferred Mineral Resources.

Validation

All ore block models were validated globally and locally. Global validation compared the wireframe volume and grade with the ore block model volume and grade, at a zero-cut-off grade. The global volume comparison between the wireframes and the sub celled ore block models was close. The global grade comparisons of grade within the wireframes compared to the modelled grades is within 10%, with small differences occurring due to the clustering of grades within the wireframes.

Local validation was completed by comparing the composite grades used to estimate the block values against the estimated block values. There was close correlation between composite assays and estimated block grades, with some small differences resulting from the smoothing effect of ordinary kriging. Min/max checks were utilised to ensure all blocks were populated. OBM validation functions were used to check for overlapping blocks, there were no incidence of overlapping blocks.

Metallurgical Testwork

Three stages of metallurgical test work have been completed on the North Stanmore Project, focusing on beneficiation, and leach test work to establish potential recoveries and processing options.

Core Resources (**Core**) located in Brisbane completed the third stage of test work including beneficiation test work in March of 2024 and reported that the REE feed grade increased 63% by rejecting the +53 μ m feed material from across all samples. Core also completed leach test work on the beneficiated material¹⁴

The leach test work program involved diagnostic metallurgical testing on a composite blend of the beneficiated samples with a head grade of 1,283 ppm TREO. This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) as well as the less valuable light rare earth elements Pr (94%), Nd (94%), with a combined recovery of 93% MREE.

Scandium recoveries of 50% had previously been achieved, with optimisation work occurring in parallel. These assays were conducted by Australian Laboratory Services Brisbane. The objective of the diagnostic test work was to recover REE and Sc from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).

¹⁴ Refer VTM ASX release dated 14 May 2024, North Stanmore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries Refer VTM ASX release dated 14 May 2024, North Stanmore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries

Reasonable Prospects Hurdle

Clause 20 of the JORC (2012) Code requires that all reports of Mineral Resources must have reasonable prospects for eventual economic extraction, regardless of the classification of the resource. MEC Mining deems that there are reasonable prospects for eventual economic extraction using open pit mining on the following basis:

- North Stanmore Mineral Resources occur close to surface and are believed to be amenable to an opencut mining operation.
- Metallurgical testwork has returned very favourable process recovery results.
- The North Stanmore Project is situated approximately 6km from the Cue township and approximately 420km to Geraldton Port via the Great Northern Highway, one of West Australia's major arterial road networks.

This announcement has been authorised by the Board of Victory Metals Limited.

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Victory Metals Limited

Victory is focused upon the exploration and development of its Heavy Rare Earth Element and critical mineral discovery in the Cue Region of Western Australia. Victory's key assets include a portfolio of assets located in the Midwest region of Western Australia, approximately 665 km from Perth. Victory's clay REE discovery is rapidly evolving with the system demonstrating high ratios of Heavy Rare Earth Oxides and Critical Magnet Metals NdPr + DyTb.

Competent Person's Statement

The information in this announcement that relates to the Mineral Resource estimate is derived from information compiled by Mr Dean O'Keefe, a Fellow of the Australasian Institute of Mining and Metallurgy (FAusIMM, #112948) and Mr Kahan Cervoj, a Member of the Australasian Institute of Mining and Metallurgy (MAusIMM, #211785), co Competent Persons for this style of mineralisation. Mr O'Keefe and Mr Cervoj are consultants to Victory Metals Limited, and are fulltime employees of MEC Mining Pty Ltd, an independent mining and exploration consultancy. Both Mr O'Keefe and Mr Cervoj have sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which they are undertaking to qualify as Competent Person as defined in the 2012 edition of the Australasian Code for the Reporting of Exploration Results, Mineral Resources, and Ore Reserves (JORC Code). The co Competent Persons are not aware of any new information or omission of data that may materially affect the stated Mineral Resource estimate.

APPENDIX 1: JORC CODE TABLE 1

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<p>Sampling techniques</p>	<ul style="list-style-type: none"> Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information 	<ul style="list-style-type: none"> Victory Metals Australia (ASX:VTM) completed one Air-core (AC) drilling campaign and a diamond drilling program at North Stanmore during the period September-December 2023. Victory Metals Australia (ASX:VTM) completed a reverse circulation (RC) drilling programme a reverse circulation (RC) drilling programme from January–March 2023. (AC) holes were drilled vertically and spaced 100m apart along 200m - 400m spaced drill lines. (AC) drilling samples were collected as 1-m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the split sample was placed into calico sample bags for transport to Perth. Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5 kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg. A reputable commercial transport company was used to transport the bags. A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Nd and Y) from the 1-m sample piles. pXRF reading times were 45 secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards. The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (La, Ce, Nd and Y) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory's secure warehouse in Perth. Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight. RC drill samples were collected as 1-m samples from the rig cyclone and placed on top of black plastic, which was laid on the natural ground surface to prevent contamination, in separate piles and in orderly rows. A hand-held trowel was used to collect 4-m composite samples from the 1-m piles. Compositing did not account for lithology changes. These composite samples weighed between 2 and 3 kg
<p>Drilling techniques</p>	<ul style="list-style-type: none"> Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face- 	<ul style="list-style-type: none"> (AC) drilling uses a three bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and feature an inner tube with an outer barrel (similar to RC drilling). (AC) drilling uses small compressors (750 cfm/250 psi) to drill holes into the weathered layer of loose soil and fragments of rock.

Criteria	JORC Code explanation	Commentary
	<p>sampling bit or other type, whether core is oriented and if so, by what method, etc.).</p>	<ul style="list-style-type: none"> (RC) Drilling used a 5½" face sampling hammer with 1,350cfm/500 psi onboard compressor, which was occasionally supplemented with an additional booster (2,100cfm/1,000 psi). After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rods inside wall, which flushes the cuttings up and out of the drill hole through the rod's inner tube, causing Less chance of cross-contamination. (AC) drill rigs are lighter in weight than other rigs, meaning they are quicker and more manoeuvrable in the bush. (AC) Drilling was performed by Seismic Drilling Pty Ltd and Orlando Drilling Pty Ltd, and the RC drilling was performed by Orlando Drilling Pty Ltd. The drill rigs were regularly inspected by VTM personnel and contract staff. The drill rig with automatic rod handlers, with fire and dust suppression systems, mobile and radio communications, qualified and ticketed safety trained operators and offsideers, are required by Victory's work health and safety systems.
<p>Drill sample recovery</p>	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	<ul style="list-style-type: none"> The majority of samples were dry and sample recovery was variable, where excessive water flows were encountered during drilling. Representative percussion drillhole samples were collected as 1-meter intervals, with corresponding chips placed into chip trays and kept for reference at VTM's facilities. Measures taken to ensure sample representivity and recovery included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.
<p>Logging</p>	<ul style="list-style-type: none"> Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. 	<ul style="list-style-type: none"> All percussion samples in the chip trays were lithologically logged using standard industry logging software on a notebook computer. All (AC) samples have been logged for lithology, alteration, quartz veins, colour, fabrics. All (AC) samples have been analysed by a handheld pXRF. All samples were subjected to a NIR spectrometer for the identification of minerals and the variations in mineral chemistry to detect alteration assemblages and regolith profiles. All geological information noted above has been completed by a competent person as recognized by JORC.
	<ul style="list-style-type: none"> Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography. 	<ul style="list-style-type: none"> Logging is qualitative in nature. (AC) samples have been photographed.
	<ul style="list-style-type: none"> The total length and percentage of the relevant intersections logged. 	<ul style="list-style-type: none"> 90% of the sample intervals were logged.

Criteria	JORC Code explanation	Commentary
Subsampling techniques and sample preparation	<ul style="list-style-type: none"> If core, whether cut or sawn and whether quarter, half or all core taken. 	<ul style="list-style-type: none"> Diamond drilling was PQ core. Half core samples were taken, with the exception of when a field duplicate was collected and then the samples were quarter core.
	<ul style="list-style-type: none"> If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry. 	<ul style="list-style-type: none"> Air core and RC sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. Most 1-meter samples were dry and weighed between 1.5 and 2.5 kgs. Samples from the cyclone were placed into green drill bags in laid out in orderly rows on the ground. Using a hand-held trowel, 1m samples were collected from the one-meter drill bags after splitting of the sample. These samples were placed into calico bags and weighed between 1.5 and 2.5 kgs.
	<ul style="list-style-type: none"> For all sample types, the nature, quality and appropriateness of the sample preparation technique. 	<ul style="list-style-type: none"> Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include: <ul style="list-style-type: none"> ME-4ACD81: Four acid digestion followed by ICP-AES measurement ME-MS81: Lithium borate fusion followed by acid dissolution and ICP-AES measurement ME-ICP06: Fusion decomposition followed by ICP-AES measurement REOs were all analysed by ME-MS81 (four acid digestion followed by ICP-AES measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors. Base metals are assayed by ME-ICP06: Fusion decomposition. Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.
	<ul style="list-style-type: none"> Quality control procedures adopted for all subsampling stages to maximise representivity of samples. 	<ul style="list-style-type: none"> Using a riffle splitter, 1m composite samples were collected from the individual sample bags. Quality control of the assaying comprised the collection of a duplicate sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples.
	<ul style="list-style-type: none"> Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling. 	<ul style="list-style-type: none"> Fourteen field duplicates of quarter core (diamond PQ) were compared to the original sample for each REO element and results were found to be acceptable.
	<ul style="list-style-type: none"> Whether sample sizes are appropriate to the grain size of the material being sampled. 	<ul style="list-style-type: none"> Composite samples weighed between 1 and 2 Kg's. Sample sizes are considered appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. 	<ul style="list-style-type: none"> All samples were analysed in the field using a handheld Olympus Vanta XRF unit to identify geochemical thresholds. These results are not considered dependable without calibration using chemical analysis. They were used as a guide to the relative presence or absence of certain elements, including REOs to help guide the drill program and which samples were submitted for analytical analysis. All pXRF anomalous samples were sent to ALS Wangarra in Perth for analysis. Samples were submitted for sample preparation and geochemical analysis by ALS in Wangara, Perth, a NATA accredited laboratory underwent lithium borate fusion prior to acid dissolution and ICP-AES (ALS method ME-

Criteria	JORC Code explanation	Commentary
		<p>MS81, a total assay technique) for Ba, La, Ce, Cr, Cs, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Sc, Sm, Sn, Sr, Ta, Tm, Yb, Lu, Y, Th, & U.</p> <ul style="list-style-type: none"> Ag, As, Cd, Co, Cu, Li, Mo, Ni, Pb, Ti, Zn (base metals) were analysed using a 4-acid digest and read by ICP-AES (ALS method ME-4ACD81, a partial assay technique). All samples were crushed and pulverized so that 95% of the sample passed 75µ (ALS methods CRU-31, PUL-31). The sample preparation and analysis is considered appropriate for the analytes.
	<ul style="list-style-type: none"> For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. 	<ul style="list-style-type: none"> At Victory's Perth facility spot checks were completed on selected samples using a handheld Olympus Vanta XRF unit. The pXRF device was used to determine anomalous REO geochemistry (La, Ce, Nd and Y) from the 1-m sample piles. pXRF reading times were 45 secs over 3 beams for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their analytical accuracy was checked using REO -bearing geochemical standards. The pXRF results were not used for estimation.
	<ul style="list-style-type: none"> Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established. 	<ul style="list-style-type: none"> Sample weights were measured for 174 of the AC drillholes, and recovery was measured for 7 of the diamond drillholes. Sample recovery for the diamond drillholes recovery was 103%. Based on the information available, sample recovery is acceptable for the diamond holes. The discrepancy between the target weight and the measured weight for the air-core samples indicates potential for bias, however, there may have been an issue with the target weight, and this should be reassessed. Assay analytical precision was established by laboratory repeats and was deemed acceptable to the CP. The performance of standards was deemed to be acceptable, except for Eu2O3 and Lu2O3 in OREAS 464 for which the failure rate is high – it is suspected that this is a CRM preparation issue. Results for 103 blank samples are available. The mean TREO for these samples is 23 ppm. The CP's deemed the performance of blanks to be acceptable. Field duplicate data is available only for 14 samples from diamond drill core. The mean grade of the original sample was generally reproduced by the duplicate for the various analytes and is acceptable to the CP's. In April 2024, 37 samples were submitted to an umpire laboratory, Intertek Genalysis in Perth. The results were compared to the original assay results from ALS laboratories for the key analytes of interest to the project. There was no observable bias between the original assays completed by ALS and the checks completed by Intertek Genalysis Perth. Twinned hole results are discussed in the relevant section below.
Verification of sampling and assaying	<ul style="list-style-type: none"> The verification of significant intersections by either independent or alternative company personnel. 	<ul style="list-style-type: none"> Victory's representative Prof Kenneth Collerson (PhD, FAusIMM) undertook verification of significant intersections.
	<ul style="list-style-type: none"> The use of twinned holes. 	<ul style="list-style-type: none"> Eleven percussion (air core and RC) drillholes have been twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis only if the initial screening by handheld pXRF were greater than 200ppm TREO, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole. QQ plots were prepared between the percussion and diamond assays paired at 5m, with good correlation between the two drillhole types.

Criteria	JORC Code explanation	Commentary																																																			
	<ul style="list-style-type: none"> Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. 	<ul style="list-style-type: none"> ALS laboratories routinely re-assayed anomalous assays as part of their normal QAQC procedures 																																																			
	<ul style="list-style-type: none"> Discuss any adjustment to assay data. 	<ul style="list-style-type: none"> REO assay results were adjusted to convert elemental values to the oxide equivalent for REOs. The stoichiometric conversion factors used are provided below: <table border="1"> <thead> <tr> <th>Element</th> <th>Oxide</th> <th>Element to stoichiometric oxide conversion factor</th> </tr> </thead> <tbody> <tr> <td>Ce (Cerium)</td> <td>CeO₂</td> <td>1.2284</td> </tr> <tr> <td>Dy (Dysprosium)</td> <td>Dy₂O₃</td> <td>1.1477</td> </tr> <tr> <td>Er (Erbium)</td> <td>Er₂O₃</td> <td>1.1435</td> </tr> <tr> <td>Eu (Europium)</td> <td>Eu₂O₃</td> <td>1.1579</td> </tr> <tr> <td>Gd (Gadolinium)</td> <td>Gd₂O₃</td> <td>1.1526</td> </tr> <tr> <td>Ho (Holmium)</td> <td>Ho₂O₃</td> <td>1.1455</td> </tr> <tr> <td>La (Lanthanum)</td> <td>La₂O₃</td> <td>1.1728</td> </tr> <tr> <td>Lu (Lutetium)</td> <td>Lu₂O₃</td> <td>1.1371</td> </tr> <tr> <td>Nd (Neodymium)</td> <td>Nd₂O₃</td> <td>1.1664</td> </tr> <tr> <td>Pr (Praseodymium)</td> <td>Pr₆O₁₁</td> <td>1.2082</td> </tr> <tr> <td>Sc (Scandium)</td> <td>Sc₂O₃</td> <td>1.5338</td> </tr> <tr> <td>Sm (Samarium)</td> <td>Sm₂O₃</td> <td>1.1596</td> </tr> <tr> <td>Tb (Terbium)</td> <td>Tb₄O₇</td> <td>1.1762</td> </tr> <tr> <td>Tm (Thulium)</td> <td>Tm₂O₃</td> <td>1.1421</td> </tr> <tr> <td>Y (Yttrium)</td> <td>Y₂O₃</td> <td>1.2699</td> </tr> <tr> <td>Yb (Ytterbium)</td> <td>Yb₂O₃</td> <td>1.1387</td> </tr> </tbody> </table>	Element	Oxide	Element to stoichiometric oxide conversion factor	Ce (Cerium)	CeO ₂	1.2284	Dy (Dysprosium)	Dy ₂ O ₃	1.1477	Er (Erbium)	Er ₂ O ₃	1.1435	Eu (Europium)	Eu ₂ O ₃	1.1579	Gd (Gadolinium)	Gd ₂ O ₃	1.1526	Ho (Holmium)	Ho ₂ O ₃	1.1455	La (Lanthanum)	La ₂ O ₃	1.1728	Lu (Lutetium)	Lu ₂ O ₃	1.1371	Nd (Neodymium)	Nd ₂ O ₃	1.1664	Pr (Praseodymium)	Pr ₆ O ₁₁	1.2082	Sc (Scandium)	Sc ₂ O ₃	1.5338	Sm (Samarium)	Sm ₂ O ₃	1.1596	Tb (Terbium)	Tb ₄ O ₇	1.1762	Tm (Thulium)	Tm ₂ O ₃	1.1421	Y (Yttrium)	Y ₂ O ₃	1.2699	Yb (Ytterbium)	Yb ₂ O ₃	1.1387
Element	Oxide	Element to stoichiometric oxide conversion factor																																																			
Ce (Cerium)	CeO ₂	1.2284																																																			
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Location of data points	<ul style="list-style-type: none"> Accuracy and quality of surveys used to locate drillholes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. 	<ul style="list-style-type: none"> 55% of the drillholes were surveyed by DGPS. The remaining holes were surveyed by handheld GPS with an accuracy of +/- 5 m. Elevation values (Z) were used from the topography surface where no DGPS data was available. There were no downhole surveys completed 																																																			
	<ul style="list-style-type: none"> Specification of the grid system used. 	<ul style="list-style-type: none"> All coordinates are in GDA94 Zone 50 																																																			
	<ul style="list-style-type: none"> Quality and adequacy of topographic control. 	<ul style="list-style-type: none"> A three second SRTM Digital Elevation Model was used to represent the topographical surface sourced from Geoscience Australia. The topography was adjusted by using the DGPS surveyed collar coordinates to model a more accurate topographical surface. It is recommended that a LiDAR based DEM is used in future. 																																																			
Data spacing and distribution	<ul style="list-style-type: none"> Data spacing for reporting of Exploration Results. 	<ul style="list-style-type: none"> The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m. 																																																			
	<ul style="list-style-type: none"> Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral 	<ul style="list-style-type: none"> Given the nature of the exploration programs, the spacing of the exploration drilling is appropriate for understanding the exploration potential and the identification of structural controls on the mineralisation. In areas of closer spaced drilling the spacing demonstrates grade and geological continuity sufficient to support Indicated Mineral Resources. Where drillhole spacing increases, grade and geological continuity can be implied 																																																			

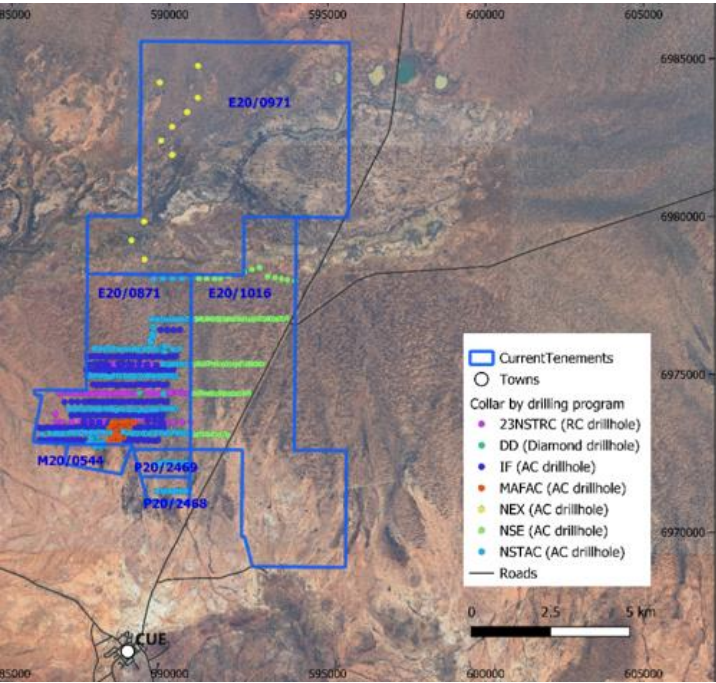
Criteria	JORC Code explanation	Commentary
	<p><i>Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></p>	<p>and has been classified as an Inferred Mineral Resource. Areas where the drillhole spacing is such that grade and geological continuity cannot be implied, have been excluded from the Mineral Resource.</p> <ul style="list-style-type: none"> The applied Mineral Resource classification is commensurate with the grade continuity demonstrated.
	<ul style="list-style-type: none"> <i>Whether sample compositing has been applied.</i> 	<ul style="list-style-type: none"> Percussion samples were collected as 1.0 m samples. Core was collected at a nominal 1.0m samples. Both core and percussion samples were composited to 1.0m for grade estimation purposes. and composited to 1.0m .
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i> 	<ul style="list-style-type: none"> Mineralisation is sub horizontal, as such the vertical drillholes are suitable to test mineralisation thickness. It is concluded from aerial magnetics that any mineralisation trends 010-030. Dips are unknown as the area is covered by a 2-25m blanket of transported cover. Percussion drilling was vertical as the mineralisation is interpreted to be sub parallel to the regolith profile. Downhole widths of mineralisation are known with percussion drilling methods to +/- 1 meter.
	<ul style="list-style-type: none"> <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i> 	<ul style="list-style-type: none"> Mineralisation is sub-horizontal. Azimuths and dips of drilling was designed to intersect the strike of the rocks at right angles.
Sample security	<ul style="list-style-type: none"> <i>The measures taken to ensure sample security.</i> 	<ul style="list-style-type: none"> All samples were packaged and managed by VTM personnel. Larger packages of samples were couriered to Core from Cue by professional transport companies in sealed bulka bags. Unused samples from the percussion drilling are stored at Victory's secure warehouse in Perth.
Audits or reviews	<ul style="list-style-type: none"> <i>The results of any audits or reviews of sampling techniques and data.</i> 	<ul style="list-style-type: none"> MEC conducted an audit of the project data and the historic MRE in April of 2024. The findings were as follows - <ul style="list-style-type: none"> Several validation issues have now been corrected in the drillhole database, and the data is of sufficient quality to inform an Indicated and Inferred mineral resource. There are no downhole surveys so there is a risk of the hole paths deviating from planned, particularly with the deeper drillholes. Satisfactory QAQC data (standards, blanks, and pulp repeats) are available to support the MRE.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
<p>Mineral tenement and land tenure status</p>	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	<ul style="list-style-type: none"> The North Stanmore REO Project MRE comprises six tenements E20/0971, E 20/1016, E 20/0871, M 20/0544, P 20/2468, and P 20/2469. All tenements are held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory Metals Ltd. MEC Mining has verified that at the time of the report date that all tenements are currently in good standing. Native Title claim WC2004/010 (Wajarri Yamatji #1) was registered by the Yaatji Marlpa Aboriginal Corp in 2004 and covers the entire project area, including Coodardy and Emily Wells.
<p>Exploration done by other parties</p>	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> The area has been previously explored by Harmony Gold (2007-2010) in JV with Big Bell Ops, Mt Kersey (1994- 1996), and Westgold (2011), and Metals X (2013). Exploration by these companies has been piecemeal and not regionally systematic. Harmony Gold intersected 3m @ 2.5 g/t Au and 2m @ 8.85 g/t Au in the Mafeking Bore area but did not follow up these intersections. Other historical drill holes in the area commonly intersected > 100 ppb Au. There has been no historical exploration for REOs in the tenement.
<p>Geology</p>	<ul style="list-style-type: none"> Deposit type, geological setting and style of mineralisation 	<ul style="list-style-type: none"> Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgarranga greenstone belts, the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late faults. The greenstone belts were intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. Two large Archaean gabbroid intrusions occur south of Cue. These are the Dalgarranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroid complex in the southeast. The North Stanmore alkaline intrusion, north of Cue, was not recognised on regional geological maps. The petrological and geochemical data indicate that it is post-tectonic and post Archean in age. Similar alkaline intrusions in the vicinity of Cue are interpreted to be related to the early Proterozoic plume track responsible for alkaline magmatism, which extends in a belt from Mt Weld through Leonora to Cue. Mafic and ultramafic sills are abundant in all areas of the Cue greenstones. Gabbro sills are often differentiated with basal pyroxenite and/or peridotite and upper leucogabbroic units.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> The greenstones are deformed by large scale fold structures which are dissected by major faults and shear zones which can be mineralised. Two large suites of granitoids intrude the greenstone belts. The western margin of the project has a signature reflecting a rhyolite, rhyolite-dacite and/or dacitic rock (predominantly acid or felsic rock type). This coincides with an area of elevated TREO/LREO/HREO grades and greater average mineralisation thickness. The deposit type is regolith-hosted REO mineralisation overlying the North Stanmore alkaline intrusion. The REO mineralisation at North Stanmore is predominantly hosted within a relatively flat-laying saprolite-clay horizon, and partially extends into the Sap rock. The Saprolite is covered by 0–36m of unconsolidated colluvium. The saprolite thickness ranges from 14–58m, and overlies a basement of granite, mafic rocks, and other felsic rocks. Mineralogy studies demonstrate that the REOs are mainly hosted by sub-20-μm phases interpreted to be churchite (after xenotime) and rhabdophane (after monazite). The mineralisation is hosted in the saprolite zone of the weathering profile, between the basement granite and surface colluvium.
Drill hole Information	<ul style="list-style-type: none"> A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> easting and northing of the drill hole collar elevation or RL (Reduced Level - elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<ul style="list-style-type: none"> Five hundred and twenty-two (522) drill holes for 31,190m were used for the MRE; inclusive of 462 Air-core (AC) drillholes for 27,347m, 49 Reverse Circulation (RC) drillholes for 3,076m, and 11 diamond drill holes for 765m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory Metals from 2022 to 2023. Drillhole intersections are reported in APPENDIX 1. Drillhole coordinates are shown in APPENDIX 2.
Data aggregation methods	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. 	<ul style="list-style-type: none"> No top cuts were applied as few extreme values were identified. Samples were composited to 1m intervals based on the dominant raw sample length. A geological cutoff grade of 150ppm TREO representing the on-set of mineralisation was used during interpretation to separate mineralised from unmineralised material for the low-grade domain. A high-grade domain was modelled above a TREO 600ppm cut-off. All MRE were reported above an economic cut-off grade of 330ppm TREO.

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> The assumptions used for any reporting of metal equivalent values should be clearly stated. 	
<p>Relationship between mineralisation widths and intercept lengths</p>	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known'). 	<ul style="list-style-type: none"> The clay regolith hosted REO mineralisation is interpreted to be sub horizontal. 88% of the drillholes are vertical, and the remaining are drilled at a dip of -60°. As such intersections approximate the true width of mineralised lodes.
<p>Diagrams</p>	<ul style="list-style-type: none"> Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views 	<ul style="list-style-type: none"> Drillhole collars and tenements are shown below - 

Criteria	JORC Code explanation	Commentary
Balanced reporting	<ul style="list-style-type: none"> Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results. 	<ul style="list-style-type: none"> All exploration results have been reported above a 150ppm TREM cut-off.
Other substantive exploration data	<ul style="list-style-type: none"> Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances 	<ul style="list-style-type: none"> Metallurgical testwork: <ul style="list-style-type: none"> Three stages of metallurgical test work have been completed on the North Stanmore project, focusing on beneficiation, and on leach test work to establish potential recoveries Core Resources ("Core") in Brisbane completed Stage 3 test work including beneficiation test work in March of 2024 and reported an increase, to the Rare Earth Element ("REO") feed grade of 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material. The Leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). Additionally, Scandium ("Sc") recoveries of (50%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO and Sc from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Further work	<ul style="list-style-type: none"> The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive. 	<ul style="list-style-type: none"> Further metallurgical testwork will focus on further optimization of the leaching of the upgraded samples and the generation of Mixed Rare Earth Carbonate (MREC) for potential off takers. Additional variability leach testing of individual samples is also planned. Variability leach testwork will inform geo-metallurgical variability across the North Stanmore project. Further metallurgical test work will also focus on the most optimized leaching conditions and removal of gangue materials against the higher rare earth extractions that can be achieved. Mincore Melbourne have been appointed to conduct a Scoping Study on the North Stanmore Project

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<i>Database integrity</i>	<ul style="list-style-type: none"> Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. 	<ul style="list-style-type: none"> An initial Database was supplied to MEC by RSC, the database was then integrated with newly acquired data by MEC for a data audit before commencing a MRE. All validation issues relating to data were identified and remedied prior to MRE.
	<ul style="list-style-type: none"> Data validation procedures used. 	<ul style="list-style-type: none"> Drillhole collar, downhole survey, assay, geology, and recovery data were imported into Micromine software. The imported data was then compared to the database values with no discrepancies identified. The data was then desurveyed in Micromine and reviewed spatially with no discrepancies identified.
<i>Site visits</i>	<ul style="list-style-type: none"> Comment on any site visits undertaken by the Competent Person and the outcome of those visits. 	<ul style="list-style-type: none"> Dean O’Keefe, the competent person for this Mineral Resource Estimate visited the North Stanmore project site on May 30, 2024. Co CP for the North Stanmore REO MRE, Kahan Cervoj has not conducted a site visit.
	<ul style="list-style-type: none"> If no site visits have been undertaken indicate why this is the case. 	<ul style="list-style-type: none"> A site visit has been conducted by Dean O’Keefe.
<i>Geological interpretation</i>	<ul style="list-style-type: none"> Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. 	<ul style="list-style-type: none"> Confidence in the interpretation of the transported colluvium that truncates the saprolite is commensurate with the drillhole spacing and ranges from low to moderate confidence. The mineralisation is hosted within the saprolite, with some mineralisation extending into the Sap rock. There is reasonable confidence in the interpretation of the saprolite commensurate with the available drilling.
	<ul style="list-style-type: none"> Nature of the data used and of any assumptions made. 	<ul style="list-style-type: none"> Surface AC, RC, as well as diamond drilling, have been used to inform the MRE.
	<ul style="list-style-type: none"> The effect, if any, of alternative interpretations on Mineral Resource estimation. 	<ul style="list-style-type: none"> The potential for alternate interpretations at a prospect scale is considered unlikely. However, there is a likelihood of variation at the local scale, and this has been reflected in the Mineral Resource classification.
	<ul style="list-style-type: none"> The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology. 	<ul style="list-style-type: none"> The MRE has been interpreted as low grade domains representing the on-set of REO mineralisation at 150ppm TREO (low grade or LG), and higher-grade core greater than 600ppm TREO (high grade or HG).
<i>Dimensions</i>	<ul style="list-style-type: none"> The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource. 	<ul style="list-style-type: none"> The North Stanmore deposit extends over 8km across and along strike and is around 70m thick; mineralisation varies between 4m to 60m in true thickness. The southwestern part of the deposit is thicker than the remainder of the deposit.
<i>Estimation and modelling techniques</i>	<ul style="list-style-type: none"> The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used. 	<ul style="list-style-type: none"> The final interpretational wireframes and estimation work was completed using Micromine v2023.5. The estimation was constrained by hard domain boundaries generated from mineralisation wireframes. The available samples were coded by domains (HG, LG), and 1.0m composites were created honouring these boundaries.

Criteria	JORC Code explanation	Commentary																								
		<ul style="list-style-type: none"> The REO graded was estimated using ordinary kriging of the 1.0m composite grades for individual REO grades, HREO, LREO, and TREO. The estimation for credit elements was completed using Inverse Distance Cubed for Cu, Ni, Co, Hf, and Sc. There were no extreme values observed that required topcuts to be applied. For estimation purposes, all boundaries were treated as hard boundaries. The primary search was 500 m in the direction of maximum continuity, 400 m along the intermediate direction of continuity, and 25 m in the minor direction of continuity. Up to 5 samples per octant sector (maximum number of informing samples was 40 samples) were used. The secondary search was 1,000 m in the direction of maximum continuity, 800 m along the intermediate direction of continuity, and 50 m in the minor direction of continuity, up to 5 samples per octant sector (maximum of 40 informing samples) was used. The third search was 1,500 m in the direction of maximum continuity, 1,200 m along the intermediate direction of continuity, and 75m in the minor direction of continuity, with a maximum of 40 informing samples (no octant search applied). The maximum distance for extrapolation for the Inferred Mineral Resource was 1,500 m. 																								
	<ul style="list-style-type: none"> The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data. 	<ul style="list-style-type: none"> The July 2024 MEC MRE was compared to the previous August 2023 RSC MRE. An economic cutoff grade of TREO >330ppm was applied to the MEC Mining July 2024 MRE due to scandium, hafnium, being potential credit elements along with the presence of nickel, cobalt, and copper. MEC reported the MRE at a reduced cut-off grade as the TREO was inclusive of scandium. MRE tonnage is similar, the TREO ppm grade is also similar, and as a result the contained TREO. <table border="1" data-bbox="1205 981 2029 1061"> <thead> <tr> <th>MRE</th> <th>CUTOFF TREO ppm</th> <th>Tonnage Mt</th> <th>TREO (Y) ppm</th> <th>MREO ppm</th> <th>HREO ppm</th> <th>NdPr ppm</th> <th>TREO (Y) t</th> </tr> </thead> <tbody> <tr> <td>RSC August 2023</td> <td>400</td> <td>250</td> <td>520</td> <td>110</td> <td>170</td> <td>90</td> <td>130,000</td> </tr> <tr> <td>MEC July 2024</td> <td>330</td> <td>235</td> <td>520</td> <td>107</td> <td>180</td> <td>87</td> <td>122,300</td> </tr> </tbody> </table>	MRE	CUTOFF TREO ppm	Tonnage Mt	TREO (Y) ppm	MREO ppm	HREO ppm	NdPr ppm	TREO (Y) t	RSC August 2023	400	250	520	110	170	90	130,000	MEC July 2024	330	235	520	107	180	87	122,300
MRE	CUTOFF TREO ppm	Tonnage Mt	TREO (Y) ppm	MREO ppm	HREO ppm	NdPr ppm	TREO (Y) t																			
RSC August 2023	400	250	520	110	170	90	130,000																			
MEC July 2024	330	235	520	107	180	87	122,300																			
	<ul style="list-style-type: none"> The assumptions made regarding recovery of by-products. 	<ul style="list-style-type: none"> Test work has demonstrated that scandium is recoverable and may become a byproduct. Available metallurgical test work has demonstrated that likely processing will be able to recover significant proportions of Scandium, Nickel, Cobalt, Copper and Hafnium. 																								

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation). 	<ul style="list-style-type: none"> Test work completed by Victory Metals determined that the level of Uranium (U) and Thorium (Th). The levels of uranium and thorium were assessed for the project and returned very low values. Due to the low values within both ore and waste the uranium and thorium were not estimated, however, both values may be estimated in the future of required for integration into processing studies. <p>Waste U Max = 24ppm, Mean = 1.7ppm Th Max = 67ppm, Mean = 7.9ppm</p> <p>Low Grade (+150ppm TREO) U Max = 12ppm, Mean = 2.11ppm Th Max = 61ppm, Mean = 7.15ppm</p> <p>High grade (+600ppm TREO) U Max = 11ppm, Mean = 1.8ppm Th Max = 68ppm, Mean = 6.9ppm</p> <ul style="list-style-type: none"> Metallurgical recovery to date of deleterious Uranium (U) 2.4ppm and Thorium (Th) 5ppm are less than average abundances in the upper continental crust (U) 3ppm (Th) 10ppm. Scandium, Copper, Cobalt, and Nickel were estimated within this MRE and are considered significant.
	<ul style="list-style-type: none"> In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. 	<ul style="list-style-type: none"> Drillhole spacing is consistent and varies in the East and North-East of the deposit. Nominal drillhole spacing is 50 x 50m expanding to ~250 north by 100m east across strike. The block size used for the estimation 50m east x 50m north and 1 mRL.
	<ul style="list-style-type: none"> Any assumptions behind modelling of selective mining units. 	<ul style="list-style-type: none"> No support correction was applied to allow for selective mining units at this stage of the project life.
	<ul style="list-style-type: none"> Any assumptions about correlation between variables 	<ul style="list-style-type: none"> No assumptions were made regarding correlations between variables.
	<ul style="list-style-type: none"> Description of how the geological interpretation was used to control the resource estimates. 	<ul style="list-style-type: none"> A geological cutoff grade of 150ppm was chosen to distinguish the mineralised material from poorly unmineralised material. The low-grade domain was then Interpreted at 150ppm TREO reflecting the on-set of mineralisation. The interpretation was carried out in section lines and a highly mineralised domain with TREO greater than 600ppm was also delineated.
	<ul style="list-style-type: none"> Discussion of basis for using or not using grade cutting or capping. 	<ul style="list-style-type: none"> Few extreme values were present and no topcuts were applied.
	<ul style="list-style-type: none"> The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available. 	<ul style="list-style-type: none"> The OBM estimate was validated, validation approaches included: <ul style="list-style-type: none"> Visual checks for composite grades versus estimated block grades.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> ○ Comparison of global mean grades of composites versus blocks for each Domain. This check ensures that the global statistics for each estimated variable represent the composited statistics in that domain. ○ Histograms of composites versus block distributions to check preservation of the distribution post-estimate. ○ Swath plots (also known as trend plots) to compare the spatial variation of grades between composites and blocks across the block model. ○ On completion of the OBM, checks were conducted for overlapping or missing blocks, and none were found. • Primary relevant elements of interest were estimated individually (Dy₂O₃, Er₂O₃, Eu₂O₃, Gd₂O₃, Ho₂O₃, La₂O₃, Lu₂O₃, Nd₂O₃, Pr₆O₁₁, Sm₂O₃, Tb₄O₇, Tm₂O₃, Y₂O₃, Yb₂O₃).
Moisture	<ul style="list-style-type: none"> • Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content. 	<ul style="list-style-type: none"> • Tonnages were estimated on a dry basis.
Cut-off parameters	<ul style="list-style-type: none"> • The basis of the adopted cut-off grade(s) or quality parameters applied. 	<ul style="list-style-type: none"> • The MRE was reported at a 330ppm TREO cutoff grade.
Mining factors or assumptions	<ul style="list-style-type: none"> • Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources • • not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made. 	<ul style="list-style-type: none"> • The CPs deems that there are reasonable prospects for eventual economic extraction using open pit mining methods as a function of: <ul style="list-style-type: none"> ○ The relative shallow depth of the mineralisation and presence of loosely consolidated transported Colluvium above the mineralisation. ○ Proximity to significant existing infrastructure (located adjacent to the Gt Northern Highway and the township of Cue). • Future pit optimisation studies will confirm the designation of the blocks for RPEEE.

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	<ul style="list-style-type: none"> The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made. 	<ul style="list-style-type: none"> Extensive metallurgical studies by Core metallurgy regarding the beneficiation and extraction of Ce, Dy, Er, Eu, Gd, Ho, La, Lu, Mn, Nd, Pr, Sc, Sm, Tb, Th, Tm, U, Y, Yb, have been completed. The leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trailed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements (“MREO”). Additionally, Scandium (“Sc”) recoveries of (50%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO and Sc from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Environmental factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made. 	<ul style="list-style-type: none"> The North Stanmore prospect is located in the Murchison of Western Australia, a mining district with considerable mining history and well understood environmental standards and protocols. No environmental assumptions were made for the MRE. Scoping studies will assess these requirements in the future.
Bulk density	<ul style="list-style-type: none"> Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. 	<ul style="list-style-type: none"> Downhole geophysical density is available for 10 diamond drillholes at 10cm depth increments, for a total of 5,896 readings. Core length, diameter and weight are available for 8 of the diamond drillholes for 50 readings Regression analysis was performed to compare the two different approaches to measuring density. The regression calculated densities were used for the high grade and low-grade domains separately to estimate MRE tonnage.
	<ul style="list-style-type: none"> The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit. 	<ul style="list-style-type: none"> Downhole density measurements were obtained from 10 diamond drillholes at 10cm depth increments, for 5,896 readings. No anomalous density readings were observed in the data. Downhole geophysical density measurements were taken in rod, then corrected to account for this, using a factor calculated from a calibration drillhole (DD004).

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> Discuss assumptions for bulk density estimates used in the evaluation process of the different materials. 	<ul style="list-style-type: none"> Core length, diameter and weight are available for 8 of the diamond drillholes for a total of 50 readings. From this information, density was calculated using the formula: $\text{Density} = \frac{m}{\pi r^2 h}$ Where “r” is the radius of the PQ core (0.0425m), “h” is the length of the core in metres, and “m” is the mass in kilograms. The density was converted from kg/m³ to g/cm³ for consistency with units used for downhole geophysical density. Four anomalous calculated density values were identified where density <1 g/cm³. Regression analysis was applied to calculate the density from geophysical measurements for the high grade and low-grade domains. The mean density from regression analysis for the High-grade domain is 1.75t/m³, and for the low-grade domain 2.02t/m³.
Classification	<ul style="list-style-type: none"> The basis for the classification of the Mineral Resources into varying confidence categories. 	<ul style="list-style-type: none"> Mineral Resources were classified as Indicated and Inferred. Material not classified as either Indicated or inferred Material remains unclassified material has been reported as Exploration Target. Indicated Mineral Resource classification was based on drillhole spacing (250 x 100m closing to 50 x 50m in some areas), acceptable underlying QAQC, and DGPS survey of drillhole collar. The DGPS survey provided increased certainty regarding the drillhole collar location and compensated for a low-resolution topography survey. The topographical surface was adjusted to include the DGPS surveyed drillhole collar coordinates. 63% (by tonnage) of the MRE are classified as Indicated Mineral Resources, 37% (by tonnage) are classified as Inferred Mineral Resources.
	<ul style="list-style-type: none"> Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). 	<ul style="list-style-type: none"> Grade and tonnage estimation has been considered for the MRE classification. The CP’s have considered all relevant factors
	<ul style="list-style-type: none"> Whether the result appropriately reflects the Competent Person’s view of the deposit. 	<ul style="list-style-type: none"> The MRE classification of Inferred and Indicated MRE reflects the CP’s understanding of the deposit.
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of Mineral Resource estimates. 	<ul style="list-style-type: none"> MEC has conducted an internal review of the July 2023 MRE.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. 	<ul style="list-style-type: none"> No statistical test of the accuracy and confidence in the MRE has been undertaken. The low variability of the mineralisation grades, the relatively consistent mineralisation geometry, the geometry and large areal extent of the mineralisation provide qualitative confidence in the MRE.
	<ul style="list-style-type: none"> The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. 	<ul style="list-style-type: none"> The estimate is considered a good global estimate, and the relative confidence in the underlying data (QAQC), drillhole spacing, geological continuity and

Criteria	JORC Code explanation	Commentary
	<p><i>Documentation should include assumptions made and the procedures used.</i></p>	<p>interpretation, has been appropriately reflected by the CPs in the Resource Classification.</p>
	<ul style="list-style-type: none"> • <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> • There has been no production at the North Stanmore project.